

DESIGN AND ANALYSIS OF A DISTRIBUTED WATER HEAT PUMP SYSTEM FOR
NEAR- AND NET-ZERO ENERGY COMMERCIAL BUILDINGS

by

Maudud Hassan Quazi

Bachelor of Engineering (Mechanical)
Ryerson University
Toronto, Canada, 2007

A MRP
presented to Ryerson University
in partial fulfillment of the
requirements for the degree of
Master of Engineering
in the program of
Mechanical and Industrial Engineering

Toronto, Ontario, Canada 2016
©(Maudud Hassan Quazi) 2016

AUTHOR'S DECLARATION FOR ELECTRONIC SUBMISSION OF A MRP

I hereby declare that I am the sole author of this MRP. This is a true copy of the MRP, including any required final revisions, as accepted by my examiners.

I authorize Ryerson University to lend this MRP to other institutions or individuals for the purpose of scholarly research.

I further authorize Ryerson University to reproduce this MRP by photocopying or by other means, in total or in part, at the request of other institutions or individuals for the purpose of scholarly research.

I understand that my MRP may be made electronically available to the public.

DESIGN AND ANALYSIS OF A DISTRIBUTED WATER HEAT PUMP SYSTEM FOR NEAR- AND NET-ZERO ENERGY COMMERCIAL BUILDINGS

Master of Engineering (Mechanical), 2016

Maudud Hassan Quazi
Ryerson University

Abstract

This objective of this project is to determine the energy and environmental potential of distributed common loop water source heat pump system in a near or net-zero commercial office building, which has simultaneous heating and cooling load in winter and shoulder seasons. It is expected that the perimeter zones will have heating demand during those months, while the core zones will have consistent cooling demand throughout the year. The motive is to reclaim the rejected heat from the cooling operation and transfer it to the zones requiring heating. The building under study is a 60,000 ft² three storey commercial office building, which has private offices along the perimeter, and open work area in the core.

In the first part of the analysis, the base building has been modelled and simulated to the minimum requirements of ASHRAE 90.1-Energy Standard for Buildings except Low-Rise Residential Buildings using simulation software eQuest 3.65. The Heating Ventilation and Air-conditioning (HVAC) system used is four-pipe fan coil system serving individual zones. The fan coil units use a centralized natural gas boiler and a variable capacity centrifugal chiller as external source of heating and cooling respectively. The base case consumes a total of 524.54 x 1000 kWh of electricity and 1,056 million Btu of natural gas annually.

The second part is the modelling and simulation of a proposed case, which uses the same building envelope, occupancy, lighting and equipment as the base case. The HVAC system used is a distributed common loop heat pump system connected to a cooling tower for heat rejection, and a condensing boiler for heat addition. During the occupied hours, when simultaneous cooling and heating loads exist in the building, the cooling zone heat pumps rejects exhaust heat into the common loop, and the heat is subsequently used by the heat pumps operating in heating mode. Using this method, the heat pump system reduces its dependence on the cooling tower and the boiler, which only operate to maintain the loop temperature in an acceptable range.

There is 9,510 kWh (1.81%) increase in electricity consumption by proposed case comparing to the base building. Natural gas consumption has been reduced by 353.65 million Btu (33.48%). Annual utility bill has increased by \$1,483.00 which is 1.88% higher than the base case. 15.7 tonnes of greenhouse gas can be reduced if the proposed case is adopted.

Acknowledgements

First of all, I would like to humble myself to my Creator, who has given me the ability to learn.

I would like to thank Dr. Alan Fung for being my advisor and for providing his valuable guidance for this project. I would also like to thank Dr. Wey Leong for serving on the examination committee.

I would like to recognize the tireless support of my parents and siblings for my education and the sacrifices of my wife and son during my master's study.

Table of Contents

Author's declaration.....	.ii
Abstract.....	.iii
Acknowledgements.....	.v
List of Tables.....	.viii
List of Figures.....	.ix
List of Appendices.....	.x
1. Introduction.....	.1
1.1 Purpose of the project.....	.1
1.2 Energy use of commercial buildings in Canada.....	.1
1.3 Commercial building heating and cooling load characteristics.....	.4
1.4 Heating ventilation and air conditioning (HVAC) system.....	.6
1.5 Heat pump technology and its working principal.....	.9
1.6 Energy efficiency requirement for internal closed loop heat pumps.....	.15
1.7 AHRAE 90.1 Standard.....	.15
1.8 eQuest building simulation tool.....	.18
1.9 HVAC Zoning in eQuest.....	.20
1.10 Net zero energy building.....	.20
2. Literature Review.....	.22
2.1 Overview of building simulation.....	.22
2.2 Building envelope design for energy balance.....	.25
2.3 Net zero energy building design.....	.29
2.4 Effect of building aspect ratio on energy efficiency.....	.34
2.5 Design of typical water source heat pump systems.....	.35
2.5.1 Daikin McQuay Inc. design guide for heat pumps.....	.35
2.5.2 Thermal performance of heat pumps.....	.42
2.5.3 Effect of heat pump operating conditions.....	.43
2.6 Energy conservation using water source heat pumps.....	.45
2.7 Optimizing water loop temperature.....	.47
2.8 Case study: Office building heat recovery using heat pumps.....	.47
3. Objective and methodology.....	.51
4. Modelling and simulation.....	.52
4.1 The base case.....	.52
4.1.1 Base case simulation results.....	.62
4.2 Proposed case 1.....	.66
4.3 Result comparison.....	.71
4.4 Greenhouse gas reduction.....	.73
5. Modelling and sensitivity analysis.....	.75
5.1 Sensitivity analysis for finding optimum operating temperature of the loop.....	.75
5.1.1 Proposed case 2.....	.75
5.1.2 Proposed case 3.....	.75
5.1.3 Proposed case 4.....	.75
5.1.4 Energy consumption comparison.....	.76
5.2 Comparison between the base case and optimum proposed case.....	.76
6. Conclusion.....	.78

References.....	154
-----------------	-----

List of Tables

Table 1: Building characteristics and energy use by primary activity.....	6
Table 2: Daikin McQuay water source heat pump performance.....	12
Table 3. ClimateMaster water source heat pump performance.....	13
Table 4: Trance Inc. Water source heat pump performance.....	14
Table 5: Minimum COP requirements for internal loop heat pumps (NRCan).....	15
Table 6: Climate zone designation.....	30
Table 7: Aspect ratio for simulation geometry (McKeen & Fung).....	34
Table 8: Annual energy consumption for different aspect ratio (McKeen & Fung).....	35
Table 9: Cooling COP of water source heat pump in variant condition (Zheng & Jing).....	44
Table 10: Heating COP of water source heat pump in variant condition (Zheng & Jing).....	44
Table 11: Modelling parameters of the commercial office building for case study (Rao & Harry).....	46
Base building design parameters:	
Table 12: Project and site data.....	53
Table 13: Electricity time of use (TOU) rate for summer.....	53
Table 13A: Electricity time of use (TOU) rate for winter.....	54
Table 14: Natural gas rate.....	54
Table 15: Building shell and footprint.....	55
Table 16: Building envelope construction.....	55
Table 17: Exterior doors and windows.....	56
Table 18: Exterior shades and blinds.....	56
Table 19: Roof skylight schedule.....	56
Table 20: Daylight control.....	57
Table 21: Building operation schedule.....	57
Table 22: Activity area allocation.....	57
Table 23: Interior lighting loads.....	58
Table 24: Office equipment loads and profiles.....	58
Table 25: Zone HVAC system parameters.....	59
Table 26: Cooling primary equipment design parameters.....	59
Table 27: Heating primary equipment.....	60
Table 28: Domestic hot water modelling parameters.....	60
Table 29: Base building peak load components (eQuest simulation result).....	63
Table 30: Base building zone peak heating and cooling loads (eQuest simulation result).....	64
Table 31: Base building monthly and annual electricity consumption.....	65
Table 32: Base building monthly and annual gas consumption.....	66
Table 33: Proposed case 1 zone HVAC system parameters.....	67
Table 34: Proposed case 1 water source heat pump.....	67
Table 35: Proposed case 1 monthly and annual electricity consumption.....	69
Table 36: Proposed case 1 monthly and annual natural gas consumption.....	70
Table 37: Proposed case 1 hourly energy consumption data on January 4 th	71
Table 38: Base case vs proposed case 1 electricity consumption comparison.....	72
Table 39: Base case vs proposed case 1 natural gas consumption.....	73
Table 40: Sensitivity test to optimize heat pump water loop temperature.....	76
Table 41: Energy and economic comparison between the base and the optimum proposed case.	77

List of Figures

Figure 1: Secondary energy use by sector (NRCan).....	2
Figure 2: GHG emission by sector (NRCan).....	2
Figure 3: Commercial/institutional floor space by activity type in 2009 (NRCan).....	3
Figure 4: Energy use by fuel type (NRCan).....	3
Figure 5: Energy use by end-uses (NRCan).....	4
Figure 6: Example of an all air HVAC system.....	7
Figure 7: Example of water-to-air HVAC system.....	8
Figure 8: Example of a building air system designed in eQuest.....	9
Figure 9: Heat pump cycle based on vapour compression.....	10
Figure 10: Example of a 3D building model generated by eQuest.....	19
Figure 11: Energy transfer between a building and its surrounding (Chwieduk).....	29
Figure 12: Annual energy use intensity of commercial buildings in different zones based on average of 16 commercial building type (Hootman).....	31
Figure 13: Commercial/institutional building energy intensity by activity type (NRCan).....	32
Figure 14: Configuration of conventional water-source heat pump system for cooling only operation (Daikin McQuay Inc.).....	37
Figure 15: Configuration of conventional water-source heat pump system for mainly heating operation (Daikin McQuay Inc.).....	38
Figure 16: Configuration of conventional water-source heat pump system in buildings with high internal gain (Daikin McQuay Inc.).....	39
Figure 17: Configuration of conventional water-source heat pump system for simultaneous cooling and heating load (Daikin McQuay Inc.).....	40
Figure 18: Heat pump system with heat storage (Daikin McQuay Inc.).....	41
Figure 19: Source temperature at supply and return sides of the heat pump (Liu, Qu, Ge).....	43
Figure 20: Schematic for ventilation heating and cooling system of a building using heat pump heat recovery system.....	49
Figure 21: Modelled vs actual energy consumption of a building using heat pump heat recovery system.....	50
Figure 22: 3D view of the three storey office building for the base case.....	61
Figure 23: Schematic of heating, cooling and domestic hot water for the base building.....	62
Figure 24: Common loop water source heat pump schematic for the proposed case.....	68

List of Appendices

Appendix 1: Conceptual design of common loop water source heat pump with heat storage.....	79
Appendix 2: Typical office floor layout with water source heat pumps.....	81
Appendix 3: Building load from eQuest simulation.....	83

1. Introduction

1.1 Purpose of the Project

The purpose of this project is to examine energy saving potential of an office building located in Toronto by modelling it to ASHRAE 90.1 standard and using distributed water loop heat pump (DWLHP) system for providing simultaneous heating and cooling in different zones. Toronto has a large number of commercial buildings used for variety of different industries. Often the office buildings have cooling load in the core zones during the winter season because of heat generated from occupancy, lighting and other office equipment. Buildings also lose heat to the ambient during the winter because of the difference between the indoor design temperature and the outdoor temperature. Thus addition of heating energy is required to maintain the indoor comfort condition. A common loop water source heat pump is a system, where some heat pumps extract heat from the water loop and add thermodynamic work in order to release higher amount of heat to the space; on the other hand heat pumps in cooling mode extract heat from the space and perform thermodynamic work to reject more heat to the water loop. It is also known that normally the offices are occupied for a certain period of time during the day, and unoccupied for the remaining hours. During the unoccupied hours of winter, interior heat generation does not take place. Therefore, to eliminate the role of external heat generating equipment, the cumulative daily heat rejection to the common water loop must exceed the cumulative daily heat extracted.

1.2 Energy Use of Commercial Buildings

According to a Natural Resources Canada publication titled Energy Efficiency Trends in Canada 1990 to 2009, floor space for the entire commercial/institutional sector is equivalent to about 40 percent of the total residential floor space. In 2009, the commercial/institutional sector was responsible for 14 percent of the total energy use in Canada and produced 13 percent of the associated greenhouse gas (GHG) emissions, shown in Figure 1 and Figure 2 (NRCan, 2011).

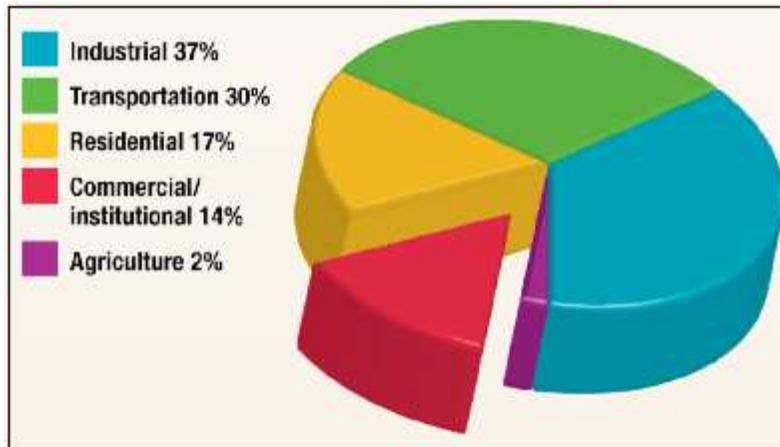


Figure 1: Secondary energy use by sector (NRCan, 2011)

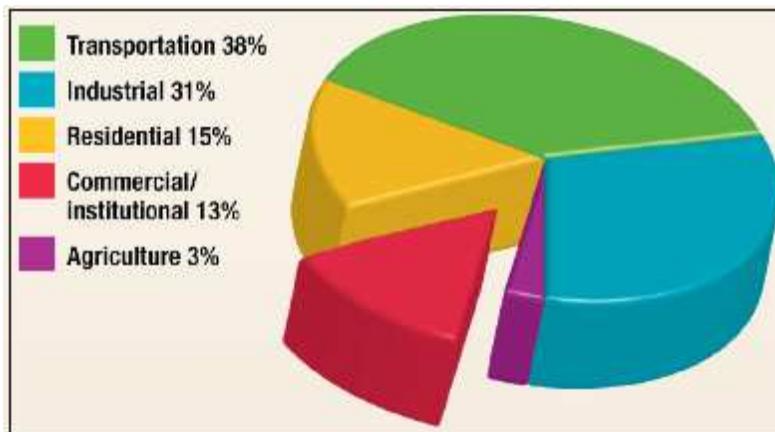


Figure 2: GHG emission by sector (NRCan, 2011)

Space heating accounts for the largest share of energy use. Figure 3 shows that in the commercial sector offices, retail trade and educational services account for 70 percent of the total Canadian commercial/institutional floor space, which in 2009 was estimated at 709.5 million m² (NRCan, 2011).

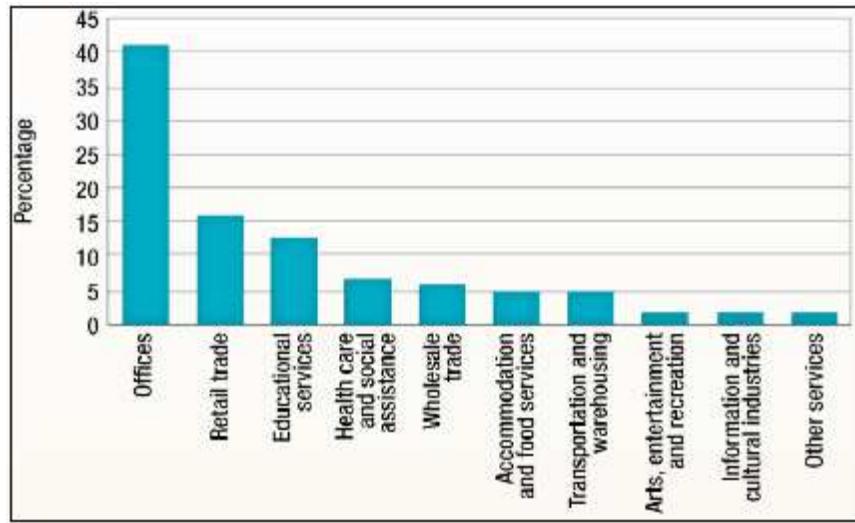


Figure 3: Commercial/institutional floor space by activity type in 2009 (NRCan, 2011)

Natural gas and electricity are the main energy source for the commercial/industrial sector, accounting for 87 percent of the energy use. According to Figure 4 and Figure 5, electricity is the primary source of energy for lighting, space cooling, auxiliary motors and equipment. Natural gas and the remaining fuels are the primary energy sources for space and water heating (NRCan, 2011).

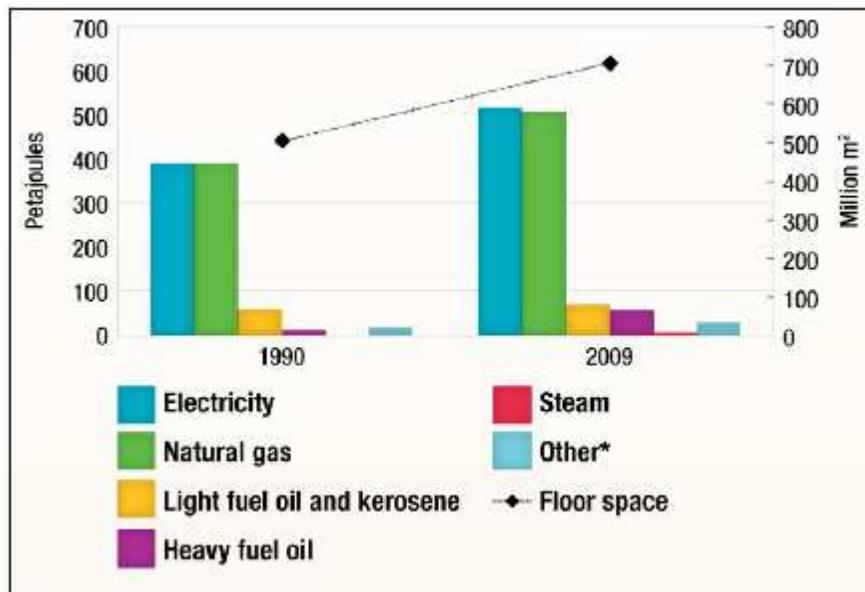


Figure 4: Energy use by fuel type (NRCan, 2011)

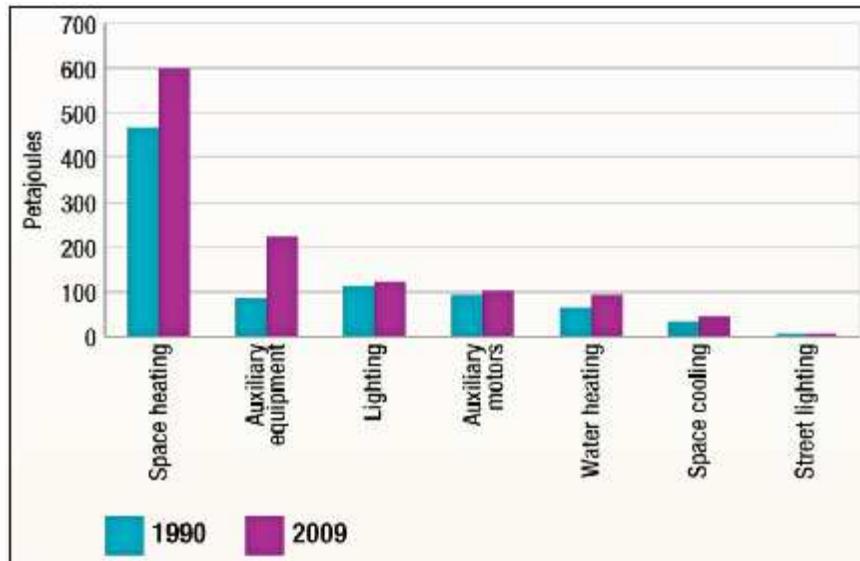


Figure 5: Energy use by end-use (NRCAN, 2011)

1.3 Commercial Building heating and cooling load characteristics

Office buildings are of two types; those that are occupied by the owner for company head office or local business, and the ones that are built for leasing to tenants. In both cases a safe and comfortable working condition takes the utmost priority. A comfortable indoor working condition is vital to the performance of the workers and thus, a design must take in consideration all necessary factors. Few important environmental requirements for comfortable working conditions are temperature, humidity, air movement, noise, cleanliness. The factors that affect the environmental requirements are: climate conditions: local temperature, humidity, wind speed, day and night length, rain, snow etc.

Building Physical Characteristics include:

- Building envelope such as wall, floor, roof, windows, doors and framing.
- Orientation and aspect ratio of the building.
- Reflectance and solar heat gain through the windows and doors.
- Heat loss/heat gain and humidity transfer through infiltration dependent upon the air tightness of the building envelope.
- Internal sources such as lighting, office equipment, motors etc.

Enclosed space require fresh air supply, which is required to be heated, cooled, humidified and de-humidified based on design conditions.

Density of population adds to the heating/cooling load of the building in two ways. Human body produces heat, thus higher occupancy density adds more heat to the indoor environment, and increases requirement for cooling while decreases heating requirement. Higher occupancy also requires increased outdoor air, which need to be conditioned before introducing to the indoor environment. Activities of the occupant also contribute to the heating and cooling load. Walking or physical activities generate more heat than sedentary activities.

This project analyzes and optimizes aspects of building design, which contributes to the heating and cooling load as well as energy consumption. These factors will be discussed in details in the forthcoming sections.

While building envelope design and internal factors influence heating and cooling load in the interior space, building HVAC system provide the heating, cooling, humidification and de-humidification for maintaining indoor comfort condition. The perception of comfort, temperature and thermal acceptability is related to one's rate of metabolic heat production, its rate of transfer to the environment, and the resulting physiological adjustments and body temperatures. The heat transfer rate from the body is influenced by the environmental factors of air temperature, thermal radiation, air movement, and humidity, and by the personal factors of activity and clothing. The temperature range for comfort in summer is higher than for winter. The acceptable range of operative temperature for winter and summer is 73 - 75 °F (23 - 24 °C) (McQuiston, 1982).

In the process of producing cooling and heating for buildings, the HVAC system consumes energy in the form of electricity, natural gas, oil and other sources. The total energy consumptions of commercial and institutional buildings account for 12% of Canada's secondary energy use and 11% of our national greenhouse gas (GHG) emission (NRCan, 2011). In the United States residential and commercial buildings consume over 40% of all the primary energy supply. They also represent over 72% of all electrical power generation and 55% of natural gas consumption. Table 1 shows that according to a 2009 report by Natural Resources Canada titled

‘Commercial and Institutional Energy Use-Building 2009’, commercial office (non-medical) buildings make up 147.5 million m² of floor space, which is 19.25% of all commercial and institutional buildings (NRCan, 2012).

Table 1: Building characteristics and energy use by primary activity (NRCan, 2012)

Primary activity	Building characteristics and energy use by primary activity of the building								
		Buildings	Floor space		Energy use		Energy intensity		
			Q.I.	(millions of m ²)	Q.I.	(PJ)	Q.I.	(GJ/m ²)	Q.I.
Office building (non-medical)	83 583	A	147.5	A	176.6	A	1.20	A	
Medical office building	10 525	A	9.6	A	10.5	A	1.09	A	
Elementary or secondary school	18 425	A	83.6	A	64.4	A	0.77	A	
Nursing or residential care facility	6 482	A	25.0	B	39.1	B	1.56	A	
Warehouse	32 879	A	83.0	A	55.0	A	0.66	A	
Hotel or motel	9 963	C	19.7	B	26.5	C	1.35	A	
Hospital	752	A	15.1	A	36.5	A	2.42	A	
Food or beverage store	40 403	A	29.3	A	82.7	A	2.82	A	
Non-food retail store	56 750	A	68.9	A	65.2	A	0.95	A	
Other*	222 505	A	284.3	A	285.8	A	1.01	A	
Canada	482 266	A	765.9	A	842.2	A	1.10	A	

Building overall energy performance can be improved by two ways:

- Improving construction of the building envelope to minimize transfer of heat and moisture through the wall, roof, windows and doors.
- Improving energy consumption of the HVAC system by optimizing design, and using fuel efficient equipment.

1.4 Building Heating Ventilation and Air-Conditioning (HVAC) System

As mentioned earlier, providing comfort condition in the building indoor environment is necessary for performance of the occupants. Building HVAC system maintains the indoor comfort condition by offsetting the heat gain/loss through building envelope, infiltration, fresh air and internal gain/loss. Building HVAC system is normally sized to meet annual peak heating and cooling demands though the peak conditions may happen for a very short time of the year. During the cooling mode the HVAC system removes heat from the indoor environment and releases the removed heat to the ambient; during the heating season, the HVAC system adds heat

to the indoor environment to raise the space temperature. Common HVAC systems are three types:

- All air system
- Water to air system
- All water system

All Air System:

An all air HVAC system uses only air to deliver heating and cooling to the space. It does not use any water to generate or transport energy. Normally cooling is produced by DX coils, and cooled air is blown into the indoor space by fans. Heating is produced by electric heater or gas burner. Supply fans are used for blowing air into the zones. Return fan draws room air, part of which is exhausted so that fresh outdoor air can be brought in through the supply fan. Part of the return air, which is already conditioned, is mixed with the fresh air, conditioned by the heating or the cooling system, and then re-circulated back into the indoor space by the supply air. A typical all air system is shown in Figure 6.

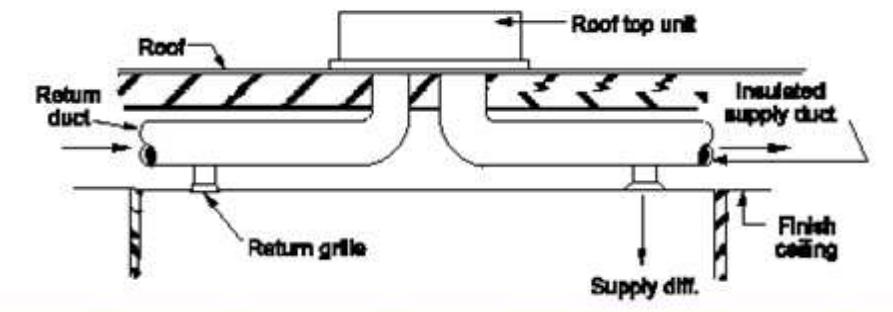


Figure 6: Example of an air system (Schneider Electric, 2006)

Water-to-air System:

Cooling is produced by a cooling unit, which can be of many types such as chiller, heat pump, cooling economizer, deep lake cooling system. Cold water is then transmitted through carrying pipe and circulated through cooling coil. During the heating season, hot water is produced by boiler, heat pump, solar heating system etc., and pumped through hot water pipes and finally circulated through hot water coils. For both heating and cooling, air is blown over the heating/cooling coil in order to bring the space supply air to design temperature. A typical

water-to-air HVAC system is shown in Figure 7.

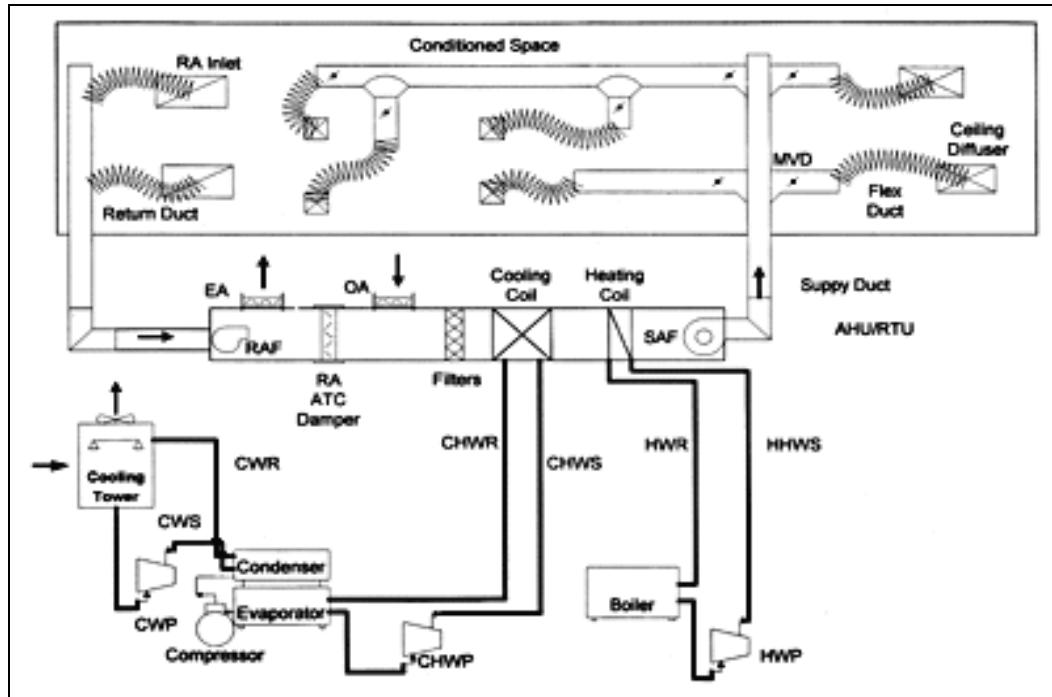


Figure 7: Example of a water-to-air HVAC system (Schneider Electric, 2006)

All Water System:

All water system does not use any fan to blow tempered air into the zone. Normally cooling and heating is produced in the central plant by cooling equipment such as chiller, heat pump etc. and heating equipment such as boiler, solar system etc. and transported through pipes to the individual zones. Depending on the cooling or heating demand, chilled or heated water is then circulated through coils or tubes, which emit heat to the space through radiation. Examples of all-water system are radiant floor heater, baseboard radiator, ceiling radiator etc.

In all of the above cases provision must be made to draw fresh outside air into the room to meet ASHRAE-62.1 minimum fresh air requirement.

Figure 8 shows screenshot of a sample air side HVAC system modelled in eQuest energy simulation software.

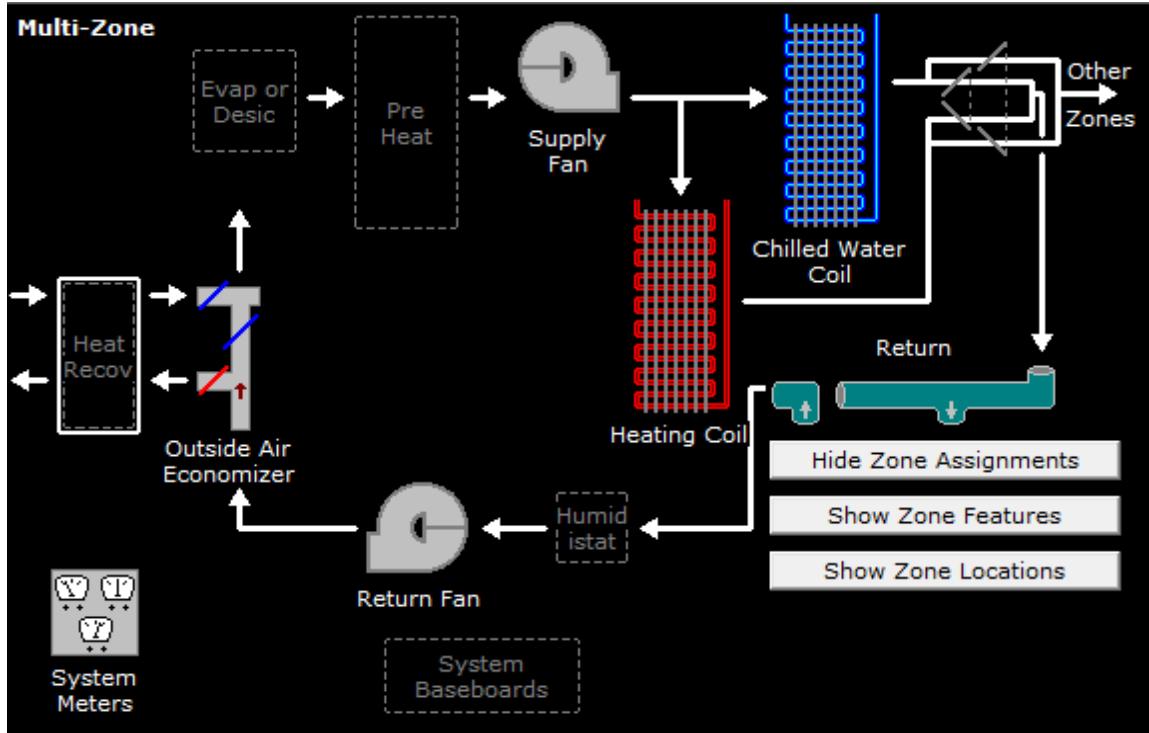


Figure 8: Building air system designed in eQuest

1.5 Heat Pump Technology

Traditionally heat pumps are designed based on vapor compression cycle. In the heating mode, heat is generally absorbed from the heat source (evaporator) and released to the zone (condenser) in requirement of heating. In the cooling mode, heat is extracted from the zone (evaporator), which requires cooling, and released into a relatively cooler heat sink (condenser). As this project involves water source heat pumps, water is the heat source in heating mode and heat sink in the cooling mode; room air is heat sink in the heating mode and heat source in the cooling mode. Different types of refrigerant gases are used in the vapor compression systems. Figure 9 illustrates a process flow of the refrigeration in a heat pump.

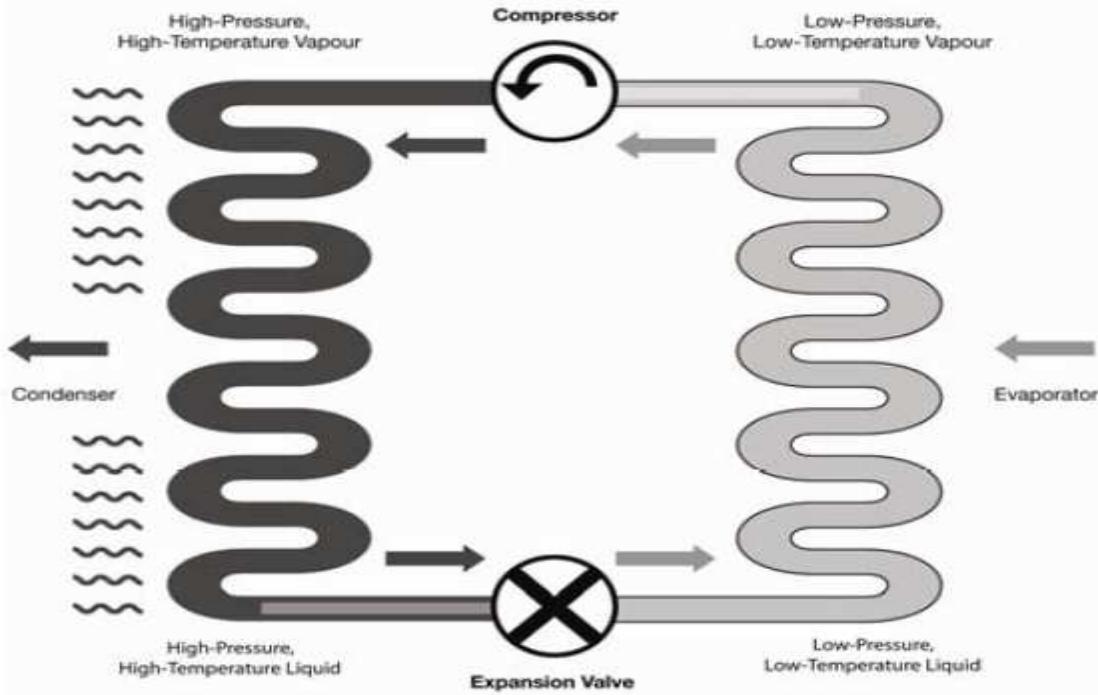


Figure 9: Heat pump cycle based on vapour compression (CEA Technologies)

Heat pump typically delivers or extracts much more heat than the work input provided to it. A heat pump can have coefficient of performance of 3.5 and higher depending of the supply water temperature (heat source), return air temperature (heat sink), water flow rate and air flow rate. This means that if the heat pump uses 1 kW of electricity, it can deliver 3.5 kW of heating or higher. Heat pump energy performance for heating can be calculated as:

$$\text{COP} = \text{Heat Delivered (kW)} / \text{Electrical Energy Input (kW)} \quad (\text{Equation 1})$$

$$\text{Or, COP} = \text{Heating Energy Delivered (Btu/h)} / (\text{Energy input in Watts} \times 3.412 \text{ Btu/Watt-hour}) \quad (\text{Equation 2})$$

Heat pump efficiency for cooling can be shown as:

$$\text{Energy Efficiency Ratio (EER)} = \text{Cooling Capacity (Btu/h)} / \text{Energy input (watts)} \quad (\text{Equation 3})$$

$$\text{Cooling COP} = \text{Cooling EER} / 3.412 \text{ Btu/watt-hour} \quad (\text{Equation 4})$$

The higher the COP and EER are, the more efficient the heat pump is. Calculation of the COP

and EER only considers the energy consumed by the compressor; energy consumed by fans or pumps are not included.

From the definition of COP it is seen that the heat extracted for cooling is higher than the heat rejected for heating, as the Heating Energy Delivered includes the energy introduced by the compressor.

For the Heating Operation:

$$\text{COP}_{\text{heat}} = Q_{h(\text{out})}/W_h \quad (\text{Equation 5})$$

$$\text{COP}_{\text{heat}} = (Q_{h(\text{in})} + W_h)/W_h \quad (\text{Equation 6})$$

$$Q_{h(\text{in})} = \text{COP}_{\text{heat}} \cdot W_h - W_h \quad (\text{Equation 7})$$

COP_{heat} is the coefficient of performance of the heat pumps during the heating operation; it can also be explained as the heat pumps' efficiency of adding heat to the space

$Q_{h(\text{out})}$ is the heat added to the space by the heat pumps; also known as the heating load

$Q_{h(\text{in})}$ is the heat extracted from the common water loop by the heat pumps

W_h is the work done by the heat pump compressor, defined as the heating-end-use energy (kWh) in the hourly report.

Similarly for the Cooling Operation:

$$\text{COP}_{\text{cool}} = Q_{c(\text{in})}/W_c \quad (\text{Equation 8})$$

$$\text{COP}_{\text{cool}} = (Q_{c(\text{out})} - W_c)/W_c \quad (\text{Equation 9})$$

$$Q_{c(\text{out})} = \text{COP}_{\text{cool}} \cdot W_c + W_c \quad (\text{Equation 10})$$

COP_{cool} is the coefficient of performance of the heat pumps during the cooling operation. It can also be explained as the efficiency of the heat pump to remove heat from the space.

$Q_{c(\text{out})}$ is the heat added to the common water loop by the heat pumps

$Q_{c(\text{in})}$ is the heat extracted from space by the heat pumps; also known as the space cooling load

W_c is the work done by the heat pump compressor, defined as the cooling-end-use energy (kWh) in the hourly report.

From Equation 1 to 10, it is evident that for the het balancing and heat re-use system to work; the daily total cooling load can be less than the daily total heat load of the space. This can also be

formulated as:

$$Q_{c(in)} \geq Q_{h(out)} - W_c - W_h \quad (\text{Equation 11})$$

Heat Pump Efficiency:

Heat pump efficiency will play a major role in determining how the zone loads should be balanced. Three major brands of heat pumps have been analyzed to examine the performance efficiency. Different sizes and associated energy performances are shown in Table 2, Table 3 and Table 4.

Table 2: Affinity Series water source heat pumps performance (Daikin McQuay, 2007)

Enfinity Horizontal ISO Performance Data – Water Loop

Water Loop Performance Data per ISO Standard 13256-1.

UNIT SIZE	AIRFLOW		WATERFLOW		VOLTAGE	COOLING				HEATING			
	CFM	L/S	GPM	L/S		BTU/HR	WATTS	EER	COP	BTU/HR	WATTS	COP	
007	300	142	2.1	0.14	115-1-60	8028	682	11.8	3.5	10715	744	4.2	
					208/230-1-60								
009	300	142	2.3	0.14	115-1-60	8813	681	12.9	3.8	11769	745	4.6	
					208/230-1-60								
012	400	189	3.0	0.19	115-1-60	12941	1021	12.7	3.7	15804	1080	4.3	
					208/230-1-60								
					265-1-60								
					230-1-50								
019	630	297	5.3	0.33	208/230-1-60	21000	6149	14.9	4.4	23600	6910	4.8	
					265-1-60								
024	800	378	6.2	0.39	208/230-1-60	24700	7232	14.4	4.2	28400	8316	4.7	
					265-1-60								
					208/230-3-60								
					460-3-60								
030	1000	472	7.6	0.48	208/230-1-60	30400	8901	15.3	4.5	36200	10600	5.0	
					265-1-60								
					208/230-3-60								
					460-3-60								
036	1200	566	9.0	0.57	208/230-1-60	35800	10483	15.2	4.5	42500	12444	4.9	
					208/230-3-60								
					460-3-60								
					575-60-3								
042	1400	661	10.7	0.68	208/230-1-60	43000	12591	15.0	4.4	50700	14845	5.0	
					208/230-3-60								
					460-3-60								
					575-60-3								
048	1600	755	12.3	0.78	208/230-1-60	48400	14172	14.1	4.1	57100	16719	4.7	
					208/230-3-60								
					460-3-60								
					575-60-3								
060	2000	944	15.2	0.96	208/230-1-60	59500	17422	14.6	4.3	69400	20321	4.9	
					208/230-3-60								
					460-3-60								
					575-60-3								

Notes:

EER = Energy Efficiency Ratio COP = Coefficient of Performance L/s = Liters per second

Cooling capacity is based on 80.6°F db, 66.2°F wb (27/19°C) entering air temperature and 86°F (30°C) entering water temperature.
Heating capacity is based on 68°F (20°C) entering air temperature and 68°F (20°C) entering water temperature.

For the McQuay water source heat pump units, cooling COP ranges from 3.5 to 4.3, which implicates that if the compressor consumes 1 kW of electrical energy, the heat pump will extract 3.5 to 4.3 kW of heat from the zones that are in need of cooling. However, heat pumps operating in cooling mode will reject 4.5 to 5.3 kW of heat into the return water loop. Heating the COP ranges from 4.2 to 4.9, which implicates that if the compressor introduces 1 kW of energy, 4.2 to 4.9 kW of heat will be provided to the zones that require heating. During the heating process, water source heat pumps will extract 3.2 to 3.9 kW of heat energy from the supply water.

Table 3: Tranquility series water source heat pump performance (ClimateMaster, 2014)

Model	Water Loop Heat Pump				Ground Water Heat Pump			
	Cooling 86°F		Heating 68°F		Cooling 59°F		Heating 50°F	
	Capacity Btuh	EER Btuh/W	Capacity Btuh	COP	Capacity Btuh	EER Btuh/W	Capacity Btuh	COP
TE026 Part	19,200	19.8	23,600	7.0	22,000	34.1	19,000	5.8
TE026 Full	25,000	17.4	31,400	6.0	28,500	26.4	25,800	5.3
TE038 Part	27,400	20.1	32,600	6.5	30,700	34.4	27,300	5.1
TE038 Full	37,700	17.9	45,700	5.8	42,100	26.1	37,900	5.2
TE049 Part	36,300	18.8	42,200	6.1	41,800	32.9	34,800	5.0
TE049 Full	48,600	16.8	56,700	5.1	55,000	25.3	46,800	4.6
TE064 Part	46,300	18.7	54,700	6.0	53,100	32.4	44,000	5.0
TE064 Full	61,500	16.2	77,400	5.4	71,500	24.4	63,200	4.8
TE072 Part	53,000	16.8	64,600	5.2	60,800	28.6	53,200	4.5
TE072 Full	68,300	15.1	85,300	4.8	77,700	22.5	71,400	4.4

Cooling capacities based upon 80.6°F DB, 66.2°F WB entering air temperature
 Heating capacities based upon 68°F DB, 59°F WB entering air temperature

Table 3 shows performance of the ClimateMaster Tranquility-30 series water source heat pumps. This variable speed heat pump's capacity can vary between 1.5 ton to 6 ton. At full load, cooling COP can range from 4.4 to 5.1, which means for 1 kW of electrical energy consumed by compressor, the heat pump can remove 4.4 to 5.1 kW of heat from the zones required cooling, and reject the heat to the water loop. At full load, heating COP ranges from 4.8 to 6.0, which implies that for 1 kW of electrical energy consumed by the compressor, 4.8 to 6.0 kW of heat is provided to the space requiring heat; therefore 3.8 to 5.0 kW of heat is extracted from the water loop. Since the cooling load in the core zone is weather independent, the peak cooling load will

persist throughout the year. The peak heating load will likely happen during the winter days in January. As this project aims to have a balanced load during the peak heating, only full load efficiencies will be used for modelling and analysis.

Table 4: Axiom series water-source heat pumps performance (Trane Inc., 2013)

Horizontal EXH ARI-ISO performance														
Model	Rated water flow (GPM)	Rated airflow (SCFM)	Cooling capacity WLHP (BTUH)	Heating capacity WLHP (BTUH)	COP WLHP	Cooling capacity GWHP (BTUH)	Heating capacity GWHP (BTUH)	COP GWHP	Cooling capacity GLHP (BTUH)	Heating capacity GLHP (BTUH)	EER GLHP	COP GLHP		
EXHF006	1.8	215	7600	15.0	8800	4.9	8800	23.4	7600	4.4	8000	17.4	5000	3.4
EXHF009	2.1	285	9000	14.9	11100	5.4	10000	21.9	9100	4.7	9400	16.9	7000	3.8
EXHF012	2.8	380	11900	15.5	14600	5.2	14000	26.6	11900	4.5	12700	18.8	9000	3.6
EXHF015	3.5	475	15100	15.3	18300	4.8	17500	25.0	15200	4.2	15900	17.9	11300	3.4
EXHF018	4.2	570	19300	16.7	23300	5.1	20600	25.0	19100	4.5	19000	18.7	14200	3.6
EXHF024	5.6	760	23800	16.0	27700	4.8	25900	23.8	24100	4.5	24700	18.0	18800	3.6
EXHF030	7.0	950	30500	16.8	36200	5.4	33700	24.3	29600	4.9	31600	19.7	22700	3.7
EXHF036	8.4	1140	35200	17.0	44400	5.4	39700	25.8	36500	4.8	36700	19.1	28200	3.8
EXHF042	9.8	1330	42500	16.8	52400	5.3	45800	23.3	43100	4.7	43700	18.5	31200	3.9
EXHF048	11.2	1520	47800	16.1	60000	5.3	52000	22.8	48800	4.7	49100	17.7	38000	3.9
EXHF060	14.0	1700	58600	15.0	77800	4.9	64700	22.0	64100	4.4	61400	17.1	50400	3.8
EXHF070	15.4	2090	66600	15.5	82100	4.5	70900	21.1	68900	4.1	68500	16.9	52600	3.5

Notes: Rated in accordance with ISO Standard 13256-1: 1998 (Water Loop Heat Pumps). EWT, 80.6°F DB/66.2°F WB EAT in cooling and 68°F EWT, 68°F DB/59°F WB EAT in heating. Certified conditions are 86°F

Table 4 shows performance of the Trane Axiom series water source heat pumps. This high efficiency heat pump's capacity can vary between 0.5 ton to 6 ton. At full load, cooling COP can range from 4.4 to 5.0, which means for 1 kW of electrical energy consumed by compressor, the heat pump can remove 4.4 to 5.0 kW of heat from the zones required cooling, and reject the heat to the water loop. At full load, heating COP ranges from 4.5 to 5.4, which implicates that for 1 kW of electrical energy consumed by the compressor, 4.5 to 5.4 kW of heat is provided to the space requiring heat; therefore 3.5 to 4.4 kW of heat is extracted from the water loop.

From Table 2 to Table 4, it can be inferred that in order to have a balanced load condition, the proposed net zero building should have a higher cooling load than the heating load in winter peak conditions. Once the peak condition is balanced, ways of offsetting imbalance during the off-peak hours will be investigated and analyzed.

1.6 Energy Efficiency Requirement for Internal Closed Loop Heat Pumps (NRCan, 2016)

Natural Resource Canada has published the minimum efficiency requirements (table 5) for heat pumps used in the distributed common loop heat pumps in an article titled “Internal water loop heat-pumps”. The energy efficiency rating applies to water source heat pump not exceeding 40 kW (135,000 Btu) in heating/cooling as per the rating standard of CAN/CSA-C13256-1.

Table 5: Minimum COP requirements for heat pumps

PRODUCT CLASS	MINIMUM COP	
	Cooling COP _c	Heating COP _h
November 2006		
Cooling capacity < 5 kW	≥ 3.28 with 30°C inlet water	≥ 4.2 with 20°C inlet water
Cooling capacity ≥ 5 kW and ≤ 40 kW	≥ 3.52 with 30°C inlet water	≥ 4.2 with 20°C inlet water

1.7 ASHRAE 90.1 Standards (ASHRAE, 2013)

The purpose of ASHRAE 90.1 is to establish the minimum energy efficiency requirement of buildings other than low rise residential buildings, for:

- Design, construction and a plant for operations and maintenance, and
- Utilization of on site, renewable energy sources.

It sets a minimum energy efficiency standard for:

- New buildings and their systems.
- New portion of the buildings and their systems.
- New system and equipment in existing buildings.

The original Standard 90 was first published in 1975, and revised editions were published in 1980, 1989 and 1999 using the ANSI and ASHRAE periodic maintenance procedures.

Prescriptive requirements of ASHRAE 90.1 2013 related to the building envelope, HVAC, DHW, power, lighting and auxiliary equipment will be used to design the base case commercial building.

Roof assembly maximum U-value = 0.032 Btu/h-ft².°F

Roof assembly minimum R-value = 30

Above grade wall maximum U-value = 0.080 Btu/hr.ft².°F

Above grade wall minimum R-value = 13.3

Slab-on-grade floors minimum R-value = R20 for 24 inch along the exterior cavity

Opaque door maximum U-value = 0.500 Btu/h-ft².°F

Vertical fenestration (0% to 40% of Wall) with non-metal framing, maximum U-value = 0.32 Btu/h-ft².°F

Vertical fenestration (0% to 40% of Wall) with non-metal framing, maximum solar heat gain coefficient (SHGC) = 0.40

Vertical fenestration (0% to 40% of Wall) with non-metal framing, minimum visible transmittance (VT) = 0.44

Skylight, 0% to 3% of Roof

Maximum U-value = 0.50 Btu/h-ft².°F

Max SHGC = 0.40

HVAC System Requirements:

Setback Control: Heating systems shall be equipped with controls configured to automatically

restart and temporarily operate the system as required to maintain zone temperature above and adjustable heating setpoint at least 10F below the occupied heating setpoint. Cooling systems shall be equipped with controls configured to automatically restart and temporarily operate the mechanical cooling system as required to maintain zone temperature below an adjustable cooling setpoint at least 5 °F above the occupied cooling setpoint or to prevent high humidity level.

Hydronic (water loop) Heat Pump Systems: Hydronic heat pumps connected to a common heat pump water loop with central devices for heat rejection (e.g. cooling tower) and heat addition (e.g. boiler) shall have the following:

Controls those are capable of providing a heat-pump water supply temperature dead band of at least 20 °F between initiation of heat rejection and heat addition by the central devices (e.g. tower and boiler).

Fan Efficiency: Fans shall have a fan efficiency grade of 67% or higher based on manufacturers' certified data, as defined by AMCA 205. The total efficiency of the fan at the design point of operation shall be within 15 percentage points of the maximum total efficiency of the fan.

Boiler Turndown: Boiler systems with design input of at least 1,000,000 Btu/h shall comply with the turn-down ratio specified in Table 6.5.4.1

The system turndown requirement shall be met through the use of multiple single-input boilers, one or more modulating boilers, or a combination of single-input and modulating boilers.

All boilers shall meet the minimum efficiency requirements in Table 6.7.1-6

Hydronic Variable Flow System: HVAC pumping systems having a total pump system power exceeding 10 hp that include control valves designed to modulate or step open and close as a function of load shall be designed for variable fluid flow and shall be capable of reducing pump flow rates to 50% or less of the design flow rate.

Hydronic heat pumps and water-cooled unitary air-conditioners having a total pump system power exceeding 5 hp shall have controls and/or devices (such as variable-speed control) that

will result in pump motor demand or no more than 30% of design wattage at 50% of design water flow.

Water source heat pump minimum cooling efficiency required at 86°F entering water temperature:

<17,000 Btu/h ; 12.2 EER

>=17,000Btu/h and <65,000 Btu/h; 13.0 EER

>=65,000 Btu/h and <135,000 Btu/h; 13.0EER

Heating mode minimum efficiency at 68 °F enter water temperature: 4.3 COP

Gas fired heating boiler minimum annual fuel usage efficiency (AFUE) = 80%

Minimum efficiency of propeller or axial fan cooling tower rated at 95 °F entering water, 85 °F leaving water and 75 °F entering wet bulb = 40.2 gpm/hp.

Electrically operated multi-split heat recover air-to-air variable flow applied heat pump cooling mode minimum efficiency:

>=65,000 Btu/h and <135,000 Btu/h: 10.8 EER and 12.1 IEER

1.8 eQuest Building Simulation (Nall and Crawley, 2011)

Building energy simulation programs have been in existence for about 18 years. Initially, they were commissioned by gas and electricity utility associations to influence designers in the selection of gas or electric systems. Subsequent development of programs was sponsored by the federal government with North Baltimore Local School Board (NBLSD) as a research tool and the U.S. Post Office programs a compliance tool for design guidelines. These federal efforts have culminated in the BLAST and DOE-2 programs available today. This project utilizes energy simulation software eQuest V3.65, which is a DOE-2 based building energy simulation wizard. eQuest combines the DOE-2 engine with a building creation wizard and an energy efficiency measure (EEM) wizard. The building creation wizard can be used to create a complete building using steps that take input in the following design aspects, which contribute to building energy consumptions:

- Architectural design.

- HVAC design and equipment.
- Building type and size.
- Floor plan layout.
- Construction material.
- Area usage and occupancy distribution.
- Lighting and internal equipment.

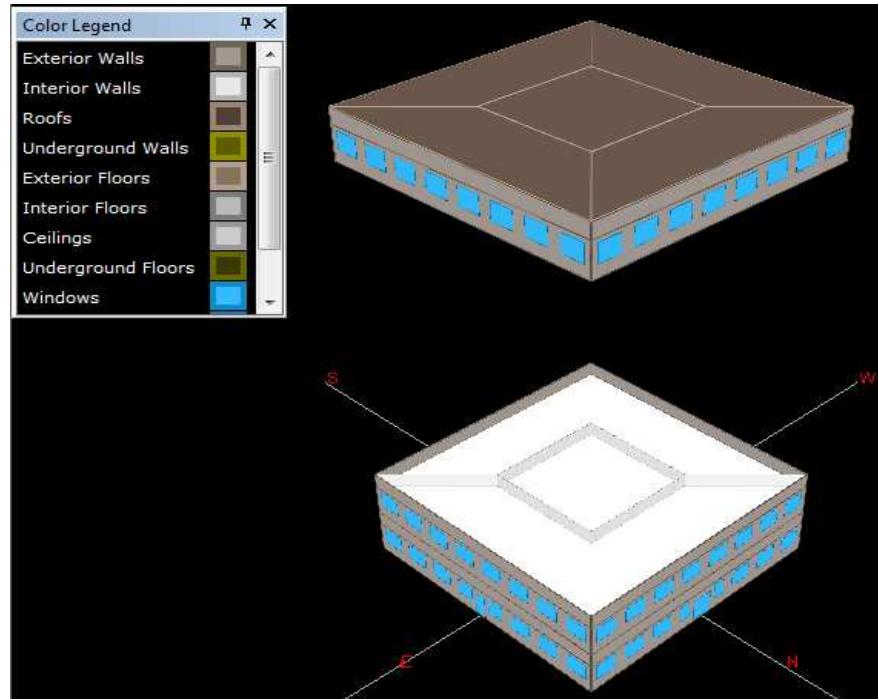


Figure 10: Sample base building model in eQuest

After compiling the complete building information, eQuest produces a detailed simulation of the building, heating and cooling load calculation and annual energy consumption of the building. eQuest performs hourly simulation of the building using local weather data for an entire year using the following information:

- Walls
- Windows
- Glass
- People
- Plug load

- Ventilation

The DOE engine simulates the performance of fans, pumps, chillers, boilers and other energy consuming equipment. Once a simulation is complete, eQuest produces graphic results of estimated monthly and yearly energy consumptions.

1.9 HVAC Zoning in eQuest (Hirsch & Associates, 2009)

The official eQuest tutorial published by Hirsch describes that HVAC zoning recognizes that the load profiles seen by different spaces in a building differ. It is suggested that areas with similar load profiles be grouped under the same thermostat control to improve comfort and save energy. The zone temperatures are effected by internal gains, solar gains, and envelope gains and losses. The following factors should be considered when creating zones in eQuest:

- Magnitude and schedule of internal loads
- Magnitude and schedule of solar gains
- Schedule of fan system operations
- Outside air temperature
- Intended efficiency measures
- One exterior zone per major orientation (12 to 18 ft deep)
- One internal zone per use schedule
- One zone each for special uses such as conference rooms, cafeterias etc.
- Separate ground and top floor zones.

1.10 Net Zero Energy Building (Duncan, 2009)

A Net Zero Energy Building (NZEB) must achieve an operating net zero energy demand, which means that the total energy consumed by building must be met by the energy produced within the site. The choice of building façade, mechanical systems and occupant behaviour has significant impact on the design of the NZEB. Envelop energy demands include sensible conduction and solar load, whereas infiltration contributes to latent and sensible gain/loss. Occupancy energy consumption involves sensible and latent heat gain due to occupants, lighting and equipment. Building system energy efficiency involves HVAC system efficiency, configuration and control strategies. The first step to design a net zero building is estimating the

building's energy demand by performing energy model, which predicts building load and energy consumption. Initially the building is modelled to represent ASHRAE 90.1-2010 minimum energy efficiency requirement, which recommends energy densities and schedules for occupancy, lighting and equipment/plug load gains. The base case is then improved and simulated for better energy performance of the building. For a large office, the gains to a space are dominated by windows solar transmittance and thermal conductance, occupant, lighting and equipment load. In winter, heat is lost through the walls and windows by conduction, whereas heat is gained due to solar transmittance through the windows. Proper solar shading practice can reduce heat gain in summer and increase heat gain in winter. High performance façade significantly reduces solar gain and infiltration load. A large portion of the load comes from the plug and lighting load during the cooling season. These can be addressed by optimizing daylight penetration, internal lighting controls and use of energy efficiency appliances.

2. Literature Review

A set of publications and case studies have been reviewed, which will be used as the guiding principle for creating a methodology of the design of a net zero energy building, heated and conditioned by common loop water source heat pumps systems.

2.1 Simulation Overview (Clarke, 2001)

In the book “Energy Simulation in Building Design”, Clarke has presented overview, method and validation technique of energy simulation. Clarke presented that buildings typically account for around 50% of the total energy consumption in a developed country and similar portion of the carbon dioxide emission. Building energy simulation approach is able to address all aspects of a building’s life cycle and thereby help designers to strike a balance between energy use, indoor comfort and local/global impact. A brief summary of simulation overview and thermo physical factors of a building have been extracted from Clarke’s book.

A building interacts in a dynamic manner to dictate comfort levels and energy demands. Components that contribute to the load and energy of a building are constructional elements, room contents, glazing systems, occupancy, use, plant system, HVAC distribution system, lighting and internal equipment. Our focus on building energy analysis here is mainly based on energy consumed by building heating, ventilating and air-conditioning (HVAC) system, which is linked to building heat transfer processes that are highly inter-related. Therefore it is necessary to apply simultaneous solution techniques if the performance is to be both accurate and preserve the spatial and temporal integrity of the modelled system. These simultaneous heat transfer processes involve a large number of complex equations combined to present heat transfer and energy consumption process of a complex building system. A simulation process can be utilized throughout the design process from the early concept stage through the detailed design. It helps owners and designer to make the right decision in terms of their energy focus and financial feasibility. There are a number of building simulation programs; however it is more efficient to use a single program throughout the design process than use a progression of tools. This will help to use theoretical discontinuities and pernicious assumptions. Simulation tools can be used at multiple stages of the design; each simulation can optimize a single aspect of the building

design. It is possible to use a simulation program to determine the optimum combination of zoning and constructional scheme that will provide a climate responsive solution and minimize the need for a mechanical plant. Some simulation might focus on the choice of construction materials and their relative positioning within multi-layered construction so that good temperature and load leveling is attained. Simulation can also be used to perform optimum daylight capture and shading strategies in order to utilize sunlight to gain heat during colder season, while avoid solar heat gain during the summer/cooling months. This strategy may involve optimized sizing and material selection for gaining solar heat during the winter, while reducing conductive heat loss. In the summer months, the simulation will aim for minimizing both solar heat gain as well as conductive heat transfer between the ambient and the indoor environment; a shading strategy can be effectively used for such scenario. In both summer and winter cases, optimum daylight capture can reduce use of lighting in the perimeter zones.

Once the physical characteristics of a building are decided upon for the anticipated scenarios, different control strategies can be simulated for energy usage reduction while maintaining desired indoor environment. Basic control strategies will help to decide on the start stop control of HVAC systems, appropriate temperature setback during unoccupied hours, location of sensors and interrelation of thermal and visual comfort variables. To further stress on these scenarios, one can design and simulate HVAC system controls in terms of how the system will turn on and off on demand or whether the HVAC equipment will just modulate according to the heating/cooling demand or how should the equipment respond from the sequence of operation perspective. Similarly sensors can be integrated in the model to test benefits of occupancy sensor driven lighting control, day light control to optimize natural light and solar heat gain/heat loss and HVAC temperature setbacks.

Building energy consumption by HVAC system is directly influenced by various heat and mass transfer between the ambient and the indoor environment. A good simulation software should simultaneously process all energy transport paths, and the HVAC system, which maintains desired indoor environment by converting energy (electricity, natural gas etc.) into heating and cooling. Major factors influencing heat and cooling loads are briefly discussed here.

Conduction Loss/Gain: This can be defined as the heat transfer through the envelope of the building due to the temperature difference between the indoor and the outside. Building envelop consists of the walls, windows, doors, roof and the floor which is in contact with the earth. The rate at which heat travels through the building envelope is a deciding factor in the heating and cooling load of a building. The thermo physical properties influencing heating/cooling load are conductivity, k (Btu/ft. $^{\circ}$ F), density, ρ (lb/ft 3) and specific heat capacity, C_p (Btu/lb.F). By combining these three factors, overall thermal transmittance U (Btu/ft 2 .F) of the wall can be found. As the goal of this project is not to analyze the calculation methods of the heat loss/heat gain, it is only important to understand how the conductive heat loss takes place and using its knowledge to optimize envelope construction of the intended office building.

Surface Convection: Convection is the process of exchanging the heat flux between a surface and the adjacent air layer. In the case of the ambient, convection is wind induced and considered as forced convection, whereas in the indoor environment, convection is natural unless mechanical forced flow is used. In energy simulation it is normal practice to make use of time varying, but surface-averaged convection coefficient h_c (Btu/ft 2 . $^{\circ}$ F). Typically for external building surfaces, wind speed and direction data are available for some reference height. Convective heat loss and heat gain will be different with building shape, orientation and aspect ratio. Wind direction will cause higher convective heat loss/gain in certain perimeter areas than the other.

Internal Surface Long Wave Radiation: Long wave radiation is a function of the prevailing surface temperature, the surface emissivities, the extent to which the surfaces are in visual contact and the nature of the surface reflection. Generally windows with low emissive increase the reflection of longwave solar radiation and breaks inter surface heat exchange. Optimization of solar radiation will be experimented in order to balance thermal load of the building.

Shortwave Radiation: This is the solar energy gain which constitutes a significant portion of the cooling load and which can offset some of the heating load in winter. Proper treatment of the solar radiation can help reduce the heating load in the perimeter zones. When solar energy impinges on any glazing, it is partially reflected and partially transmitted into the indoor space. The transmitted beam strikes internal surfaces where it goes through absorption, reflection and

transmission. The heat flux is then stored and lagged in the internal surfaces, thus giving rise to the solar heat gain. The thermo physical properties of interest include shortwave absorptive for opaque elements and absorptive, transmissivity and reflectivity for transparent elements.

Shading and Insolation: The solar energy incident on a building is influenced by shading as caused by parts of itself, surrounding buildings, façade features and natural obstructions such as trees. Shading and insolation are therefore function of solar position and target geometry. The design optimization strategy is to use design parameters such as orientation, shape and obstruction geometry to so modify the shading/insolation patterns that environmental performance is improved without recourse to mechanical intervention.

2.2 Building Envelop Design for Energy Balance (Chwieduk, 2014)

Solar Thermal Efficiency of Building Envelope:

A number of recommendations were made concerning shaping of building envelopes in high altitude countries based on simulation by Sodha. Since the principle objective of this project is to balance load during winter and shoulder seasons, recommendations are provided to optimize solar gain in those two periods.

In the winter, because of poor solar irradiation, recommendations are very strict.

- The façade should be opened for solar radiation from the south. Envelope of a building must not be shaded by elements of a building architecture or surrounding objects. If any extended curved of the south façade is used, the glazed part should have azimuth angles from -30° to $+30^\circ$.
- It is recommended to use envelope elements with high tilt angle, sloped roofs with tilt in ranges from 50 to 70. Horizontal surfaces and surfaces with small tilt angle should be avoided.
- The main façade in the south should be large grazed surface.
- Innovative materials can be proposed including smart windows with transmittivity for solar radiation depending on the angle of the inclined solar radiation, and length of the radiation wave.
- Northern parts of the building envelope are the least exposed to solar radiation.

Therefore storages, depots, technical facilities should be placed in the north most rooms. The number of windows should be minimized.

- The eastern parts of the building can be used for offices and meeting rooms, which require good daylight access during the morning hours. In summer time, these rooms will be much less heated than the ones located at the south and the west side of the building.

Direct solar gain can reduce heating load in the winter season. A direct solar gain is utilized by the room as it enters directly through windows and doors. Solar radiation passes through windows glazing, which acts as a transparent cover of the solar energy receiver (the room). Depending of the solar radiation absorptance of the surfaces of the internal walls, solar radiation is absorbed and stored for a period. The stored heat is normally exchanged between medial of different temperatures, thus the temperature within the room increases. Enlarging glazing area in the sides more exposed to solar radiation can add radiance heat to the perimeter area of the building. During the winter, large glazing also causes heat loss to the ambient. In the case of the modern windows with compact glass panes, more heat is transferred through the framing than the through the glazing, thus the frame area needs to be reduced. Large glazing can cause the indoor temperature change considerably and sharply through both heat gain and heat loss. In winter, transmittance of the solar gain should be as high as possible, while the windows should have high thermal resistance to prevent heat to be lost to the ambient. Heat insulation characteristics of the windows not only depend on the material of the glazing, but also on the entire window design, including the number of glass layers, assembly method, material and thermal performance of framing and gap between panes. Heat transfer through the central part of the window panes are relatively low, but heat transfer is significant at the edges where the panes make contact with the frame. Since metal spacers act as heat transfer medium, spacers with high insulation value should be used. Once recommendation for design window is the so-called solar glass with low iron content which gives the window high transmittance for solar radiation and low transmittance for thermal radiation. Electromagnetic glazing has been recommended in the book titled Solar Energy in Buildings. There are many different types of windows with different optical properties, and therefore different coefficients of solar radiation gains. Commonly double-glazed windows and triple-glazed windows are used. In modern compact windows, gaps between panes are filled with noble gas like argon and krypton. Different materials low

conductance such as wood or plastics with chambers filled with air or insulation can be used for framing.

Thermal resistance of a glazing is the sum of all the elementary resistance such as external thermal resistance, thermal resistance of the glazing and the internal thermal resistance. Thermal resistance of a double or triple pane window with air gaps depends on the intensity of the heat transfer phenomena of the glass material and the gap. In order to reduce heat exchange through thermal radiation, low-emission coating on the inner glass pane surfaces are used. Convective heat loss can be reduced by using proper gap between the glass panes and filling the gap with a noble gas or even creating vacuum gap. It is important to improve thermal insulating characteristics of windows. Apply low emissivity coating on the internal surface of the inner glass pane, increases thermal resistance of the double-glazed windows more than twofold. Filling the air gap between panes with noble gas reduces convective heat transfer because noble gases have fewer particles than air. In an old standard double-glazed window with an air-filled gap, the heat transfer coefficient during winter is $0.504 \text{ Btu/h-ft}^2\text{.}^\circ\text{F}$ ($2.86 \text{ W/m}^2\text{.K}$) and during summer $0.595 \text{ Btu/h-ft}^2\text{.}^\circ\text{F}$ ($3.38 \text{ W/m}^2\text{.K}$). The solar heat gain coefficient SHGC is 0.76. A double glazing with low-emissivity coating on the inner surface of the inner pane ($\epsilon=0.08$) and an argon-filled gap, the heat transfer coefficient is $0.137 \text{ Btu/h-ft}^2\text{.}^\circ\text{F}$ ($0.78 \text{ W/m}^2\text{.K}$) for winter and $0.157 \text{ Btu/h-ft}^2\text{.}^\circ\text{F}$ ($0.89 \text{ W/m}^2\text{.K}$) for summer. The Solar Heat Gain coefficient is 0.45.

Energy Balance of a Building:

Any building is influenced by its external surroundings, especially climatic conditions including solar radiation. The thermal interaction with the surrounding is influenced by building architectural and structural designs, which should increase solar radiation in winter and reduce solar gain in summer. This also requires using transparent elements of building façade of high transmittance as well as opaque elements of high absorptance for solar gain in winter.

The energy balance of a building is influenced by heat flows through its envelope, air flow through infiltration through the building envelope, air flow through ventilation and heat gain from internal heat sources. Due to the heat loss/gain factors changing with time, the internal temperature also change; the requirement for heat generation from an external source also change. Considering the heat flow into and out of the building, and the internal heat gain, the following is the expression of a building energy balance:

$$\rho c V \frac{dT_{in}}{dt} = \sum \dot{Q}_{in}(t) - \sum \dot{Q}_{out}(t) + \sum \dot{Q}_{qv}(t) \quad (\text{Equation 12})$$

where:

$\sum \dot{Q}_{in}(t)$ = the sum of energy fluxes flowing into the interior through elements of a building envelope (W);

$\sum \dot{Q}_{out}(t)$ = the sum of heat fluxes flowing out of the interior through elements of a building envelope (W);

$\sum \dot{Q}_{qv}$ = the sum of internal heat sources in a building (room) (W);

$T_{in}(t)$ = the air temperature inside a building (room) (K);

V = the air volume inside a building (m^3).

Energy balance including solar radiation flux will be the following:

$$(\rho c V) \frac{dT_{in}}{dt} = \dot{Q}_{in}(t) + \dot{Q}_h(t) + \dot{Q}_{sol}(t) - U_t(t) A_t (T_{in}(t) - T_a(t)) - \dot{Q}_{ven}(t) \quad (\text{Eq 13})$$

Here Q_{in} is internal heat gains, Q_{sol} is solar radiation gains, Q_h is heat flow supplied by the heating system in the building, Q_{ven} is the heat requirement to temper the ventilation air depending on the outdoor temperature and U_t is the heat transfer coefficient for all the envelope elements and their surfaces.

If the entire building is heated at a given time and the temperature is maintained constant, then the whole building is considered as one temperature zone. However, due to different exposure level to sun and different internal gains, different areas of the building have different heating/cooling demand; thus applying several temperature zones is adopted depending on the location and function of different rooms. Heat fluxes through different envelope elements characterized by specific thermal resistance coefficients, are exchanged between the building's interior of a certain air temperature and its exterior of ambient air, the sky temperature, and ground temperature variable in time. Internal heat sources are people (approximate heat output 50-100W/person depending on activity) appliances, devices, light sources and equipment. In some cases heat provided by the internal source may be high enough, that the interior zone may not have any heating load, and sometime cooling might be required. Figure 11 shows interaction between a building and its surroundings.

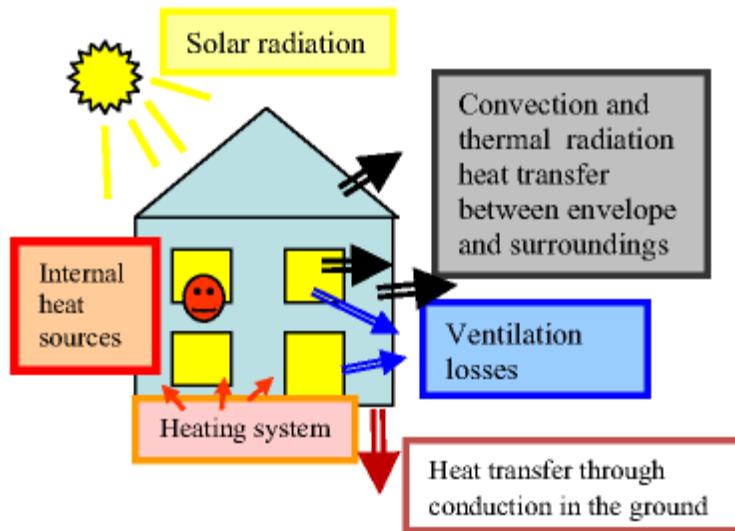


Figure 11: Energy transfer between a building and its surroundings (Chwieduk, 2014)

To minimize heat loss/gain, heat stored inside a building should stay inside as long as possible by using envelope elements of high thermal capacity, which gives an element the ability to store large amount of heat. Heat storage capacity is related to high thermal mass, volume, density and specific heat.

2.3 Net Zero Energy Building Design

Net Zero Design and Energy Basics: In the book titled *Net Zero Energy Design*, by Thomas Hootmat, the relationship between building architectural design and energy used has been emphasized. Hootman mentions that energy and architecture have always been intertwined. Architecture has always been formed by energy; it has been used to both mediate and harness the energy of the world. Hootman also explores work by Luis Fernandez-Galiano, who emphasizes on the importance of energy in architectural history. He refers to two fundamental interactions of energy and architecture; “regulation of free energy through construction” and “exploitation of accumulated energy through combustion”. Net zero energy design offers architects an opportunity to reengage in one of the fundamentals of architectural design, which combines the rigors of building science and the expression of the purpose and meaning of energy in architecture (Hootman, 2013).

Climate condition dictates the heating and cooling loads at the building envelope. In severe

climate like Canadian weather, thermal energy transfer between indoor environment of a building and the ambient can account for a large portion of the overall energy use of a building. Due to being mainly cold & dry and having heating-degree day (HDD) measured between $7200 < \text{HDD}(65^{\circ}\text{F}) < 9000$, Toronto is designated as climate zone **6B** by ASHRAE. Table 6 and Figure 12 demonstrate climate zone designation and energy use intensity (EUI) in commercial buildings.

Table 6: Climate zone definition (Hootman, 2013)

Zone No.	Climate Zone Type	Degree-days Criteria
1A	Very Hot-Humid	$9000 < \text{CDD}50^{\circ}\text{F}$
1B	Very Hot-Dry	$9000 < \text{CDD}50^{\circ}\text{F}$
2A	Hot-Humid	$6300 < \text{CDD}50^{\circ}\text{F} \leq 9000$
2B	Hot-Dry	$6300 < \text{CDD}50^{\circ}\text{F} \leq 9000$
3A	Warm-Humid	$4500 < \text{CDD}50^{\circ}\text{F} \leq 6300$
3B	Warm-Dry	$4500 < \text{CDD}50^{\circ}\text{F} \leq 6300$
3C	Warm-Marine	$\text{HDD}65^{\circ}\text{F} \leq 3600$
4A	Mixed-Humid	$\text{CDD}50^{\circ}\text{F} \leq 4500 \text{ and } \text{HDD}65^{\circ}\text{F} \leq 5400$
4B	Mixed-Dry	$\text{CDD}50^{\circ}\text{F} \leq 4500 \text{ and } \text{HDD}65^{\circ}\text{F} \leq 5400$
4C	Mixed-Marine	$3600 < \text{HDD}65^{\circ}\text{F} \leq 5400$
5	Cool-Humid	$5400 < \text{HDD}65^{\circ}\text{F} \leq 7200$
5B	Cool-Dry	$5400 < \text{HDD}65^{\circ}\text{F} \leq 7200$
5C	Cool-Marine	$5400 < \text{HDD}65^{\circ}\text{F} \leq 7200$
6A	Cold-Humid	$7200 < \text{HDD}65^{\circ}\text{F} \leq 9000$
6B	Cold-Dry	$7200 < \text{HDD}65^{\circ}\text{F} \leq 9000$
7	Very Cold	$9000 < \text{HDD}65^{\circ}\text{F} \leq 12600$
8	Subarctic	$12600 < \text{HDD}65^{\circ}\text{F}$

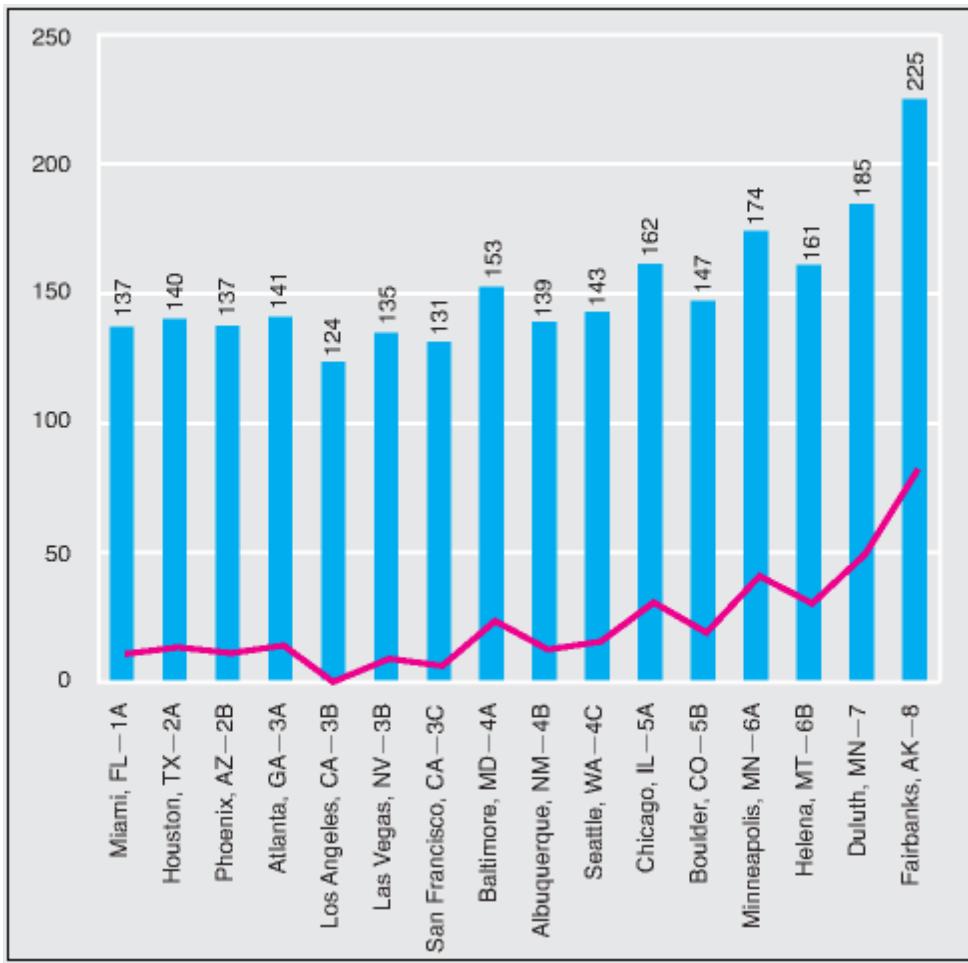


Figure 12: Annual Energy Use Intensity (kBtu/ft²/year) of commercial buildings in different zones based on average of 16 commercial building types (Hootman, 2013)

Figure 13 shows energy use intensity of commercial and institutional buildings by activity type in Canada.

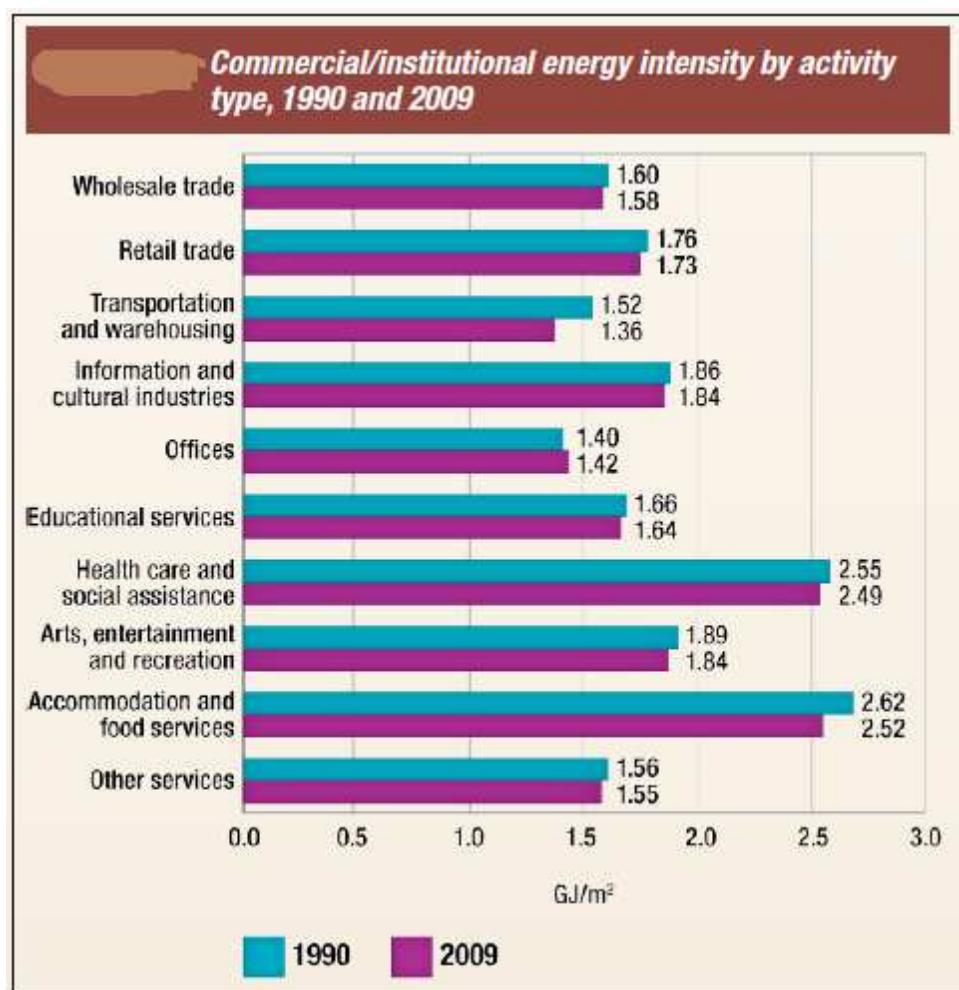


Figure 13: Commercial/institutional building energy intensity by activity type (NRCan, 2011)

The first step in establishing an energy target is setting a baseline for the design of a new building. A common energy standard is ASHRAE 90.1 “Energy Standard for Buildings except Low-rise Residential Buildings”, which establishes a minimum code performance standard for the specific building under construction (Hootman, 2013). The baseline modeling simulation of a building includes building parameters such as insulation levels, mechanical systems and building orientations. Once energy use baseline is developed, the next step is to figure out what contributes to the energy use in a building. Most commercial buildings have similar set of energy end uses. Most common end uses in the commercial buildings are:

- Interior and exterior lighting
- Space heating and cooling
- Ventilation

- Water heating
- Equipment (including office equipment)
- Cooking
- Refrigeration

A substantial portion of the building energy use is dedicated to the important function of thermal comfort. Passive architectural design and efficient building systems have dramatic impact on the thermal comfort and energy use. Many design options have been outlined by Hootman for a net zero building to meet energy target; however options related to the building geometry, envelope design, zoning and HVAC system design are focused in this project.

Building orientation is one of the most fundamentally important decisions for most net zero energy buildings, because passive strategies rely on access and utilization of the climate. From the climate perspective, orientation needs to respond to both sun and wind. Wind is variable but trends can be predicted. The path of the sun is definitively known, which can be used for daylight, solar radiation control, solar access for on-site photovoltaic and solar thermal systems. In the northern hemisphere, the sun follows a range of seasonal paths from the east to west in the southern sky. The summer has the highest sun angles, and the winter has the lowest.

Thermal zoning within a building refers to the strategic arrangement of spaces to take advantage of the thermal synergies and qualities of spaces, and their relationship to other spaces. There are two basic approaches to planning for thermal zones. The first is to consider the thermal requirements of a space in relation to the exterior. The second is to consider the thermal requirements to a space in relation to other spaces. From the activity type, identify the desired thermal condition of each space. Also identify the thermal loads of the space, based on use. From the climate analysis, identify the seasonal temperature ranges and solar radiation. These thermal conditions can be studied to determine optimal thermal zoning, to help reduce thermal transfer, create thermal buffers, and allow beneficial thermal transfer or storage. Some spaces have high internal heat gains, such as computer server rooms, data centres, mechanical rooms, and commercial kitchens. These high heat gain rooms can be located in the north perimeter for passive cooling, or can be source of heat for other areas having heating load. The heat can also be stored in an appropriate thermal storage space designed in the room. A thermal storage space is most effective when it is a remote thermal mass zone that is unoccupied and can store heat(in winter) for an extended period for use in other areas of the building and at various times.

2.4 Effect of Building Aspect Ratio on Energy Efficiency (McKeen, P., and Fung, A., July 2014)

Phillip McKeen under the supervision of Dr. Alan Fung at Ryerson University performed building simulation of multi-unit residential buildings with the objective of determining the effect of aspect ratio on the energy efficiency of the buildings. Aspect ratio defines the envelope surface area through which heat is transferred between the atmosphere and indoor environment. Analysis revealed that changing the aspect ratio resulted in different surface area of envelopes for an equivalent floor area. Though the minimum surface area has been achieved by 1:1 aspect ratio, the desired aspect ratio has been obtained through the balance of heat loss and gain due to the presence of solar radiation on specific areas of the building at specific length of time. McKeen simulated a number of building using eQuest to determine a relationship between the building aspect ratio and energy efficiency. The simulation was also used to establish a relationship between building's orientation and energy efficiency.

Design parameters of the building were moderately above the ASHRAE 90.1 2007 requirements, and Toronto climate condition was used for simulation. Thirteen different aspect ratios were modeled with the longest sides first facing south and north, and then rotated 90° so that the longest sides can face east and west. It can be seen in Table 7 that though the total floor area and the percentage of glazing are kept constant, the wall surface area, glazing area and south facing surface area changed with the change of aspect ratio and orientation.

Table 7: Different aspect ratio for simulation geometry (McKeen and Fung, 2014)

		A	B	B90°	C	C90°	D	D90°	E	E90°	F	F90°	G	G90°
Building Profile:														
Aspect Ratio (X:Y)	1:1	1.3:1	1:1.3	1.5:1	1.5:1	2:1	1:2	2.7:1	1:2.7	3.2:1	1:3.2	4.2:1	1:4.2	
Dimensions X	24.5	28.0	21.4	30.0	20.0	35.0	17.1	40.0	15.0	44.0	13.6	50.0	12.0	(m)
Dimension Y	24.5	21.4	28.0	20.0	30.0	17.1	35.0	15.0	40.0	13.6	44.0	12.0	50.0	(m)
Wall Surface Area	2987	3011		3048		3176		3353		3511		3780		(m ²)
Glazing Area (% of exterior surface)	36%	36%		36%		36%		36%		36%		36%		-
Glazing Area	1075	1084		1097		1143		1207		1264		1361		(m ²)
South Facing Surface Area	747	853	652	914	610	1067	521	1219	457	1341	415	1524	366	(m ²)
South Facing Surface Area (% of exterior surface)	25%	28%	22%	30%	20%	34%	16%	36%	14%	38%	12%	40%	10%	-

For heating and cooling, all the buildings used four-pipe fan coil units with centrifugal hermetic chiller and natural gas boiler. The annual energy consumptions due to different aspect ratio are shown in Table 8.

Table 8: Annual energy consumption for different aspect ratio (McKeen and Fung, 2014)

Aspect Ratio (x:y)	1:4.2	1:3.2	1:2.7	1:2	1.5:1	1:1.3	1:1	1.3:1	1.5:1	2:1	2.7:1	3.2:1	4.2:1
Building Profile:	G90°θ	F90°θ	E90°θ	D90°θ	C90°θ	B90°θ	A	B	C	D	E	F	G
Toronto													
Cooling Consumption	116.9	111.5	104.1	99.9	96.0	93.6	92.9	91.9	91.0	90.5	89.4	91.3	91.1
	421.0	401.2	374.8	359.8	345.8	337.1	334.6	330.7	327.5	325.9	321.7	328.5	328.1
Heating Consumption	1428	1303	1230	1157	1087	1063	1056	1048	1054	1100	1143	1211	1308
REC	35.2%	23.4%	16.5%	9.6%	3.0%	0.7%	0.0%	-0.8%	-0.2%	4.1%	8.2%	14.7%	23.9%
Combined Energy Consumption	1849	1705	1604	1517	1433	1400	1391	1378	1381	1425	1464	1540	1636
REC	33.0%	22.6%	15.4%	9.1%	3.0%	0.7%	0.0%	-0.9%	-0.6%	2.5%	5.3%	10.7%	17.6%

It is noticed from the analysis that the most energy efficient aspect ratio are 1:1, 1.3:1 and 1.5:1. Further elongation of the building in the east-west or north-south direction results in abrupt increase in both heating and cooling energy consumption.

2.5 Design of Typical Water Source Heat Pump Systems

This part of the literature review will examine design criteria of typical water source heat-pump systems used in the commercial buildings. Careful examination of the existing designs may help to innovate ways of designing a two pipe distributive system, which will operate without any external heating or cooling equipment conventionally connected to the loop. The design guides have been developed by design professionals and leading equipment manufacturers.

2.5.1 Daikin McQuay Inc Design Guide

Water source heat pump design capitalizes on the diversity factor in heating and cooling load of any building. It is unrealistic to think that all the heat gain factors happening during the peak cooling hours in a large commercial building. Same thing can be said about the heating load. Load level in different zones can also vary. At a certain hour some zones may require higher

cooling and heating than others, while the latter zones may require higher cooling and heating at a different time of the day. Central heating and cooling systems have poor part-load efficiencies, and maintaining individual zone temperature is also proven difficult (McQuay Inc., 1999). With central heating and cooling systems it is common to supply both heated and cooled air in a single zone to maintain the required zone temperature. This concept can waste a lot of energy during part load condition, which happens during the most part of the year. Water source heat pumps provide the flexibility to have individual unit at each zone, operated by individual thermostat and providing either heating or cooling. Terminal water source heat pumps connected in one closed loop also allows efficient transfer of energy from the satisfied areas of the building to the areas lacking sufficient energy.

Water-source heat pump is a decentralized system that provides heating and cooling throughout the year using a two pipe system. The system circulates non-refrigerated water from which heat-pumps either extract heat for cooling or to which the heat pumps reject heat from the zones for cooling. This system achieves energy efficiency by transferring heat from the warm zones to the cold zones when they coexist. System is designed to maintain the loop temperature between 65 °F to 95 °F (18.3 °C to 35 °C) (McQuay Inc., 1999). In a conventional system supplemental heat adding equipment such as a condensing boiler and a heat rejection equipment such as a cooling tower is added in order to add heat at the lower end of the range and reject heat at the higher end of the range respectively. Figure 14 to Figure 17 show four possible configurations of water source heat pumps suggested by McQuay Inc. for different load conditions.

During hot weather with most or all units cooling, heat removed from the air is transferred to the water loop. An evaporative water cooler rejects the excess heat outdoors to maintain a maximum water temperature of approximately 90°F (32°C).

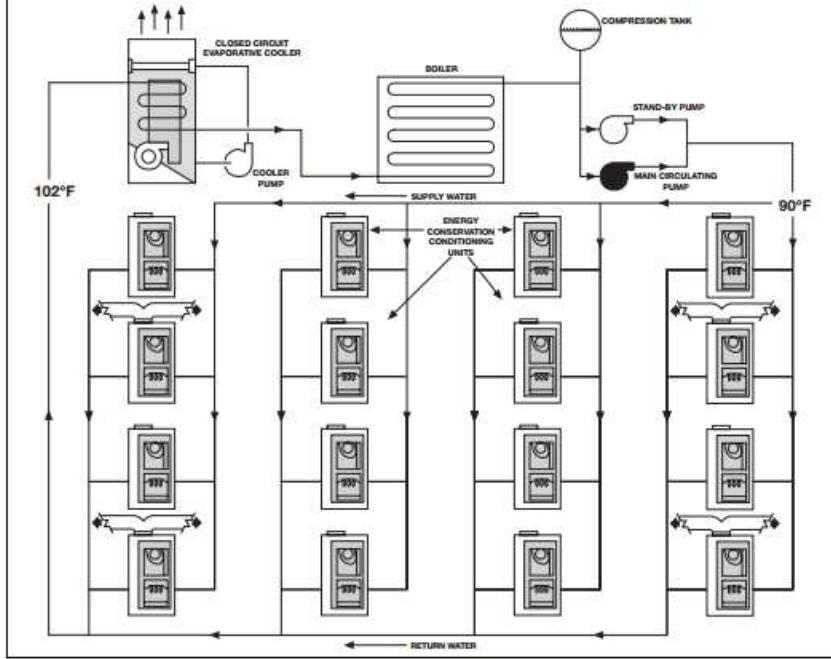


Figure 14: Configuration of conventional water-source heat pump system during cooling only operation (McQuay Inc., 1999)

Only in very cold weather with most or all units heating is it necessary to add heat to the water with a water heater. This is done when the temperature of the water loop falls to 64°F (18°C). The amount of this heat is reduced any time one or more units are operating on cooling. The central water heater is never larger than two-thirds the size required in other systems but is usually less because of diversity.

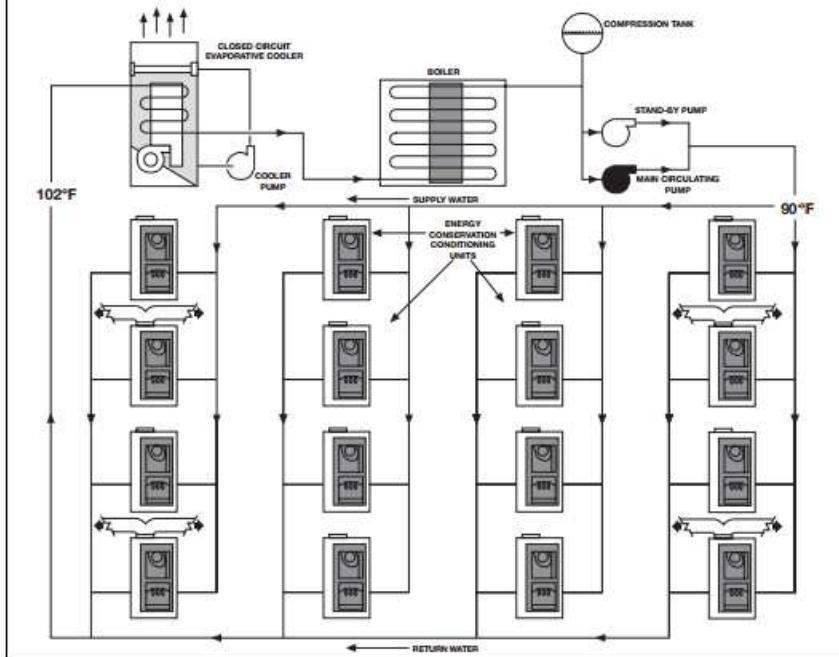


Figure 15: Configuration of conventional water-source heat pump system during mainly heating operation (McQuay Inc., 1999)

Applications such as office buildings with high heat gain from lights, people or equipment in interior areas may require cooling of the space year-round. Heat taken from those areas is rejected to the water loop providing enough heat for the building perimeter any time at least one-third of the air conditioners' capacity is operating on cooling.

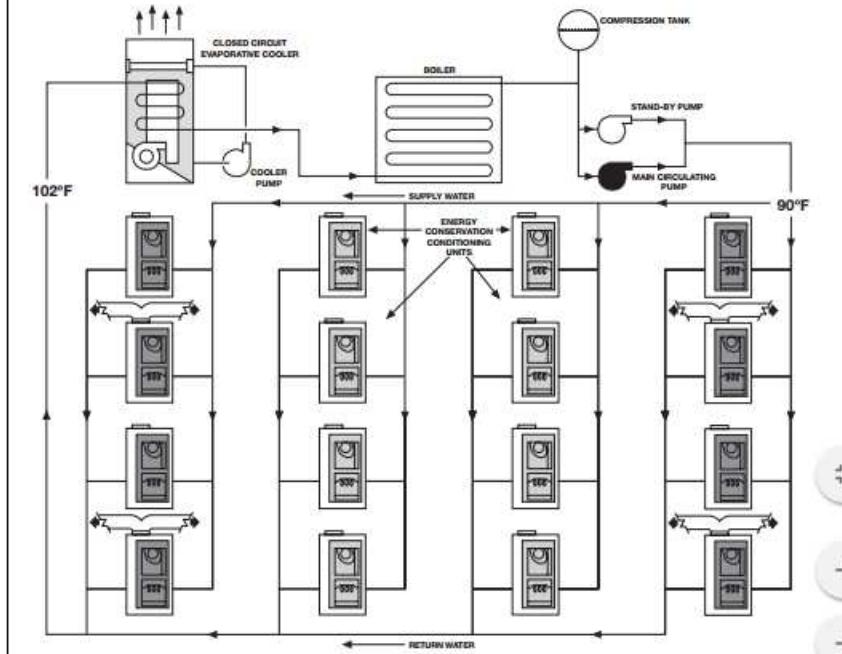


Figure 16: Configuration of conventional water-source heat pump system in buildings with high internal heat gain (McQuay Inc., 1999)

In moderate weather, units serving the shady side of a building are often heating while those serving the sunny side require cooling. When approximately one-third of the units in operation are cooling, they add sufficient heat to the water loop so that neither addition to nor rejection of heat from the water is required.

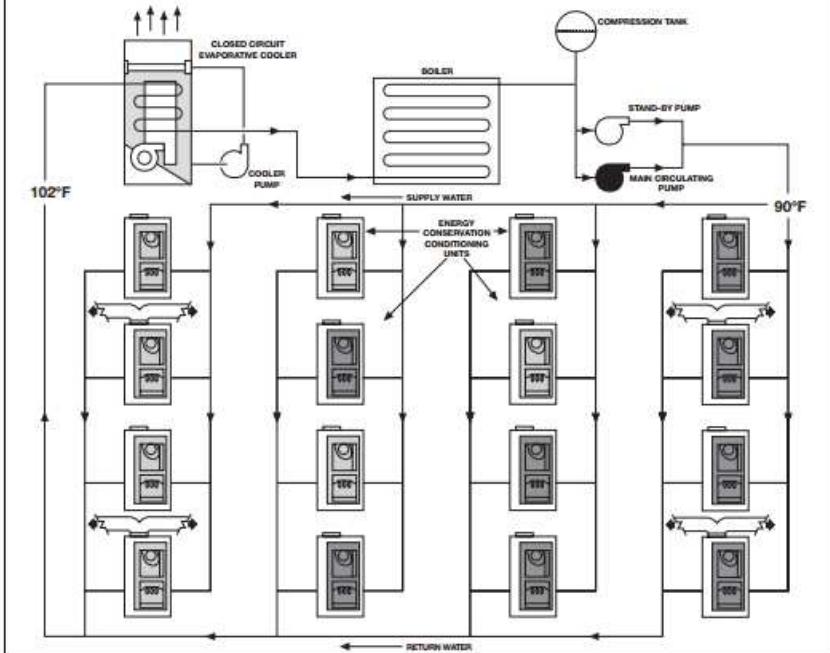


Figure 17: Configuration of conventional water-source heat pump system during simultaneous heating and cooling loads (McQuay Inc., 1999)

Energy storage tanks can be used for energy conservation. A low temperature storage tank can conserve energy by storing surplus heat produced in the building core during the day and acting as a heat source by supplying the stored heat at night for heating. A low temperature storage tank typically uses water in a tank. It can potentially eliminate use of a cooling tower in winter and shoulder season for rejection of any surplus heat. However, a cooling tower or a dry cooling is still necessary in the summer season for rejecting heat when the stored energy in the storage tank is no longer used for heating during the night time. Once surplus heat is rejected in the storage tank, its temperature can be raised up to 140 °F (60 °C) using water to water heat pump (McQuay Inc., 1999). The tank is piped parallel to the evaporative or dry cooler. When loop temperature is above the set range, loop water is diverted to the storage tank, where excess heat is rejected. This process continues until the storage tank reaches its highest temperature. At night time, when loop temperature becomes colder than the storage tank, the storage medium

rejects heat to the loop, which is then used by the heat pumps as heat source to provide energy to the areas in the need of cooling. Figure 18 is a typical schematic for a heat pump system that uses heat storage.

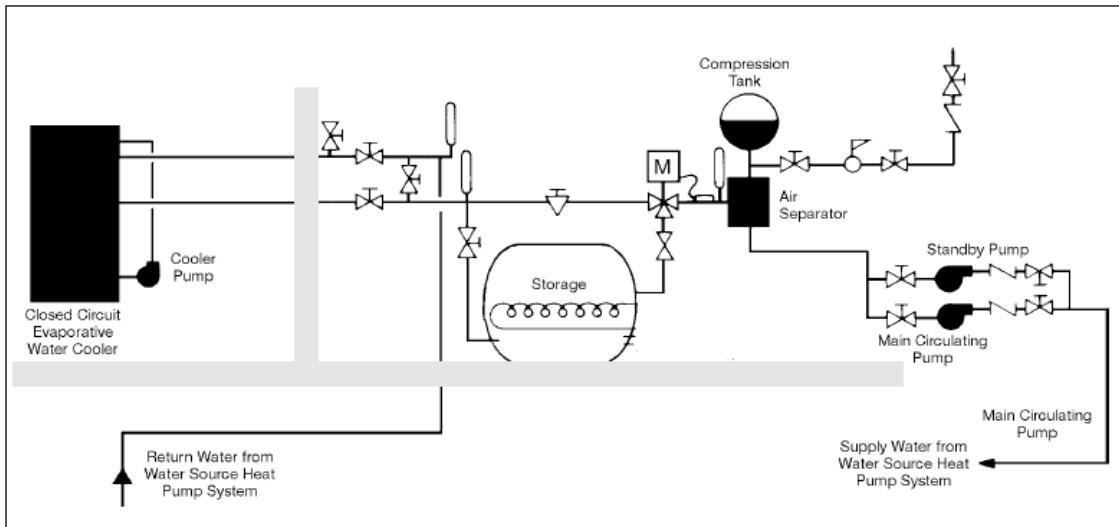


Figure 18: Heat pump system using heat storage tank (McQuay Inc., 1999)

The concept heat of heat pump system with heat storage and water-to-water heat pump is shown in Appendix A.

Water Loop Temperature Control: Water loop temperature is generally maintained between a minimum of 65 °F (18.3 °C) in winter and a maximum of 95 °F (35 °C) in the summer for optimal system operation by the building automation system (BAS) (Daikin McQuay Inc.). The control should start to reject heat in response to a temperature rise above 85 °F (29.4 °C) and achieve full capacity at 94 °F (34.4 °C). The controls should initiate addition of supplementary heat addition to the water loop when the loop temperature drops 67 °F (19.4 °C) (McQuay Inc., 1999)

Space temperature control for heat pumps includes low voltage wall thermostat. Typically one thermostat controls one heat pump; however for larger zones, two or more heat pumps can provide heating or cooling, and can be controlled by one thermostat. Night setback can substantially reduce the energy consumed by the HVAC system. Night setback can provide the following:

- 1) Restart all conditioners after a general shutdown, from a central point, when so

desired.

- 2) Stop all air conditioners from the same central point when desired.
- 3) Keep all electric circuits to the HVAC system energized at all times, to maintain a minimum conditioned space temperature at night time setting.
- 4) For systems with fans, cycle fans during night shut down period.
- 5) Switch ventilation systems off, and switch corridor lighting to night requirements.
- 6) Perimeter units can provide minimum space temperature control during the night setback.

Generally thermostats have a night temperature sensor set to control the heat pumps at 60 °F (15.6 °C) (McQuay Inc., 1999). During the morning pull-up period, most of the terminal units operate in the same mode. In winter, the perimeter units operate in the heating mode, while interior zones units are off. In summer, all units operate in the cooling mode. Through the provision of the energy storage tanks, a low temperature tank stores day surplus heat energy for overnight use.

2.5.2 Thermal Performance of Water Source Heat Pumps

Liu et al performed testing and analysis of typical water source heat pump system to establish thermal performance in the winter conditions. Testing and analysis were performed to assess energy efficiency indicator of the water source heat pump system. The following equations were used to calculate energy efficiency of the water source heat pump unit itself (EER_{HP}) and the whole system (EER_{system}):

$$EER_{HP} = Q_{cap} / W_{comp} \quad (\text{Equation 14})$$

$$EER_{system} = Q_{sh} / W_{input} \quad (\text{Equation 15})$$

Here Q_{cap} is heating produced by the heat pump

Q_{sh} is the space actual heating load

W_{comp} is the power input to the compressor

W_{input} is the total power input to the system

Test result shows that the heat pump system was able to maintain indoor average temperature at 73.76 °F (23.2 °C) for a 24 hour period though the outdoor temperature changed from 50 °F (10 °C) to 32 °F (0 °C) (Liu et al, 2011).

From the monitoring data of the heat pump system, it was noticed that the average temperature of water in the supply side of the source water is 13.20 °C (55.76 °F) and the return water temperature is 10.32 °C (50.58 °F) (Liu et al, 2011). Figure 19 shows supply and return temperature of the source water at different times in 24 hours period.

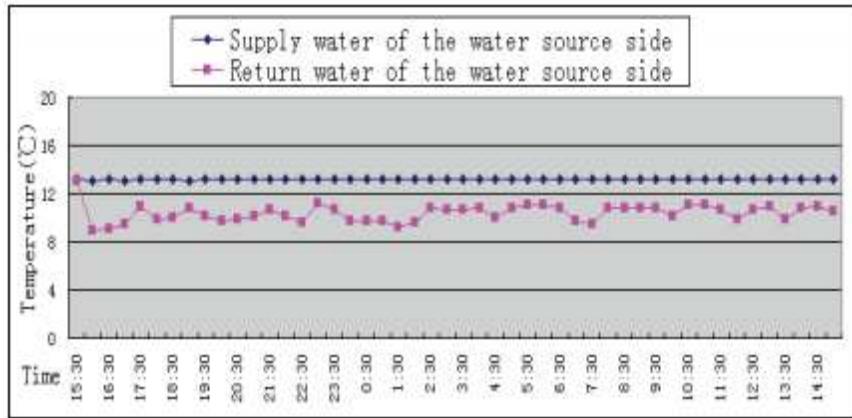


Figure 19: Source water temperature at supply and return sides of the heat pump (Liu et al, 2011)

At this design condition, the heat pump average efficiency (COP) is 3.12, whereas the rated nameplate COP is 3.51. It is suggested that the unit was operating at partial load, which caused the inefficiency. It is also suggested that the loop temperature should be increased to increase the efficiency of the heat pump (Liu et al, 2011).

2.5.3. Thermodynamic Performance Analysis of Water Source Heat Pump in Various Operating Condition

This study at the North China Electric Power University used the principal of the first law of thermodynamics to analyze performance of water source (water-to-water) heat pumps at variant operating conditions. It also suggests design and operation of water source heat pumps. Water source heat pumps usually work in off-design condition, under which the performance is different from what is rated in the equipment catalogue. The authors of this study selected a certain brand of water source heat pump with rated refrigerating capacity of 3,378 kBtu/h (990 kW), input power of 623.74 kBtu/h (182.8 kW), water flow of the condenser 396 gpm (90.1 m₃/h) and water flow of the evaporator 170.7 m₃/h (751 gpm). In the heating condition, the

heating output is 3,619 kBtu/h (1058 kW), input power is 810.72 kBtu/h (237.6 kW), water flow of the condenser is 835.56 gpm (189.9 m₃/h), and water flow of evaporator is 390.28 gpm (88.7 m³/h). Table 9 and table 10 show coefficient of performance (COP) at varying operating condition during cooling and heating operation of the water source heat pump.

Table 9: Cooling COP of water source heat pump in various operating condition

Inlet/outlet temperature Of chilled water(°)	Inlet/outlet temperature of cooling water (°C)				
	10/21	14/25	18/29	21/32	25/36
10/5	5.83698	5.302927	5.084178	4.634636	4.302235
12/7	6.248948	5.694918	5.415755	4.904835	4.578775
14/9	6.65196	6.017505	5.681233	5.165026	4.703156
16/11	6.988071	6.273696	5.988575	5.464989	4.902192
18/13		6.477668	6.189434	5.65753	5.00616
20/15		6.572518	6.335411	5.942952	5.190098

Table 10: Heating COP of water source heat pump in various operating condition

Inlet/outlet Temperature Of chilled water(°)	Inlet/outlet temperature of cooling water(°C)			
	40/45	43/48	45/50	47/52
13/5	4.317927	4.024702	3.870245	3.657708
15/7	4.452862	4.116797	3.962639	3.822368
17/9	4.629213	4.326838	4.166898	3.940586
19/11	4.849652	4.494477	4.33142	4.104377
21/13	5.020384	4.66094	4.493343	4.222542
23/15	5.238661	4.865164	4.653441	4.303186

It is evident that for cooling condition in summer, COP increases as the outlet temperature of the chilled water increases, and reduces as the inlet temperature of the cooling water increases. The outlet temperature of the chilled water can be properly increased and the inlet temperature of the cooling water can be properly decreased to reduce energy consumption (Zheng and Jing 2009).

In the winter operation, COP increases as the outlet temperature of the chilled water increases, and reduces as the inlet temperature of the cooling water increases (Zheng and Jing 2009).

For the intended common loop water source heat pump system it is expected that there will be cooling load in the core zones of the office building during the winter and shoulder season, whereas heating load is expected in the perimeter zones. Thus, a common loop temperature shall be selected to maximize the COP of both the heat pumps operating in the heating mode and the heat pumps in the cooling mode (Zheng and Jing 2009).

2.6 Energy Conservation Using Closed Loop Heat Pump in Commercial Office Building

This paper discusses the applicability of common loop water source heat pumps in buildings, where simultaneous heating and cooling loads occur. This was examined by modelling and simulation using software. The internally generated heat is used to meet heating load before use of any external source, using the closed water room as a transport system to move heat energy from where it is extracted to where it is needed. The paper also discusses the option of using thermal storage to store heat for later use. The paper reports the result of a study on the effect of component arrangement and system control strategy on the energy saving potential of the water loop heat pump used for heating and cooling of a commercial office building.

The water loop heat pump system design is similar to that of a four pipe fan coil system. Each perimeter zone is served by individual heat pumps, while the cores zones are served by a central air handling unit. In a typical winter day the perimeter zones normally require heating while the core zones require cooling because of human occupancy, lighting and equipment. The closed loop water first passes through the core zones, where the heat pump rejects extracted heat into the water loop. The heated water then passes through perimeter zones, where the heat is introduced by the heat pump.

This concept was simulated for both series circuit and parallel circuit concepts. For the series circuit configuration during the experimental simulation it was observed that during the summer days the exhaust water temperature core zones reached as high as 93 °C (200 °F). When this water was passed to the perimeter zones, which also needs cooling, the heat pumps worked very inefficiently. In such case the heated water will need to go through a cooling tower capable of bringing the water temperature down to a temperature that provides minimum cooling COP of the perimeter heat pumps. In winter the heated water will travel to the perimeter heat pumps directly without going through the cooling tower.

In the parallel configuration, water will be allowed to both core zone and perimeter zones at the same time during the summer months, thus allow the perimeter and core zone to receive water at the same temperature. During the winter the water flow will go through the core zones first and then the perimeter zones.

The building that was modelled under this study is a two storey building located in St. Louis, Missouri, which has a cold winter with record coldest temperature of -23 °C (-9.4 °F). Modelling parameters of the building are shown in Table 11:

Table 11: Modelling parameters of the commercial office building (Rao and Harry, 2009)

Building roof area	22,810 sq.ft. (2119 sq.m.)
Building floor area	45, 620 sq.ft. (4238 sq.m)
Building exterior wall	9,460 sq.ft. (879 sq.m)
Fenestration glass area	7,536 sq.ft. (700 sq.m.)
Internal load density in each zone	2.9 W/sq.ft (31 W/sq.m.)
Total occupancy	408 People
Ceiling height	8.5 ft (2.59 m)
Roof U-factor	0.25 Btu/hr.sq.ft.°F (0.79 W/sq.m.°C)
Exterior wall U-factor	0.2 Btu/hr.sq.ft.°F (0.63 W/sq.m.°C)
Glass U-factor	1 Btu/hr.sq.ft.°F (3.15 W/sq.m.°C)
Shading coefficient	0.6
Interior setpoint temperature	75 °F (23.9 °C)
Relative humidity	50%
Building thermal mass	Medium
Building operation	24 hours

The building was modelled in multiple states. After simulating the building with energy storage, it was found that there is a large drop in auxiliary heating energy consumption in St. Louis and Minneapolis, which have very cold winters (Rao and Harry, 2009). The energy saving has not been quantified in the report.

2.7 Optimizing Water Loop Temperature

Selecting the optimized temperature was part of a study performed by the University of Nebraska-Lincoln on the control strategy of water loop heat pump system. It is stated that generally the conventional heat pump loop temperature is maintained between 60 °F lower limit and 90 °F upper limit; heating boiler and cooling tower are programmed to this temperature range (Lian, 2011). Generally no measure is taken in the loop temperature is floating in this range. From a parametric analysis to find out the optimal supply temperature for the water source heat pump system, it has been found that the heat pump performance is more sensitive to the loop supply water temperature in the cooling mode than in the heating mode. By gather data from a heat pump manufacturer, it was found that the cooling energy efficiency ratio (EER) increases from 11 to 20 when the loop supply temperature decreases from 85 °F to 50 °F, and the heating EER increases from 17 to 19.5 when the supply temperature increases from 50 °F to 85 °F. Based on a mathematical model, Lian concluded that the water source heat pump system is most suitable for buildings that have interior cooling load ratio of 0.3 or higher. It is also concluded that during the heating season, the supply water temperature should be maintained as high as possible to improve the heat pump efficiency. Lian suggested that the temperature of water at the inlet of the heat pumps must be 50 °F or higher to ensure safety (Lian, 2011).

2.8 Office building-Heat recovery using water source heat pumps

This case study has been taken from ASHRAE Journal, published in December, 2014. The project of Jonxion-4905 Lapiniere is an 117,918 sq.ft. (10,955 sq.m.) office building near Montreal, and uses heat recovery from distributed common loop heat pump system without any external energy sources. Its energy consumption is only 9.7 kWh/ft² (104 kWh/m²) annually comparing to the Canadian office building average energy consumption of 31 kWh/ft² (333 kWh/m²) annually (Lussier, 2014).

Building envelope design was very crucial to balance the cooling and heating load so that the entire building and the fresh air supply can be heated by the recovered air and energy stored in the ground. Windows that are floor to ceiling are triple paned to limit the heat loss and heat gain in the perimeter areas. Windows that are 5 ft. high or less are double paned, low-e with argon

gas space. This architectural character of the building helped to minimize the perimeter heat loss so that heat rejection from the interior space can be sufficient for the perimeter heating.

The heat pump system for the building is located in the roof penthouse. Each floor has a secondary ventilation system. There is a dedicated outdoor air system (DOAS) on the roof that supplies 16,000 cfm (7551 L/s) of tempered fresh air to the secondary units, which also draws return air proportionally from the zones. The DOAS is equipped with an Energy Recovery wheel, which recovers heat and moisture from the exhaust air to pre-heat and humidify the fresh air introduced to the secondary units. There are six fan coil units to provide heating or cooling to the perimeter zones of the building. Heating and cooling to the fan coil units is provided by the central heat pump systems. Since the fan coils offset the heat loss/gain in the perimeter, the internal zones do not lose/gain heat to/from the outdoor environment; thus there is a sizable and consistent cooling load in the internal space generated from people, equipment, lighting etc.

The design incorporates two 80 ton (281 kW) centralized chillers, which act as heat pumps in the winter. Heat is removed from the interior zones by the chiller evaporators and transferred to the perimeter zones by the chiller condensers. The chiller evaporators operate 48 °F (9 °C) and condensers operate at 95 °F (35 °C), which results in a lower kW/ton. If the heat gain from the internal zones is not sufficient to heat the perimeters, the chillers extract energy from the ground using 28 geothermal closed loop vertical boreholes at 500 ft (152 m) deep. Heating coils are selected to use low temperature water allowing the chiller condenser water to provide heating without use of a boiler.

The distributed loop provides cooling to the interior space through the secondary ventilator. While the airflow from the secondary units is varied based on space load minimum fresh air supplied by the DOAS is set by ASHRAE 62.1 requirement. The fan coil units either cool or heat the perimeter zone based on the demand. All fans are equipped with variable frequency drives. Every coil is connected to the cooling and heating water loops and switches on the appropriate loop using automatic control three-way valves. All pumps are variable speed and modulate flow based on demand.

Both chilled and heated water are produced using two 80 ton (281 kW) high efficiency twin

screw compressor chillers. After one year of operation, it was observed that only one chiller is needed and it operates at 60% part load (48 ton). At this operation point, the chiller's energy consumption is about 0.65 kW/ton (Lussier, 2014). During the cooling season, when both perimeter and the interior zones are in need of cooling, the chillers extract heat from the building and then reject to the ground via the closed ground loops. Figure 20 shows schematic of the air system as well as the common loop heat recovery system.

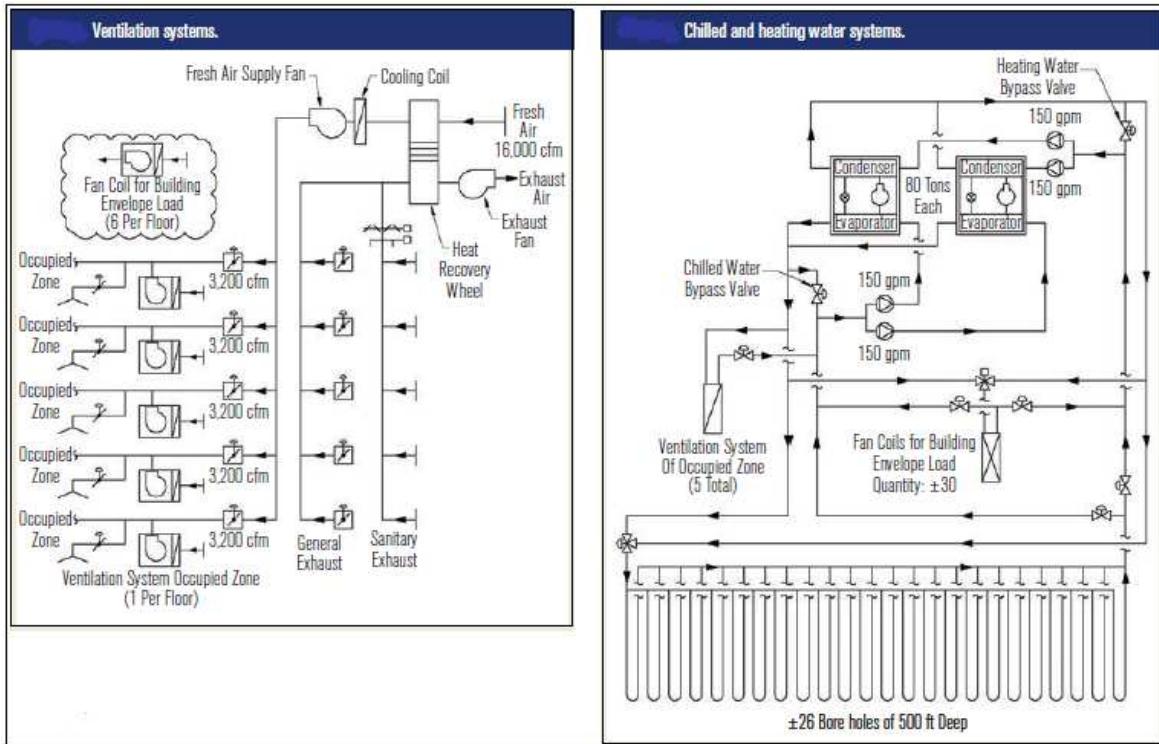


Figure 20: Schematic for ventilation, heating and cooling system (Lussier, 2014)

Energy performance of the building was modeled prior to the construction, and then actual energy consumption for one year was measured at 70% average occupancy level. Figure 21 compares model energy consumption with the actual energy consumption after one year of operation.

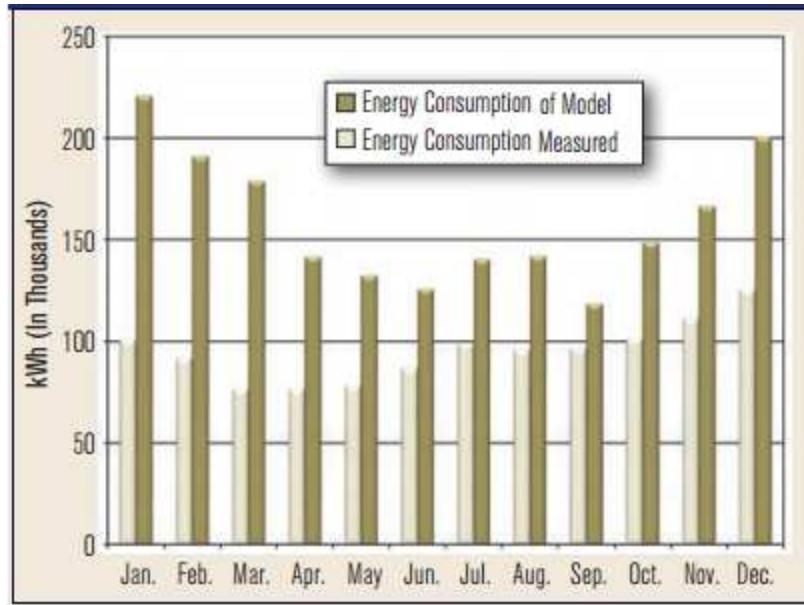


Figure 21: Modeled vs. actual energy consumption data (Lussier, 2014)

The actual total energy consumption for the year was 1,141,800 kWh, which translates to 9.7 kWh/ft² (104 kWh/m²), whereas the model energy consumption of the model was 1,906,400 kWh per year, which translates to 16 kWh/ft² (172 kWh/m²) per year. The actual annual energy consumption is 60% of the modeled energy consumption (Lussier, 2014).

3.0 Objective and Methodology

The simulation and analysis of this project is done in two parts. The first part will be modelling of a typical commercial office building in Toronto. Heating and cooling of this building will be provided by four pipe fan coil system served by centrifugal chiller and natural gas boiler. All parameters of the base case will be based on the minimum energy efficiency standard of ASHRAE 90.1. Simulation of the base model will produce the following:

- Building peak heating and cooling load (without HVAC)
- Space heating and cooling load summary. This will be used for sizing the zone heat pumps.
- Building peak heating and cooling load components.
- Building monthly and annual load summary.
- Building annual energy consumption for heating, cooling, lighting and internal equipment
- Building monthly energy consumption for heating, cooling, lighting and internal equipment.

The second part will be modelling and analysis of the same building using distributed common loop water source heat pump system. It is expected that there will be cooling load in the core zones during the winter and shoulder seasons, when heating load will exist in the perimeter zones. Heat pumps in the core zones will raise the temperature of the water loop, which will act as heat sink; the hotter water will then be used as heat source for the heat pumps in the perimeter to provide heating. The heat pump loop will be connected to a cooling tower and a condensing boiler to reject excess heat or add heat during the winter to maintain the loop at a predetermined temperature range. Peak heating and cooling load data, as well as the annual energy consumption from this model will be compared against the base case.

Once the proposed model energy consumption is determined using distributed loop water source heat pump system, a sensitivity analysis will be performed to investigate the energy saving potential by changing the common loop temperature.

4.0 Modelling and simulation

4.1 The Base Case

The base building is located in Toronto and designed to meet minimum design requirements of ASHRAE 90.1, which has been previously defined in section 1.6. It is a three storey building with a total area of 60,000 sq.ft. used for commercial office, which has private offices and board rooms along the perimeter, and open space in corridor with workstations and cubicles. The occupant density follows ASHRAE 62.1 standard for indoor air quality for buildings. Electricity rate has been taken from Toronto Hydro's time of use rate for commercial building, and the gas rate has been taken from Ontario Energy Board (rates have been shown in Table 13, 13A and 14). In order to utilize solar heat gain during the winter months, the building has been designed to have an aspect ratio of 1.5:1, which makes the north and south sides of the building longer than the east and west side. The south face of the building will be exposed to solar radiation for the longest time during the winter season. Wall, roof and window values are taken from the ASHRAE 90.1 standards, with windows making up 40% of the wall area. Windows are furnished with blinds to control the allowance of solar radiation during the summer months. Normally there is a dedicated make up air unit to introduce tempered outside air to the space, where ducts will carry the fresh air to the water loop heat pumps that serve individual zones. For the purpose of simplicity of the analysis, the make-up air unit has not been included in the model as it is independent of the building heating loop. Individual zones are heated and cooled by dedicated fan coil units that maintain minimum temperature starting from 1 hour before the building is occupied and ending 1 hour after the building is occupied; during the unoccupied hours the fan coils operate to maintain setback temperature. Heating and cooling of the building is provided by a natural gas boiler and a centrifugal chiller respectively, which uses a cooling tower for heat rejection. Domestic hot water demand and storage capacity is calculated by eQuest using the occupant density and hours of occupancy. Domestic water heating is provided by natural gas boiler, which is set to meet the minimum energy efficiency of ASHRAE 90.1 standard. The base building has been modelled using the Design Development Wizard in eQuest. Modelling parameters for the base building are shown in table 12 to table 28.

Table 12: Base building project and site data

Design Parameter/Requirement	Value
Building Type	Office building, mid-rise
Location	Canadian location
Region	Ontario region A
City	Toronto
Jurisdiction	ASHRAE 90.1
Electricity rate	Custom
Gas rate	Custom

Electricity Time of Use Rate (Source: Toronto Hydro):

According to the summer time of use (TOU) rates, effective May, 2016 to October 31, 2016 the time of use rates for weekdays are shown in table 13. Weekends and statutory holidays are at the lowest price (off-peak) all day. In addition, there is a monthly customer charge of \$30.47/month.

Table 13: Summer time-of-use electricity rate for commercial buildings (Toronto Hydro)

Time of the Day	Unit Rate (\$/kWh)	Delivery (\$/kWh)	Regulatory Charge (\$/kWh)	Debt Retirement (\$/kWh)	Total cost per unit (\$/kWh)
On-peak 11 am – 5 pm	0.18	0.044	0.050	0.007	0.281
Mid-peak 7 am – 11 am 5 pm – 7 pm	0.132	0.044	0.050	0.007	0.233
Off-peak 7 pm – 7 am	0.087	0.044	0.050	0.007	0.188

Winter time of use (TOU) electricity rates are shown in table 13A. Weekends and statutory holidays are at the lowest price (off-peak) all day.

Table 13A: Winter time-of-use electricity rate for commercial buildings (Toronto Hydro)

Time of the Day	Unit Rate (\$/kWh)	Delivery (\$/kWh)	Regulatory Charge (\$/kWh)	Debt Retirement (\$/kWh)	Total cost per unit (\$/kWh)
On-peak 7 am – 11 am 5 pm – 7 pm	0.18	0.044	0.050	0.007	0.281
Mid-peak 11 am – 5 pm	0.132	0.044	0.050	0.007	0.233
Off-peak 7 pm – 7 am	0.087	0.044b	0.050	0.007	0.188

Natural gas rate has been taken from Enbridge commercial rate, and shown in Table 14. In addition, there is a monthly customer charge of \$70/month.

Table 14: Block charges for natural gas supply for commercial buildings (Source: Enbridge)

Blocks (m ³)	Unit charge (\$/m ³)	Block (Therm)	Basic cost (\$/therm)	Supply Charge (\$/therm)	Transportation Charge (\$/therm)	Total unit cost (\$/therm)
500	0.091180	180	0.2533	0.2556	0.1482	0.6571
Next 1050	0.073162	378	0.2032	0.2556	0.1482	0.6070
Next 4500	0.060543	1620	0.1682	0.2556	0.1482	0.5720
Next 7000	0.052434	2520	0.1457	0.2556	0.1482	0.5495
Next 15250	0.048832	5490	0.1356	0.2556	0.1482	0.5394
Next 28300	0.047928	10188	0.1331	0.2556	0.1482	0.5369

Table 15: Building shell and footprint

Building shell area	60,000 ft ²
Number of floors above grade	3
Floor area at each floor	20,000 ft ²
Building dimension	173 ft x 115 ft
Daylight control	Yes
Plan north	Same as actual north
Building aspect ratio	1.5:1
Building shape	Rectangular
Perimeter depth	15 ft.
Floor to floor height	13 ft.
Percentage of area in the perimeter zones	38.8%
Floor to ceiling height	10 ft.

Table 16: Building envelope construction

Roof construction	4 in. concrete
Roof exterior finish	Built-up
Roof exterior insulation	5 in. polyurethane; RSI-5.28 (R-30)
Above grade exterior wall construction	4 in. heavy weight concrete
Exterior wall finish	Concrete with medium brown paint
Exterior wall insulation	2 in. polyisocyanurate; RSI-2.47 (R-14)
Ground floor exposure	Earth contact
Ground floor construction	6 inch concrete
Ground floor insulation	Full under slab insulation; RSI-1.76 (R-10)
Infiltration through exterior wall	0.038 cfm/ft ²
Interior wall type	Drywall (no additional insulation)

Table 17: Exterior doors and windows

Main entrance door	Revolving glass door at the south face
Other doors	1 glass door at each of the east, west and north
Revolving door dimension	Height = 7 ft.; Width = 6 ft.
All door glass property	U-factor = 0.32; SHGC = 0.40
All door framing	3 inch wide aluminum with thermal break
Exterior wall to window ratio	40%
Typical window dimension	6 ft. x 6 ft.
Window property	U-factor = 0.32; SHGC = 0.40; VT = 0.44
Window framing	Insulated fiberglass, non-operable

Table 18: Exterior shades and blinds

Blind type	Vertical blinds
Summer Season (June 21 to September 20)	
Percent of blinds closed when occupied	90% at all sides
Percent of blinds closed when unoccupied	90% at all sides
Winter Season (December 21 to March 20)	
Percent of blinds closed when occupied	20% at all sides
Percent of blinds closed when unoccupied	90% at all sides
Fall/spring season (remaining dates)	
Percent of blinds closed when occupied	20% at all sides
Percent of blinds closed when unoccupied	90% at all sides

Table 19: Roof skylight

Roof area covered by skylight	3%
Configuration	Domed with vinyl framing
Glazing type	Double acrylic white
Inside reflectance	70%

Table 20: Daylight control

Daylight control method	On/off
Percentage of lighting controlled	Ground and second floor: 100% in the perimeter zones Third floor: 100% in all zones
Photosensor per zone	1
Photosensor height	2.50 ft

Table 21: Building operation schedule

Monday to Friday	8:00 am – 5:00 pm
Saturday	Closed
Sunday	Closed
Holiday	Closed

Table 22: Activity area allocation

Activity type	Percent area (%)	Max occupancy (ft ² /person)
Office (open)	60	17
Office (executive)	20	100
Lobby	5	100
Restroom	5	100
Boardroom	4	15
Mechanical/electrical	4	333
Photocopy/Printing	2	333

Table 23: Interior lighting loads

Area type	Lighting density (W/sq.ft.)
Office (open)	1.10
Office (executive)	1.10
Lobby	1.30
Restroom	0.9
Boardroom	1.30
Mechanical/electrical	1.50
Photocopy/Printing	1.50

Table 24: Office equipment loads and profiles

Area type	Load (W/sq.ft.)	Sensible heat fraction
Office (open)	0.75	1.00
Office (executive)	0.75	1.00
Lobby	0.25	1.00
Restroom	0.10	1.00
Boardroom	0.10	1.00
Mechanical/electrical	0.10	1.00
Photocopy/Printing	0.70	1.00

Table 25: Zone HVAC system parameters

System type	4-pipe fan coil units
Location	System per zone
Cooling source	Chilled water coils
Heating source	Hot water coils
Zone thermostat set point for heating	Occupied : 70 °F; Unoccupied: 60 °F
Zone thermostat set point for cooling	Occupied : 75 °F; Unoccupied: 82 °F
Cooling supply temperature	55 °F
Heating supply temperature	95 °F
Fan operation hours	24 hours based on demand
Night time cycling	Cycles fan
Night cycle fan mode	Intermittent

Table 26: Cooling primary equipment design parameters

Chiller type	Electric centrifugal hermetic
Condenser type	Water cooled
Chiller sizing	Auto
Compressor	Variable speed
Chiller COP	3.8 (ASHRAE 90.1)
Pump configuration	Single system pump
Chilled water loop flow	Variable
Heat rejection equipment	Water cooled cooling tower
Condenser configuration	Open tower
Temperature control	Temperature reset based on demand
Capacity control	Variable speed fan
Chilled water temperature set point	44 °F
Operation control	On demand
Operating hours	24 hours based on demand

Table 27: Heating primary equipment

Heating equipment	Natural gas fired hot water boiler
Sizing	Auto
Boiler efficiency	80% (ASHRAE 90.1)
Pump configuration	Single system pump-variable speed
Hot water loop temperature	Load reset between 140 °F and 180 °F
Operation control	On demand
Operating hours	24 hours on demand

Table 28: Domestic hot water modeling parameter

Heat source	Natural gas
Heating efficiency	80% (ASHRAE 90.1)
Input rating	1,748 kBtu (calculated by eQuest)
Tank capacity	1,235 gallons (calculated by eQuest)
Supply water	140 °F (60°C)
Cold water temperature (at inlet)	Same as seasonal ground temperature

Once the modelling is completed, eQuest produced 3D view of the three storey building (shown in Figure 22), and schematic view of the heating, cooling and domestic hot water (DHW) system (shown in Figure 23).

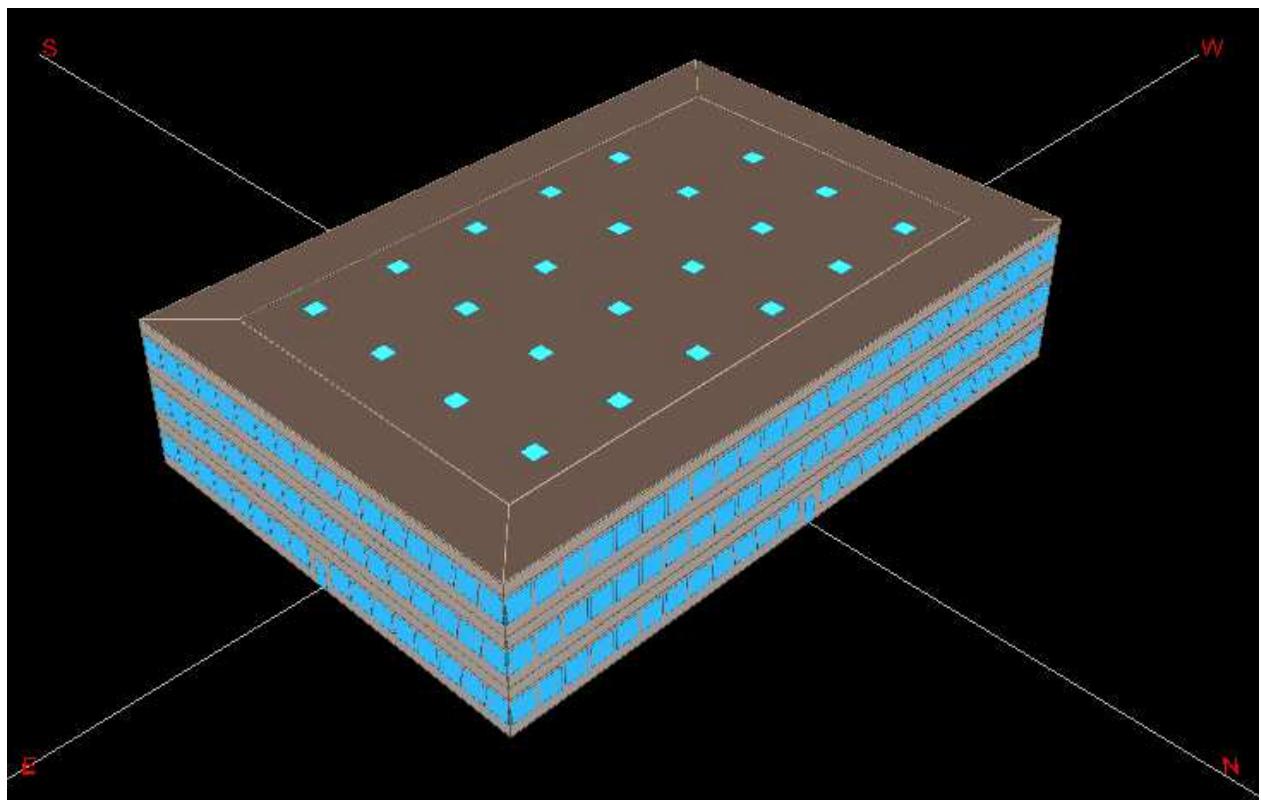


Figure 22: 3D view of the three storey office building

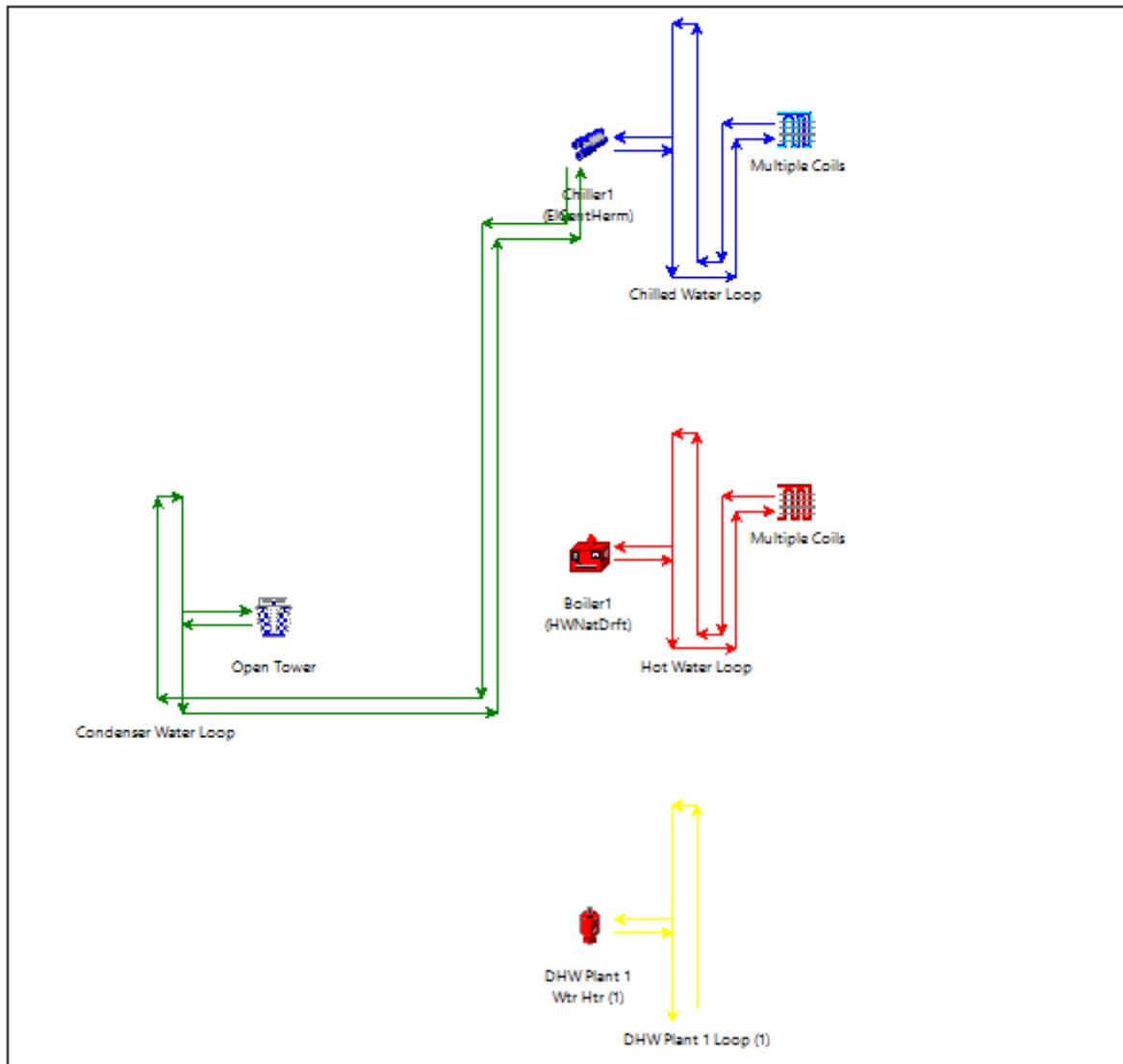


Figure 23: Heating, cooling and domestic hot water heating schematic produced by eQuest

4.1.1 Base Case Simulation Result

After simulation of the base building, eQuest has produced detailed load and energy consumption data. Peak heating and cooling loads of the building are 261.9 kBtu/h (76.7 kW) and 1458.4 kBtu/h (427.3 kW) respectively. The peak load components for the building and their effects on the heating and cooling loads are shown in Table 29.

Table 29: Building peak load and components (from eQuest simulation result)

FLOOR	AREA	59988	SQFT	5573	M2	
VOLUME		599878	CUFT	16989	M3	
TIME	COOLING LOAD				HEATING LOAD	
	JUN 11	4PM			JAN 1	6AM
DRY-BULB TEMP	86 F		30 C		-3 F	-19 C
WET-BULB TEMP	69 F		21 C		-3 F	-19 C
TOT HORIZONTAL SOLAR RAD	216 BTU/H.SQFT		680 W/M2		0 BTU/H.SQFT	0 W/M2
WINDSPEED AT SPACE	10.6 KTS		5.4 M/S		7.8 KTS	4.0 M/S
CLOUD AMOUNT 0 (CLEAR) -10	6				7	
	SENSIBLE (BTU/H)	(KW)	LATENT (BTU/H)	(KW)	SENSIBLE (BTU/H)	(KW)
WALL CONDUCTION	9.663	2.831	0.000	0.000	-32.411	-9.496
ROOF CONDUCTION	0.146	0.043	0.000	0.000	-0.886	-0.260
WINDOW GLASS+FRM COND	40.602	11.896	0.000	0.000	-212.944	-62.393
WINDOW GLASS SOLAR	231.593	67.857	0.000	0.000	11.901	3.487
DOOR CONDUCTION	0.000	0.000	0.000	0.000	0.000	0.000
INTERNAL SURFACE COND	0.000	0.000	0.000	0.000	0.000	0.000
UNDERGROUND SURF COND	-6.851	-2.007	0.000	0.000	-10.515	-3.081
OCCUPANTS TO SPACE	492.914	144.424	441.087	129.239	0.000	0.000
LIGHT TO SPACE	115.762	33.918	0.000	0.000	2.675	0.784
EQUIPMENT TO SPACE	115.049	33.709	0.000	0.000	5.980	1.752
PROCESS TO SPACE	0.000	0.000	0.000	0.000	0.000	0.000
INFILTRATION	10.543	3.089	7.891	2.312	-25.667	-7.520
TOTAL	1009.421	295.760	448.979	131.551	-261.868	-76.727
TOTAL / AREA	0.017	0.053	0.007	0.024	-0.004	-0.014
TOTAL LOAD	1458.399	KBTU/H	427.311	KW	-261.868	KBTU/H
TOTAL LOAD / AREA	24.31	BTU/H.SQFT	76.675	W/M2	4.365	BTU/H.SQFT
						13.768 W/M2

Zone peak heating and cooling loads generated by eQuest are shown in table 30. It is worth noting that at any floor, though the south and the north perimeter zones have same area, the heating load is higher in the north as it gains less solar heat than the south. Similarly, cooling load is lesser in the north perimeter than the south because the north gains less solar radiation than the south.

Table 30: Zone peak heating and cooling loads (eQuest simulation result)

Zone	Heating Load		Cooling Load	
	kBtu/h	kW	kBtu/h	kW
Ground floor south perimeter	24	7.1	46	13.4
Ground floor east perimeter	18	5.4	29	8.4
Ground floor north perimeter	29	8.5	23	6.6
Ground floor west perimeter	19	5.6	26	7.5
Ground floor core zone	2	0.7	186	54.5
Second floor south perimeter	26	7.7	70	20.4
Second floor east perimeter	18	5.4	45	13.1
Second floor north perimeter	28	8.3	33	9.8
Second floor west perimeter	19	5.5	40	11.7
Second floor core zone	0	0.1	217	63.7
Third floor south perimeter	31	9.0	71	20.9
Third floor east perimeter	21	6.2	46	13.4
Third floor north perimeter	33	9.6	35	10.3
Third floor west perimeter	22	6.4	41	12.0
Third floor core zone	51	14.8	270	79.0

Monthly total energy consumption is shown in Table 31 and monthly total gas consumption is shown in table 32. From the monthly electricity consumption, it is evident that space cooling is needed in even in the coldest months (December, January and February). This is due to the cooling requirement in the core zones, which gain internal heat but loses very little or no heat to the external atmosphere. Cooling load is higher during the summer months because all zones require cooling during them. Space heating energy consumption is the highest during the coldest months and it reduces in the shoulder seasons. During the hottest months (June, July, August and September) there is no space heating related energy consumption. Energy consumption related to domestic water heating does not change drastically from month to month; this is due to the consistency in the demand of domestic hot water. It can be noticed that the energy consumption for domestic water heating is higher during the winter months because the incoming cold water temperature is lower due to the colder earth temperature, thus more energy

is required to raise the water temperature to 140 °F.

Table 31: Monthly total electricity consumption in kWh x 1000 (generated by eQuest)

End Use	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Total
Space Cool	9.8	10.0	12.4	12.7	13.6	20.9	24.4	22.7	16.9	12.2	10.8	11.1	177.5
Heat Reject.	0.1	0.1	0.1	0.2	0.3	0.7	1.0	1.0	0.6	0.3	0.2	0.1	4.6
Refrigeration	-	-	-	-	-	-	-	-	-	-	-	-	-
Space Heat	-	-	-	-	-	-	-	-	-	-	-	-	-
HP Supp.	-	-	-	-	-	-	-	-	-	-	-	-	-
Hot Water	-	-	-	-	-	-	-	-	-	-	-	-	-
Vent. Fans	1.1	1.0	1.2	1.3	1.4	1.9	1.9	1.9	1.6	1.2	1.0	1.1	16.6
Pumps & Aux	3.4	3.4	4.1	4.2	4.7	6.8	8.6	7.7	5.9	4.1	3.5	3.8	60.0
Ext. Usage	-	-	-	-	-	-	-	-	-	-	-	-	-
Misc. Equip.	9.7	9.5	11.4	10.9	10.1	10.9	10.5	11.0	10.5	10.1	10.1	10.5	125.2
Task Lights	-	-	-	-	-	-	-	-	-	-	-	-	-
Area Lights	11.8	11.3	13.0	12.0	10.2	11.1	11.0	11.0	11.4	11.6	13.0	13.4	140.7
Total	35.9	35.4	42.1	41.2	40.3	52.3	57.4	55.3	46.8	39.4	38.5	40.0	524.5

Yearly utility bill for the base case is \$132,404, of which \$125,171 is for electricity and \$7,233 is for natural gas.

The greenhouse gas (CO₂) emission factor in Ontario for natural gas is 1,879 gram/m³ (Government of Canada, 2011). Based on that natural gas consumption of 1056 million Btu, which is equivalent to 29,316 m³, produces . Therefore, 55,084,764 grams (55.1 tonnes) of green house gas will be reduced.

Greenhouse gas (CO₂) emission factor for electricity is 244 gram/kWh (City of Toronto, 2007).

Based on that, greenhouse gas emission for electricity for the base case is 127 tonnes.

The total greenhouse gas released by the base case is 182.1 tonnes.

Table 32: Monthly total natural gas consumption in million Btu (table generated by eQuest)

End Use	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Total
Space Cool	-	-	-	-	-	-	-	-	-	-	-	-	-
Heat Reject.	-	-	-	-	-	-	-	-	-	-	-	-	-
Refrigeration	-	-	-	-	-	-	-	-	-	-	-	-	-
Space Heat	106.8	77.9	49.4	16.2	0.9	-	-	-	-	8.0	36.1	77.2	372.5
HP Supp.	-	-	-	-	-	-	-	-	-	-	-	-	-
Hot Water	57.7	58.9	70.8	66.7	57.4	57.8	52.0	51.8	49.3	49.3	52.6	59.2	683.5
Vent. Fans	-	-	-	-	-	-	-	-	-	-	-	-	-
Pumps & Aux	-	-	-	-	-	-	-	-	-	-	-	-	-
Ext. Usage	-	-	-	-	-	-	-	-	-	-	-	-	-
Misc. Equip.	-	-	-	-	-	-	-	-	-	-	-	-	-
Task Lights	-	-	-	-	-	-	-	-	-	-	-	-	-
Area Lights	-	-	-	-	-	-	-	-	-	-	-	-	-
Total	164.5	136.8	120.2	82.8	58.3	57.8	52.0	51.8	49.3	57.4	88.6	136.4	1056.0

Base building simulation results are shown in Appendix C.

4.2 Proposed Case 1

The proposed case is similar to the base case except that it uses distributed water loop heat pump system for space heating and cooling. Building envelope design, occupancy, lighting, office equipment and water heating parameters remain same as the base building. Therefore it is expected that the space heating and cooling loads will not change, but the energy consumption due to heating and cooling operation will change due to change of the HVAC system. Similar to the base case, in the proposed case, make up air has not been included in the model for the purpose of simplicity as it is independent of the space heating and cooling system. The water source heat pump design parameters are shown in Table 33 and Table 34.

Table 33: Zone HVAC system parameters

System type	Water source heat pumps
Location	System per zone
Cooling source	Water loop
Heating source	Hot water loop
Zone thermostat set point for heating	Occupied : 70 °F; Unoccupied: 60 °F
Zone thermostat set point for Cooling	Occupied : 75 °F; Unoccupied: 82 °F
Cooling supply air temperature	55 °F
Heating supply air temperature	95 °F
Cooling Energy Efficiency Ratio (EER)	13.0 (ASHRAE 90.1)
Heating Coefficient of Performance (COP)	4.3 (ASHRAE 90.1)
Fan operation hours	24 hours based on demand
Night time cycling	Cycles fan
Night cycle fan on via	Zone controls

Table 34: Water source heat pump plant equipment

Heat generating equipment	Condensing boiler
Fuel type	Natural gas
Efficiency	91.5% (ASHRAE 90.1)
Heat rejection equipment	Water cooled cooling tower
Condenser configuration	Open tower
Capacity control	Variable speed fan
Fan type	Centrifugal
Fan efficiency	High
Pump configuration	Single loop pump
Loop flow	Variable
Operation of the pump	On demand
Loop minimum temperature	68 °F (20 °C) (ASHRAE 90.1)
Loop maximum temperature	86 °F (30 °C) (ASHRAE 90.1)

Once the water source heat pump was modelled, it created a common loop system, where both heat pumps in heating mode and heat pumps in cooling mode operate simultaneously, thus the heat rejected from the cooling zones can be used in the zones in requirement of heating. The cooling tower and the condensing boiler operate on a need basis to maintain the loop supply temperature between 68 °F (20 °C) and 86 °F (30 °C), which are the energy efficiency rating conditions used in ASHRAE 90.1. Upon completion of the proposed case the common loop water source heat pump schematic was generated by eQuest, and it has been shown in Figure 24.

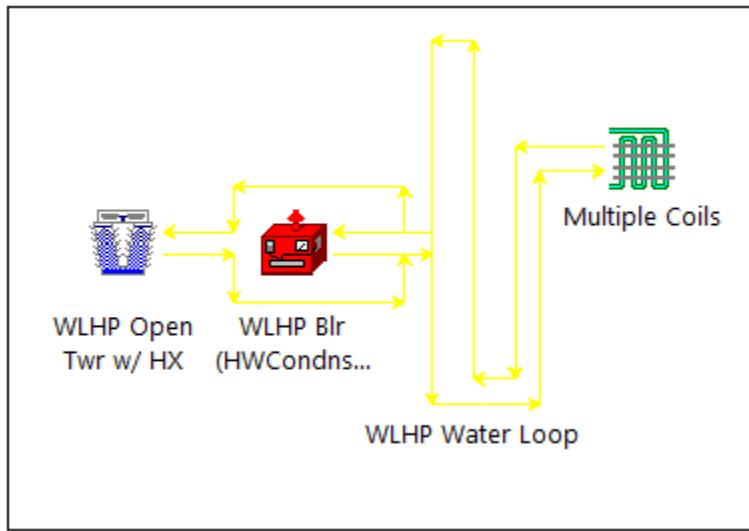


Figure 24: Common loop water source heat pump schematic generated by eQuest

The monthly and annual total electricity and natural gas consumption have been shown in Table 35 and Table 36. It is evident that cooling is required throughout the year though the cooling load doubles between winter and summer. The total annual electricity consumption is 555,370 kWh and the total natural gas consumption is 711.71 million Btu.

Table 35: Monthly electricity consumption (kWh x 1000) for proposed Case 1

End Use	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Total
Space Cool	11.1	11.7	15.6	17.5	19.4	24.8	25.3	25.4	22.1	17.1	13.6	13.1	216.6
Heat Reject.	0.0	0.0	0.0	0.1	0.1	0.3	0.5	0.4	0.2	0.1	0.1	0.0	1.8
Refrigeration	-	-	-	-	-	-	-	-	-	-	-	-	-
Space Heat	4.2	2.5	1.2	0.2	0.0	-	-	-	-	0.1	0.9	2.6	11.7
HP Supp.	-	-	-	-	-	-	-	-	-	-	-	-	-
Hot Water	-	-	-	-	-	-	-	-	-	-	-	-	-
Vent. Fans	1.5	1.4	1.7	1.7	1.8	2.4	2.5	2.5	2.1	1.6	1.4	1.6	22.2
Pumps & Aux	2.6	2.5	2.8	2.8	3.0	3.8	4.4	3.9	3.3	2.7	2.4	2.8	37.1
Ext. Usage	-	-	-	-	-	-	-	-	-	-	-	-	-
Misc. Equip.	9.7	9.5	11.4	10.9	10.1	10.9	10.5	11.0	10.5	10.1	10.1	10.5	125.2
Task Lights	-	-	-	-	-	-	-	-	-	-	-	-	-
Area Lights	11.8	11.3	13.0	12.0	10.2	11.1	11.0	11.0	11.4	11.6	13.0	13.4	140.7
Total	41.0	39.0	45.6	45.2	44.7	53.3	54.1	54.2	49.6	43.2	41.4	44.0	555.37

Table 36: Month natural gas consumption (million Btu) for proposed Case 1

End Use	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Total
Space Cool	-	-	-	-	-	-	-	-	-	-	-	-	-
Heat Reject.	-	-	-	-	-	-	-	-	-	-	-	-	-
Refrigeration	-	-	-	-	-	-	-	-	-	-	-	-	-
Space Heat	18.4	5.0	0.4	-	-	-	-	-	-	-	-	4.4	28.1
HP Supp.	-	-	-	-	-	-	-	-	-	-	-	-	-
Hot Water	57.7	58.9	70.8	66.7	57.4	57.8	52.0	51.8	49.4	49.3	52.6	59.2	683.6
Vent. Fans	-	-	-	-	-	-	-	-	-	-	-	-	-
Pumps & Aux	-	-	-	-	-	-	-	-	-	-	-	-	-
Ext. Usage	-	-	-	-	-	-	-	-	-	-	-	-	-
Misc. Equip.	-	-	-	-	-	-	-	-	-	-	-	-	-
Task Lights	-	-	-	-	-	-	-	-	-	-	-	-	-
Area Lights	-	-	-	-	-	-	-	-	-	-	-	-	-
Total	76.1	63.9	71.2	66.7	57.4	57.8	52.0	51.8	49.4	49.3	52.6	63.6	711.71

In order to verify that the heat rejected from the heat pumps in cooling mode is used for heating in zones requiring heat, hourly energy consumption data has been checked. On January 4th, which is one of the coldest days of the year, there are both heating and cooling loads during the occupied hours, shown in Table 37 (generated from eQuest hourly data). It can be noticed that there is natural gas consumption by the heating boiler from the 1st hour to the 10th hour, when there is no cooling operation. Once the cooling operation begins at the 10th hour, the heating natural gas consumption become zero due to simultaneous heating and cooling operation.

Table 37: Hourly energy consumption data on January 4th, 2016

Month	Day	Hour	Heating end-use energy (kWh)	Cooling end-use energy (kWh)	Heat rejection end-use energy (kWh)	Heating end-use energy (Btu)	Domestic hot water end-use	Total end-use energy (Btu)
1	4	1	18.470	0.000	0.000	147228	20908	168136
1	4	2	18.175	0.000	0.000	143293	20909	164202
1	4	3	18.337	0.000	0.000	145238	20901	166140
1	4	4	18.267	0.000	0.000	144376	20900	165275
1	4	5	18.150	0.000	0.000	142862	20898	163759
1	4	6	18.328	0.000	0.000	145107	20896	166004
1	4	7	17.424	0.000	0.000	139135	36557	175692
1	4	8	55.269	0.000	0.000	615185	159247	774432
1	4	9	31.133	0.000	0.000	320112	159212	479324
1	4	10	17.157	5.806	0.000	134423	281636	416059
1	4	11	12.472	17.146	0.000	0	281574	281574
1	4	12	11.861	10.349	0.000	0	281461	281461
1	4	13	11.267	21.297	0.000	0	281416	281416
1	4	14	9.533	44.941	0.000	0	281414	281414
1	4	15	7.345	51.478	0.000	0	281391	281391
1	4	16	6.063	54.262	0.006	0	218691	218691
1	4	17	7.906	42.737	0.000	0	158628	158628
1	4	18	10.626	15.664	0.000	0	95959	95959
1	4	19	0.000	0.000	0.000	0	67231	67231
1	4	20	0.000	0.000	0.000	0	67242	67242
1	4	21	0.000	0.000	0.000	0	67250	67250
1	4	22	0.000	0.000	0.000	0	20282	20282
1	4	23	0.266	0.000	0.000	0	20300	20300
1	4	24	2.136	0.000	0.000	0	20310	20310

4.3 Result Comparison:

Based on the energy consumption data, Table 38 and Table 39 have been created to compare annual energy consumption between the base case and the proposed Case 1.

Table 38: Electricity consumption comparison between base case and proposed case 1

End Use	Base Case	Proposed Case	Increase/decrease	% increase/decrease
Space Cool	177.47	216.6	39.1	22.04%
Heat Reject.	4.59	1.8	-2.8	-60.78%
Refrigeration	-	-		
Space Heat	-	11.7		
HP Supp.	-	-		
Hot Water	-	-		
Vent. Fans	16.56	22.2	5.7	34.24%
Pumps & Aux	60.02	37.1	-22.9	-38.14%
Ext. Usage	-	-		
Misc. Equip.	125.23	125.2	0.0	0.00%
Task Lights	-	-		
Area Lights	140.68	140.7	0.0	0.00%
Total	524.54	555.4	30.8	5.88%

Table 39: Annual natural gas consumption comparison in million Btu (negative denotes decrease by the proposed case1)

End Use	Base Case	Proposed Case	Increase/decrease	% increase/decrease
Space Cool	-	-		
Heat Reject.	-	-		
Refrigeration	-	-		
Space Heat	372.5	28.1	-344.4	-92.45%
HP Supp.	-	-		
Hot Water	683.5	683.6	0.1	0.01%
Vent. Fans	-	-		
Pumps & Aux	-	-		
Ext. Usage	-	-		
Misc. Equip.	-	-		
Task Lights	-	-		
Area Lights	-	-		
Total	1,056.00	711.7	-344.3	-32.60%

There is 30,800 kWh (5.88%) increase in electricity consumption by proposed Case 1; this is due to the work input to the compressors in the heat pumps for both heating and cooling operations. Electricity consumption by the cooling tower has decreased 60.78% comparing to the base case due to the exhaust heat from the cooling operation being used for space heating. Natural gas consumption for heating has drastically reduced by 344.4 million Btu (92.45%) due to the use of distributed common loop heat pump system, and the overall natural gas consumption has reduced by 32.60%. By converting the reduction of natural gas to equivalent kWh, it can be seen that 100,904.37 equivalent kWh hour has been saved. Thus, measuring the total equivalent kWh saving gives $(-100,904.37 + 30,800) = -70,104.37$ kWh of annual energy saving.

4.4 Greenhouse Gas Emission

The greenhouse gas (CO₂) emission factor in Ontario for natural gas is 1,879 gram/m³ (Government of Canada, 2011). Using the common loop water source heat pump system of

proposed case 1, the natural gas consumption has been reduced by 344.4 million Btu, which is equivalent to 9,317 m³ of natural gas. Therefore, 17,506,643 grams (17.5 ton) of greenhouse gas will be reduced.

Electricity consumption has increased by 30,800 kWh, thus green house gas emission increased by 7.52 tonnes.

Therefore, overall greenhouse gas reduction by Proposed Case1 is 10 tonnes.

5. Modelling for Sensitivity Analysis

The purpose of the sensitivity analysis is to determine the influence of the change of design parameters of the building as well as the heat pump system. The sensitivity analysis of the proposed common loop water based heat pump system will be re-modelled three times by changing design temperature of the common water loop. The result of the three models will be then compared against the proposed Case 1 to find optimum operating range of the common loop based on energy consumption.

5.1 Sensitivity analysis for finding optimum heat pump system design parameters

5.1.1 Proposed Case 2: Water loop temperature at lowest 50 °F and highest 86 °F

From the base building simulation result, it is evident that the building is cooling dominated in the winter months. Thus in order to observe the change of energy performance of the common loop heat pump system, the loop temperature of the proposed case has been lowered, which is expected to increase the cooling COP and decrease the heating COP; however, the magnitude of the cooling COP increase is higher than that of the heating COP (Lian, 2011). For the proposed Case 2, the lowest design temperature of the loop is set at 50 °F (Lian, 2011). The highest design temperature of the water loop remains 86 °F (ASHRAE 90.1). Simulation produces annual electricity and natural gas consumption of **543,700 kWh** and **700.5 million Btu** respectively.

5.1.2 Proposed Case 3: Water loop temperature at lowest 50 °F and highest 72.14 °F

For the proposed Case 3, the lowest design temperature of the loop is set at 50 °F. The highest design temperature of the water loop is lowered to 78.12 °F, which is the design outdoor wet bulb temperature in Toronto (ASHRAE Fundamental, 2005); this temperature can be achieved by the operation of a cooling tower in summer. Upon simulation, the annual electricity consumption is **534,050 kWh**, and natural gas consumption is **702.35 million Btu**.

5.1.3 Proposed Case 4: Water loop temperature lowest 68 °F and highest 72.14 °F

The water loop minimum is set at 68 °F, which is the design temperature used for minimum energy efficiency requirement in ASHRAE 90.1. The highest temperature of the loop is set at 72.14 °F, which is the design outdoor wet bulb temperature in Toronto (ASHRAE,

2005). Annual electricity consumption for proposed case 4 is **533,340 kWh**, and the natural gas consumption is **714.53 million Btu**.

5.1.4 Annual electricity and natural gas consumption of proposed case 1, 2, 3 and 4 have been compared in table 40, which helps to determine the optimum temperature setting for the common water loop.

Table 40: Sensitivity test to determine optimum temperature of the common loop

	Base Case	Proposed Case 1	Proposed Case 2	Proposed Case 3	Proposed Case 4
Electricity (kWh)	524,500	555,370	543,700	534,050	533,340
Natural Gas (MMBtu)	1056.0	711.71	700.5	702.35	714.53
Yearly electricity bill (\$)	125,171	137,979	135,173	132,794	132,609
Yearly natural gas bill (\$)	7,233	5,245	5,181	5,192	5,262
Total annual utility bill (\$)	132,404	143,224	140,354	137,986	137,871

Though, the electricity consumption of proposed Case 3 is slightly higher than that of proposed case 4, the natural gas consumption of Case 3 is significantly less than case 4. Therefore, proposed case 3 is the optimum solution, which suggests the common loop temperature should operate between 50 °F and highest 72.14 °F.

5.2 Comparison between the base case and proposed case 3

Table 41 compares between the base case and the optimum proposed case in terms of annual electricity consumption, annual natural gas consumption and annual utility bill.

Table 41: Energy and economic comparison between the base case and proposed case 3

	Base Case	Proposed Case 3
Electricity (kWh)	524,540	534,050
Natural gas (MMBtu)	1,056.00	702.35
Annual utility bill (\$)	132,404	137,986

There is 9,510 kWh (1.81%) increase in electricity consumption by proposed case 3; this is due to the work input to the compressors in the heat pumps for both heating and cooling operations. Natural gas consumption has been reduced by 353.65 million Btu (33.48%). Annual utility bill has increased by \$5,582.00 which is 4.22% higher than the base case.

The greenhouse gas (CO₂) emission factor in Ontario for natural gas is 1,879 gram/m³ (Government of Canada, 2011). Using the common loop water source heat pump system of proposed Case 3, the natural gas consumption has been reduced by 353.65 million Btu, which is equivalent to 9,567.239 m³ of natural gas. Therefore, 17,976,842 grams (17.98 ton) of green house gas will be reduced.

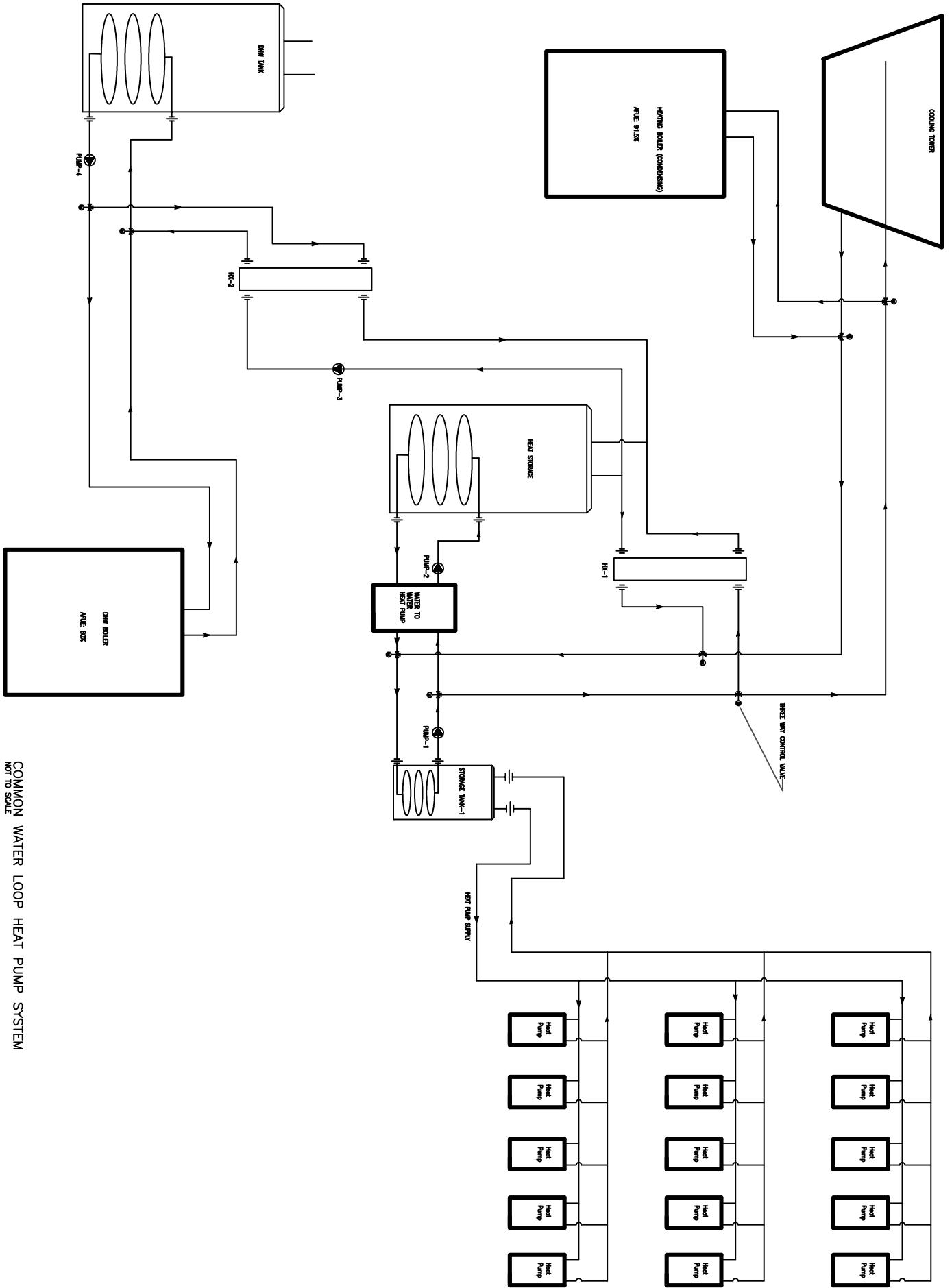
Electricity consumption has increased by 9,510 kWh, thus green house gas emission increased by 2.3 tonnes.

Therefore, overall greenhouse gas reduction by Proposed Case 3 is 15.7 tonnes.

6. Conclusion

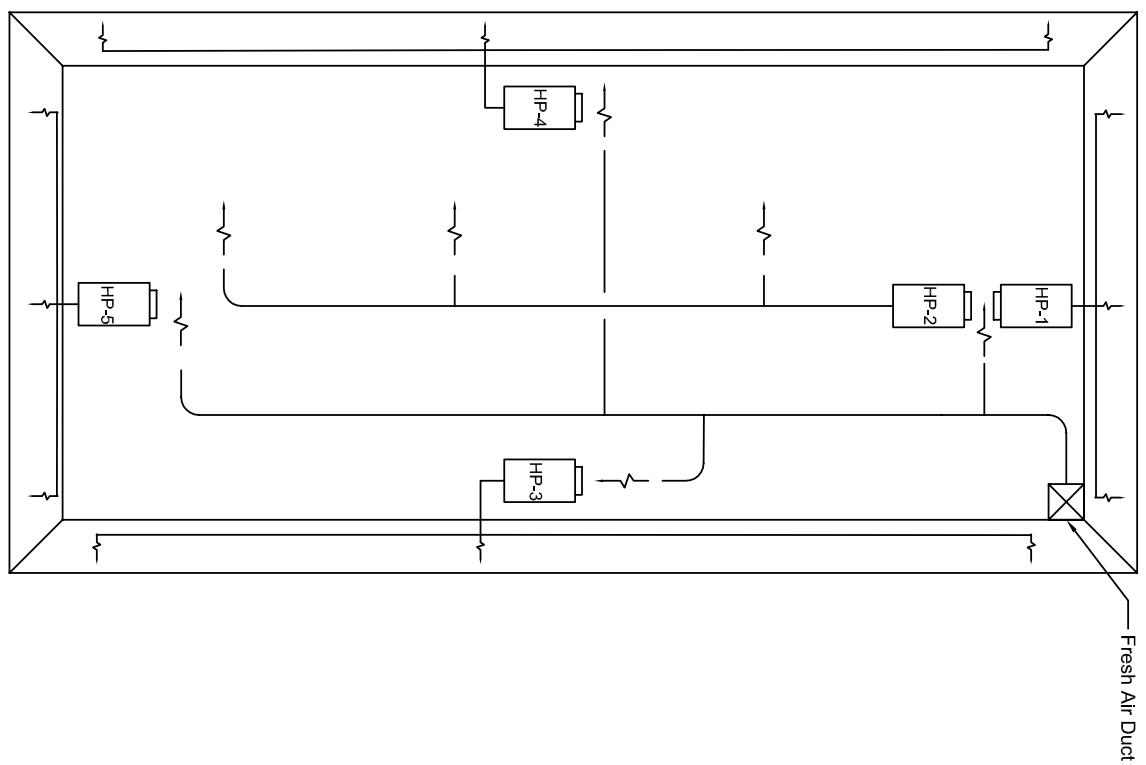
From the energy and environmental consideration, the common loop water source heat pump system is a significantly better option than the base case; however, from the economic point of view, the base case is better than the proposed case. It should be noted that further natural gas saving can be achieved if the remaining exhaust heat in the common water loop can be stored in a heat storage system, and subsequently used for space heating during the hours when there is no cooling load in the building. During the shoulder season and the summer months, the stored heat can be used for domestic water preheating using a water-to-water heat pump, which provides and excelled opportunity to reduce consumption of natural gas. This will also reduce the electricity consumption of the cooling tower, as the tower will then need to reject less heat to the atmosphere. However, some increase in the electricity consumption is expected due to the work input to the water-to-water heat pump.

Appendix 1: Conceptual design of common loop water source heat pump with heat storage



Appendix 2: Typical office floor layout with water source heat pumps

HVAC SYSTEM TYPICAL LAYOUT



Appendix 3: Building load from eQuest simulation

SPACE NAME	SPACE FLOOR	CLOUDING LOAD (KBTU/HR)	TIME OF PEAK	DRY-BULB	WET-BULB	HEATING LOAD (KBTU/HR)	TIME OF PEAK	DRY-BULB	WET-BULB
EL1 South Perim Spc (G.S1)	1.	44.461	SEP 24 3 PM	57.F	46.F	-20.583	JAN 1 6 AM	-3.F	-3.F
EL1 East Perim Spc (G.E2)	1.	27.677	JUN 14 10 AM	65.F	53.F	-15.694	JAN 1 6 AM	-3.F	-3.F
EL1 North Perim Spc (G.N3)	1.	21.484	JUN 11 4 PM	86.F	69.F	-25.001	JAN 1 6 AM	-3.F	-3.F
EL1 West Perim Spc (G.W4)	1.	24.822	JUL 10 7 PM	80.F	63.F	-16.550	JAN 1 6 AM	-3.F	-3.F
EL1 Core Spc (G.C5)	1.	185.955	SEP 3 4 PM	77.F	67.F	-1.879	JAN 1 6 AM	-3.F	-3.F
EL1 South Perim Plnm (G.S6)	1.	1.423	AUG 3 6 PM	87.F	67.F	-3.725	JAN 27 8 AM	-3.F	-4.F
EL1 East Perim Plnm (G.E7)	1.	1.030	JUL 8 5 PM	88.F	75.F	-2.597	JAN 27 8 AM	-3.F	-4.F
EL1 North Perim Plnm (G.N8)	1.	1.070	JUL 8 6 PM	88.F	75.F	-3.944	JAN 27 8 AM	-3.F	-4.F
EL1 West Perim Plnm (G.W9)	1.	0.822	JUL 8 6 PM	88.F	75.F	-2.589	JAN 27 11 AM	0.F	-1.F
EL1 Core Plnm (G.C10)	1.	0.132	AUG 3 3 PM	91.F	71.F	-0.471	JAN 27 9 AM	-3.F	-4.F
EL1 South Perim Spc (M.S11)	1.	68.079	SEP 28 3 PM	57.F	46.F	-22.515	JAN 1 8 AM	-3.F	-1.F
EL1 East Perim Spc (M.E12)	1.	43.725	MAY 7 10 AM	54.F	42.F	-15.854	JAN 1 6 AM	-3.F	-3.F
EL1 North Perim Spc (M.N13)	1.	32.413	JUN 11 4 PM	86.F	69.F	-24.211	JAN 1 6 AM	-3.F	-3.F
EL1 West Perim Spc (M.W14)	1.	39.007	APR 14 6 PM	63.F	47.F	-16.251	JAN 1 6 AM	-3.F	-3.F
EL1 Core Spc (M.C15)	1.	217.177	JUL 8 4 PM	90.F	75.F	0.000	0.F	0.F	0.F
EL1 South Perim Plnm (M.S16)	1.	1.423	AUG 3 6 PM	87.F	67.F	-3.725	JAN 27 8 AM	-3.F	-4.F
EL1 East Perim Plnm (M.E17)	1.	1.030	JUL 8 5 PM	86.F	75.F	-2.597	JAN 27 8 AM	-3.F	-4.F
EL1 North Perim Plnm (M.N18)	1.	1.070	JUL 8 6 PM	88.F	75.F	-3.944	JAN 27 8 AM	-3.F	-4.F
EL1 West Perim Plnm (M.W19)	1.	0.822	JUL 8 6 PM	88.F	75.F	-2.589	JAN 27 11 AM	0.F	-1.F
EL1 Core Plnm (M.C20)	1.	0.132	AUG 3 3 PM	91.F	71.F	-22.515	JAN 1 8 AM	0.F	-1.F
EL1 South Perim Spc (T.S21)	1.	68.079	SEP 28 3 PM	57.F	46.F	-15.854	JAN 1 6 AM	-3.F	-3.F
EL1 East Perim Spc (T.E22)	1.	43.725	MAY 7 10 AM	54.F	42.F	-24.211	JAN 1 6 AM	-3.F	-3.F
EL1 North Perim Spc (T.N23)	1.	32.413	JUN 11 4 PM	86.F	69.F	-24.984	JAN 1 5 AM	-1.F	-2.F
EL1 West Perim Spc (T.W24)	1.	39.007	APR 14 6 PM	63.F	47.F	-8.148	JAN 27 11 AM	0.F	-1.F
EL1 Core Spc (T.C25)	1.	258.234	JUL 6 4 PM	84.F	69.F	-5.409	FEB 4 8 AM	2.F	1.F
EL1 South Perim Plnm (T.S26)	1.	3.136	AUG 3 7 PM	87.F	68.F	-8.476	JAN 27 11 AM	0.F	-1.F
EL1 East Perim Plnm (T.E27)	1.	2.079	JUL 6 7 PM	80.F	70.F	-5.467	JAN 1 12 NOON	0.F	-1.F
EL1 North Perim Plnm (T.N28)	1.	2.783	AUG 5 7 PM	86.F	73.F	-25.648	JAN 1 12 NOON	1.F	0.F
EL1 West Perim Plnm (T.W29)	1.	2.051	JUL 6 9 PM	74.F	68.F	-----	-----	-----	-----
EL1 Core Plnm (T.C30)	1.	11.276	JUL 6 9 PM	74.F	68.F	-----	-----	-----	-----
SUM		1176.540				-342.156			

SUM

BUILDING PEAK

1009.421 JUN 11 4 PM 86.F 69.F -261.868 JAN 1 6 AM -3.F -3.F

REPORT- ISS-B Space Peak Load Components EL-1 East Perim Spc (G-E2)

卷之三

SPACE E11 East Perim Spc (G.E2) SPACE TEMPERATURE USED FOR THE LOADS CALCULATION IS 70 F / 21 C

MULTIPLIER	1.0	FLOOR	MULTIPLIER	1.0
FLOOR	AREA	1507	SQFT	140
VOLUME		15063	CUFT	427

TIME	COOLING LOAD		HEATING LOAD	
	JUN 14 10AM	65 F 53 F 198 BTU/H. SQFT 4.7 KTS 1 KI	18 C 12 C 624 W/M2 2.4 M/S	JAN 1 6AM
DRY-BULB TEMP WET-BULB TEMP TOTAL HORIZONTAL SOLAR RAD WIND SPEED AT SPACE CLOUD AMOUNT (0 CLEAR) -10	-19 C -19 C 0 W/M2 3.8 M/S			

	SENSIBLE (BTU/H)	LATENT (BTU/H)	(KW)	(KW)	(KW)	SENSIBLE (BTU/H)	LATENT (BTU/H)	(KW)	(KW)
WALL CONDUCTION	0.222	0.065	0.000	0.000	-	-	-	-	-
ROOF CONDUCTION	0.000	0.000	0.000	0.000	-	-	-	-	-
WINDOW GLASS-FRM COND	-1.446	-0.424	0.000	0.000	-	-	-	-	-
WINDOW GLASS SOLAR	26.362	7.724	0.000	0.000	-	-	-	-	-
DOOR CONDUCTION	0.000	0.000	0.000	0.000	-	-	-	-	-
INTERNAL SURFACE COND	0.000	0.000	0.000	0.000	-	-	-	-	-
UNDERGROUND SURF COND	-0.858	-0.251	0.000	0.000	-	-	-	-	-
OCCUPANTS TO SPACE	2.230	0.653	2.907	0.852	-	-	-	-	-
LIGHT TO SPACE	0.038	0.111	0.000	0.000	-	-	-	-	-
EQUIPMENT TO SPACE	1.245	0.365	0.000	0.000	-	-	-	-	-
PROCESS TO SPACE	0.000	0.000	0.000	0.000	-	-	-	-	-
INFILTRATION	-0.115	-0.034	0.000	0.000	-	-	-	-	-
TOTAL / AREA	27.677	8.109	2.907	0.852	-	-	-	-	-
TOTAL LOAD	30.584	KBTU/H		8.961	KW			-15.694	-4.598
								-0.010	-0.033
								-15.694	-4.598

* NOTE 1) THE ABOVE LOADS EXCLUDE OUTSIDE VENTILATION AIR
 * --- LOADS *
 * 2) TIMES GIVEN IN STANDARD TIME FOR THE LOCATION
 * IN CONSIDERATION *
 * 3) THE ABOVE LOADS ARE CALCULATED ASSUMING A
 * CONSTANT INDOOR SPACE TEMPERATURE *
 * *

Base Case Model-1

DOE-2.2-48r 5/01/2016 20:26:47 BDL RUN 3

REPORT- LS-B Space Peak Load Components EII North Perim Spc (G.N3)

WEATHER FILE- Toronto ON CWEC

SPACE EII North Perim Spc (G.N3)
SPACE TEMPERATURE USED FOR THE LOADS CALCULATION IS 70 F / 21 C

MULTIPLIER 1.0 FLOOR MULTIPLIER 1.0

FLOOR AREA 2373 SQFT 220 M2
VOLUME 23730 CUFT 672 M3

COOLING LOAD

TIME JUN 11 4PM

DRY-BULB TEMP 96 F 30 C
WET-BULB TEMP 69 F 21 C
TOT HORIZONTAL SOLAR RAD 216 BTU/H.SQFT 680 W/M2
WIND SPEED AT SPACE 10.0 KTS 5.2 M/S
CLOUD AMOUNT 0 (CLEAR) -10 6

HEATING LOAD

TIME JAN 1 6AM

SENSIBLE

(BTU/H) (KW)

LATENT

(BTU/H) (KW)

SENSIBLE

(BTU/H) (KW)

LATENT

(BTU/H) (KW)

WALL CONDUCTION	0.731	0.214	0.000	0.000
ROOF CONDUCTION	0.000	0.000	0.000	0.000
WINDOW GLASS-FRM COND	2.996	0.878	0.000	0.000
WINDOW GLASS SOLAR	11.692	3.426	0.000	0.000
DOOR CONDUCTION	0.000	0.000	0.000	0.000
INTERNAL SURFACE COND	0.000	0.000	0.000	0.000
UNDERGROUND SURF COND	-1.288	-0.377	0.000	0.000
OCCUPANTS TO SPACE	4.139	1.213	4.578	1.341
LIGHT TO SPACE	0.103	0.030	0.000	0.000
EQUIPMENT TO SPACE	2.088	0.612	0.000	0.000
PROCESS TO SPACE	0.000	0.000	0.000	0.000
INFILTRATION	1.024	0.300	0.767	0.225
TOTAL	21.484	6.295	5.345	1.566
TOTAL / AREA	0.009	0.029	0.002	0.007

TOTAL LOAD	26.829	KBTU/H	7.861	KW
TOTAL LOAD / AREA	11.31	BTU/H.SQFT	35.657	W/M2

-25.001 KBTU/H

10.536 BTU/H.SQFT

-7.325 KW

33.228 W/M2

SPACE EII West Perim Spc (G.W4)
SPACE TEMPERATURE USED FOR THE LOADS CALCULATION IS 70 F / 21 C

MULTIPLIER	1.0	FLOOR MULTIPLIER	1.0
FLOOR AREA	1507 SQFT	140 M2	
VOLUME	15068 CUFT	427 M3	
TIME	Cooling Load	Heating Load	
	JUL 10 7PM	JAN 1 6AM	
DRY-BULB TEMP	80 F	27 C	-3 F
WET-BULB TEMP	63 F	17 C	-3 F
TOT HORIZONTAL SOLAR RAD	117 BTU/H.SQFT	3.68 W/M2	0 BTU/H.SQFT
WIND SPEED AT SPACE	6.0 KTS	3.1 M/S	7.4 KTS
CLOUD AMOUNT 0 (CLEAR)	0	0	3.8 M/S
CLOUD AMOUNT -10	7	7	7

(BTU/H)	SENSIBLE (KW)	LATENT (BTU/H)	SENSIBLE (Kw)
---	---	---	---
WALL CONDUCTION	0.781	0.229	0.000
ROOF CONDUCTION	0.000	0.000	0.000
WINDOW GLASS-FRM COND	1.220	0.357	0.000
WINDOW GLASS SOLAR	22.940	6.722	0.000
DOOR CONDUCTION	0.000	0.000	0.000
INTERNAL SURFACE COND	0.000	0.000	0.000
INTERNAL SURFACE COND	-0.622	-0.182	0.000
UNDERGROUND SURF COND	0.116	0.034	0.000
OCCUPANTS TO SPACE	0.041	0.012	0.000
LIGHT TO SPACE	0.119	0.035	0.000
EQUIPMENT TO SPACE	0.000	0.000	0.000
PROCESS TO SPACE	0.228	0.067	0.000
INFILTRATION	---	---	---
TOTAL	24.822	7.273	0.000
TOTAL / AREA	0.016	0.052	0.000
TOTAL LOAD	24.822 BTU/H	7.273 KW	-16.550 BTU/H
TOTAL LOAD / AREA	16.47 BTU/H.SQFT	51.956 W/M2	10.984 BTU/H.SQFT
			-4.849 KW
			34.642 W/M2

* NOTE 1) THE ABOVE LOADS EXCLUDE OUTSIDE VENTILATION AIR
* --- LOADS
* 2) TIMES GIVEN IN STANDARD TIME FOR THE LOCATION
* IN CONSIDERATION
* 3) THE ABOVE LOADS ARE CALCULATED ASSUMING A
* CONSTANT INDOOR SPACE TEMPERATURE

SPACE EII Core Spc (G.C5)
SPACE TEMPERATURE USED FOR THE LOADS CALCULATION IS 70 F / 21 C

MULTIPLIER	1.0	FLOOR MULTIPLIER	1.0
FLOOR AREA	12236 SQFT	1.137 M2	
VOLUME	122364 CUFT	3465 M3	

TIME	COOLING LOAD			HEATING LOAD		
	SEP 3	4PM	JAN 1	6AM	JAN 1	6AM
DRY-BULB TEMP	77 F	25 C	-3 F	-19 C		
WET-BULB TEMP	67 F	19 C	-3 F	-19 C		
TOT HORIZONTAL SOLAR RAD	99 BTU/H.SQFT	312 W/M2	0 BTU/H.SQFT	0 W/M2		
WIND SPEED AT SPACE	8.0 KTS	4.1 M/S	7.4 KTS	3.8 M/S		
CLOUD AMOUNT 0 (CLEAR) -10	4		7			

(BTU/H)	SENSIBLE		(BTU/H)	LATENT		(BTU/H)	SENSIBLE	
	(KW)	(KW)		(BTU/H)	(KW)		(BTU/H)	(KW)
WALL CONDUCTION	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
ROOF CONDUCTION	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
WINDOW GLASS-FRM COND	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
WINDOW GLASS SOLAR	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
DOOR CONDUCTION	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
INTERNAL SURFACE COND	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
UNDERGROUND SURF COND	-1.372	-0.402	0.000	0.000	0.000	-3.929	-1.151	
OCCUPANTS TO SPACE	126.588	37.090	127.571	37.378	0.000	0.000	0.000	
LIGHT TO SPACE	34.704	10.168	0.000	0.000	0.000	0.676	0.198	
EQUIPMENT TO SPACE	25.994	7.616	0.000	0.000	0.000	1.834	0.537	
PROCESS TO SPACE	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
INFILTRATION	0.044	0.013	0.101	0.030	0.000	-0.460	-0.135	
TOTAL	185.958	54.486	127.671	37.408	-1.879	-0.550		
TOTAL / AREA	0.015	0.048	0.010	0.033	0.000	0.000		
TOTAL LOAD	313.629	91.893	KW		-1.879	KBTU/H	-0.550	KW
TOTAL LOAD / AREA	25.63	BTU/H.SQFT	80.835	W/M2	0.154	BTU/H.SQFT	0.484	W/M2

* NOTE 1) THE ABOVE LOADS EXCLUDE OUTSIDE VENTILATION AIR
* --- LOADS

* 2) TIMES GIVEN IN STANDARD TIME FOR THE LOCATION

* IN CONSIDERATION

* 3) THE ABOVE LOADS ARE CALCULATED ASSUMING A

* CONSTANT INDOOR SPACE TEMPERATURE

* *****

SPACE EII East Perim Plm (G.E7)
SPACE TEMPERATURE USED FOR THE LOADS CALCULATION IS 70 F / 21 C

MULTIPLIER	1.0	FLOOR MULTIPLIER	1.0
FLOOR AREA	1507 SQFT	140 M ²	
VOLUME	4520 CUFT	128 M ³	

TIME	COOLING LOAD			HEATING LOAD		
	JUL	8	5PM	JAN	27	8AM
DRY-BULB TEMP	98 F		31 C	-3 F		-19 C
WET-BULB TEMP	75 F		24 C	-4 F		-20 C
TOT HORIZONTAL SOLAR RAD	172 BTU/H.SQFT		542 W/M ²	4 BTU/H.SQFT		12 W/M ²
WIND SPEED AT SPACE	8.5 KTS		4.4 M/S	5.6 KTS		2.9 M/S
CLOUD AMOUNT 0 (CLEAR) -10	7		1			

	SENSIBLE (BTU/H)		LATENT (BTU/H)		SENSIBLE (BTU/H)	
	(KBTU/H)	(KW)	(KBTU/H)	(KW)	(KBTU/H)	(KW)
WALL CONDUCTION	0.723	0.212	0.000	0.000	-1.330	-0.390
ROOF CONDUCTION	0.000	0.000	0.000	0.000	0.000	0.000
WINDOW GLASS-FRM COND	0.000	0.000	0.000	0.000	0.000	0.000
WINDOW GLASS SOLAR	0.000	0.000	0.000	0.000	0.000	0.000
DOOR CONDUCTION	0.000	0.000	0.000	0.000	0.000	0.000
INTERNAL SURFACE COND	0.000	0.000	0.000	0.000	0.000	0.000
UNDERGROUND SURF COND	0.000	0.000	0.000	0.000	0.000	0.000
OCUPANTS TO SPACE	0.000	0.000	0.000	0.000	0.000	0.000
LIGHT TO SPACE	0.000	0.000	0.000	0.000	0.000	0.000
EQUIPMENT TO SPACE	0.000	0.000	0.000	0.000	0.000	0.000
PROCESS TO SPACE	0.000	0.000	0.000	0.000	0.000	0.000
INFILTRATION	0.307	0.090	0.535	0.157	-1.267	-0.371
TOTAL	1.030	0.302	0.535	0.157	-2.597	-0.761
TOTAL / AREA	0.001	0.002	0.000	0.001	-0.002	-0.005
TOTAL LOAD	1.565 KBTU/H		0.459 KW		-2.597 KBTU/H	
TOTAL LOAD / AREA	1.04 BTU/H.SQFT		3.276 W/M ²		1.724 BTU/H.SQFT	

* * NOTE 1) THE ABOVE LOADS EXCLUDE OUTSIDE VENTILATION AIR
* * --- LOADS
* * 2) TIMES GIVEN IN STANDARD TIME FOR THE LOCATION
* * IN CONSIDERATION
* * 3) THE ABOVE LOADS ARE CALCULATED ASSUMING A
* * CONSTANT INDOOR SPACE TEMPERATURE
* *

SPACE ELL North Perim Plnm (G.N8)
SPACE TEMPERATURE USED FOR THE LOADS CALCULATION IS 70 F / 21 C

MULTIPLIER 1.0 FLOOR MULTIPLIER 1.0

FLOOR AREA 2373 SQFT 220 M2
VOLUME 7119 CUFT 202 M3

TIME	COOLING LOAD		HEATING LOAD	
	JUL 8	6PM	JAN 27	8AM
DRY-BULB TEMP	98 F	31 C	-3 F	-19 C
WET-BULB TEMP	75 F	24 C	-4 F	-20 C
TOT HORIZONTAL SOLAR RAD	126 BTU/H.SQFT	397 W/M2	4 BTU/H.SQFT	12 W/M2
WIND SPEED AT SPACE	7.1 KTS	3.6 M/S	5.6 KTS	2.9 M/S
CLOUD AMOUNT 0 (CLEAR) -10	1			

	SENSIBLE (BTU/H)		LATENT (BTU/H)		SENSIBLE (BTU/H)	
	(KBTU/H)	(KW)	(KBTU/H)	(KW)	(KBTU/H)	(KW)
WALL CONDUCTION	0.611	0.179	0.000	0.000	-2.043	-0.599
ROOF CONDUCTION	0.000	0.000	0.000	0.000	0.000	0.000
WINDOW GLASS-FRM COND	0.000	0.000	0.000	0.000	0.000	0.000
WINDOW GLASS SOLAR	0.000	0.000	0.000	0.000	0.000	0.000
DOOR CONDUCTION	0.000	0.000	0.000	0.000	0.000	0.000
INTERNAL SURFACE COND	0.000	0.000	0.000	0.000	0.000	0.000
UNDERGROUND SURF COND	0.000	0.000	0.000	0.000	0.000	0.000
OCCUPANTS TO SPACE	0.000	0.000	0.000	0.000	0.000	0.000
LIGHT TO SPACE	0.000	0.000	0.000	0.000	0.000	0.000
EQUIPMENT TO SPACE	0.000	0.000	0.000	0.000	0.000	0.000
PROCESS TO SPACE	0.000	0.000	0.000	0.000	0.000	0.000
INFILTRATION	0.459	0.135	0.800	0.234	-1.901	-0.557
TOTAL	1.070	0.313	0.800	0.234	-3.944	-1.156
TOTAL / AREA	0.000	0.001	0.000	0.001	-0.002	-0.005
TOTAL LOAD	1.870	KBTU/H	0.548 KW	0.445 W/M2	-3.944 KBTU/H	-1.156 KW
TOTAL LOAD / AREA	0.79	BTU/H.SQFT			1.662 BTU/H.SQFT	5.242 W/M2

* * NOTE 1) THE ABOVE LOADS EXCLUDE OUTSIDE VENTILATION AIR
* * --- LOADS
* * 2) TIMES GIVEN IN STANDARD TIME FOR THE LOCATION
* * IN CONSIDERATION
* * 3) THE ABOVE LOADS ARE CALCULATED ASSUMING A
* * CONSTANT INDOOR SPACE TEMPERATURE
* *

Base Case Model-1

DOE-2.2-48r 5/01/2016 20:26:47 BDL RUN 3

卷之三

WEATHER FILE - 1888 ON CWEC

SPACE ELL West Perim Plm (G.W9)
SPACE TEMPERATURE USED FOR THE LOADS CALCULATION IS 70 F / 21 C

MULTIPLIER	1.0	FLOOR	MULTIPLIER	1.0
AREA	1507 4520	SQFT CUTY	140 128	M2 M3
VOLUME				

TIME	COOLING LOAD		HEATING LOAD	
	JUL 8	6PM	JAN 27	11AM
DRY-BULB TEMP	88 F	31 C	0 F	-18 C
WET-BULB TEMP	75 F	24 C	-1 F	-18 C
HORIZONTAL SOLAR RAD	126 BTU/H. SQFT	397 W/M2	115 BTU/H. SQFT	362 W/M2
WIND SPEED AT SPACE	7.1 KTS	3.6 M/S	2.8 KTS	1.5 M/S
CLOUD AMOUNT (0 CLEAR) -10	1			

	SENSIBLE (BTU/H)	LATENT (BTU/H)	SENSIBLE (BTU/H)	LATENT (BTU/H)
	(KW)	(KW)	(KW)	(KW)
WALL CONDUCTION	0.516	0.151	0.000	0.000
ROOF CONDUCTION	0.000	0.000	0.000	0.000
WINDOW GLASS-FRM COND	0.000	0.000	0.000	0.000
WINDOW GLASS SOLAR	0.000	0.000	0.000	0.000
DOOR CONDUCTION	0.000	0.000	0.000	0.000
INTERNAL SURFACE COND	0.000	0.000	0.000	0.000
UNDERGROUND SURF COND	0.000	0.000	0.000	0.000
OCCUPANTS TO SPACE	0.000	0.000	0.000	0.000
LIGHT TO SPACE	0.000	0.000	0.000	0.000
EQUIPMENT TO SPACE	0.000	0.000	0.000	0.000
PROCESS TO SPACE	0.000	0.000	0.000	0.000
INFILTRATION	0.306	0.090	0.533	0.156
TOTAL / AREA	0.822	0.241	0.533	0.156
TOTAL LOAD	1.355	0.002	0.000	0.001
			0.397	KW
			-2.589	KBTU/H

* * * * *

* * * * *

NOTE 1) THE ABOVE LOADS EXCLUDE OUTSIDE VENTILATION AIR
TONS

* * * * *

U.S. CONSTITUTION FOR THE LOCATION *

* * * * * 3) THE ABOVE LOADS ARE CALCULATED ASSUMING A

* * * * *

* * * * *

Base Case Model-1

DOE-2.2-48r 5/01/2016 20:26:47 BDL RUN 3

REPORT- LS-B Space Peak Load Components EII South Perim Spc (M.S11) WEATHER FILE- Toronto ON CWEC

SPACE EII South Perim Spc (M.S11)
SPACE TEMPERATURE USED FOR THE LOADS CALCULATION IS 70 F / 21 C

MULTIPLIER	1.0	FLOOR MULTIPLIER	1.0
FLOOR AREA	2373 SQFT	220 M2	
VOLUME	23730 CUFT	672 M3	

TIME	COOLING LOAD			HEATING LOAD		
	SEP 28	3PM		JAN 1	8AM	
DRY-BULB TEMP	57 F	14 C	0 F	-18 C		
WET-BULB TEMP	46 F	8 C	-1 F	-18 C		
TOT HORIZONTAL SOLAR RAD	21.6 BTU/H.SQFT	680 W/M2	1 BTU/H.SQFT	3 W/M2		
WIND SPEED AT SPACE	8.7 KTS	4.5 M/S	10.7 KTS	5.5 M/S		
CLOUD AMOUNT 0 (CLEAR) -10	1		4			

	SENSIBLE (BTU/H)	LATENT (BTU/H)	SENSIBLE (BTU/H)	LATENT (KW)
	(KW)	(KW)	(KW)	(KW)
WALL CONDUCTION	0.336	0.198	0.000	0.000
ROOF CONDUCTION	0.000	0.000	0.000	0.000
WINDOW GLASS-FRM COND	-4.070	-1.193	0.000	0.000
WINDOW GLASS SOLAR	60.-205	17.640	0.000	0.000
DOOR CONDUCTION	0.000	0.000	0.000	0.000
INTERNAL SURFACE COND	0.000	0.000	0.000	0.000
UNDERGROUND SURF COND	0.000	0.000	0.000	0.000
OCCUPANTS TO SPACE	7.728	2.264	6.637	1.945
LIGHT TO SPACE	0.161	0.047	0.000	0.000
EQUIPMENT TO SPACE	4.166	1.221	0.000	0.000
PROCESS TO SPACE	0.000	0.000	0.000	0.000
INFILTRATION	-0.445	-0.130	0.000	0.000
TOTAL	68.079	19.947	6.637	1.945
TOTAL / AREA	0.029	0.090	0.003	0.009
TOTAL LOAD	74.716	KBTU/H	21.892	KW
TOTAL LOAD / AREA	31.49	BTU/H.SQFT	99.301	W/M2

-22.515 KW
9.488 BTU/H.SQFT

SPACE EII East Perim Spc (M.E12)
SPACE TEMPERATURE USED FOR THE LOADS CALCULATION IS 70 F / 21 C

MULTIPLIER	1.0	FLOOR MULTIPLIER	1.0
FLOOR AREA	1507 SQFT	140 M2	
VOLUME	15068 CUFT	427 M3	

TIME	COOLING LOAD			HEATING LOAD		
	MAY 7 10AM			JAN 1 6AM		
DRY-BULB TEMP	54 F	12 C		-3 F	-19 C	
WET-BULB TEMP	42 F	6 C		-3 F	-19 C	
TOT HORIZONTAL SOLAR RAD	19.4 BTU/H.SQFT	611 W/M2		0 BTU/H.SQFT	0 W/M2	
WIND SPEED AT SPACE	4.0 KTS	2.1 M/S		7.4 KTS	3.8 M/S	
CLOUD AMOUNT 0 (CLEAR) -10	1			7		

	SENSIBLE (BTU/H)	LATENT (BTU/H)	SENSIBLE (BTU/H)	LATENT (BTU/H)
---	---	---	---	---
WALL CONDUCTION	-0.130	-0.138	0.000	0.000
ROOF CONDUCTION	0.000	0.000	0.000	0.000
WINDOW GLASS-FRM COND	-3.173	-0.930	0.000	0.000
WINDOW GLASS SOLAR	40.279	11.502	0.000	0.000
DOOR CONDUCTION	0.000	0.000	0.000	0.000
INTERNAL SURFACE COND	0.000	0.000	0.000	0.000
UNDERGROUND SURF COND	0.000	0.000	0.000	0.000
OCCUPANTS TO SPACE	4.512	1.322	4.214	1.235
LIGHT TO SPACE	0.051	0.015	0.000	0.000
EQUIPMENT TO SPACE	2.551	0.747	0.000	0.000
PROCESS TO SPACE	0.000	0.000	0.000	0.000
INFILTRATION	-0.365	-0.107	0.000	0.000
TOTAL	43.725	12.811	4.214	1.235
TOTAL / AREA	0.029	0.092	0.003	0.009
TOTAL LOAD	47.939 BTU/H	14.046 KW		
TOTAL LOAD / AREA	31.82 BTU/H.SQFT	100.342 W/M2		
			-15.854 BTU/H	-4.645 KW
			10.522 BTU/H.SQFT	33.185 W/M2

- * * NOTE 1) THE ABOVE LOADS EXCLUDE OUTSIDE VENTILATION AIR
- * --- LOADS
- * 2) TIMES GIVEN IN STANDARD TIME FOR THE LOCATION
- * IN CONSIDERATION
- * 3) THE ABOVE LOADS ARE CALCULATED ASSUMING A
- * CONSTANT INDOOR SPACE TEMPERATURE

Base Case Modell-1

DOE-2.2-48r 5/01/2016 20:26:47 BDL RUN 3

REPORT- LS-B Space Peak Load Components EII North Perim SPC (M.11.3) WEATHER FILE- TORONTO ON CWEC

- 1 -

SPACE E11 North Perim Spc (M.N13) SPACE TEMPERATURE USED FOR THE LOADS CALCULATION IS 70 F / 21 C

MULTIPLIER	1.0	FLOOR AREA	237.3	SQFT	220	FLOOR MULTIPLIER	1.0
FLOOR	1	AREA	237.30	CURRENT	67.72		
STORY TYPE							

TIME	COOLING LOAD		HEATING LOAD	
	JUN 11 4PM	JAN 1 6AM	JAN 1 6AM	JAN 1 6AM
DRY-BULB TEMP	86 F	30 C	-3 F	-19 C
WET-BULB TEMP	69 F	21 C	-3 F	-19 C
TOT HORIZONTAL SOLAR RAD	216 BTU/H. SQFT	680 W/M2	0 BTU/H. SQFT	0 W/M2
WIND SPEED AT SPACE	10.0 KTS	5.2 M/S	7.4 KTS	3.8 M/S
CLOUD AMOUNT (0=CLEAR) -10	6	7		

WALL CONDUCTION	0.748	0.219	0.000	0.000	-3.360	-0.984
ROOF CONDUCTION	0.000	0.000	0.000	0.000	0.000	0.000
WINDOW GLASS+FRM COND	3.529	1.034	0.000	0.000	-19.000	-5.567
WINDOW GLASS SOLAR	14.948	4.380	0.000	0.000	0.213	0.063
DOOR CONDUCTION	0.000	0.000	0.000	0.000	0.000	0.000
INTERNAL SURFACE COND	0.000	0.000	0.000	0.000	0.000	0.000
UNDERGROUND SURF COND	0.000	0.000	0.000	0.000	0.000	0.000
OCCUPANTS TO SPACE	7.939	2.326	6.637	1.345	0.000	0.000
LIGHT TO SPACE	0.044	0.013	0.000	0.000	0.130	0.038
EQUIPMENT TO SPACE	4.182	1.225	0.000	0.000	0.280	0.082
PROCESS TO SPACE	0.000	0.000	0.000	0.000	0.000	0.000
INFILTRATION	1.024	0.300	0.767	0.225	-2.475	-0.725
TOTAL / AREA	32.413	9.497	7.404	2.169	-24.211	-7.094
TOTAL LOAD	39.817	KBTU/H	11.666	KW	-24.211	KBTU/H
TOTAL / AREA	32.413	KBTU/H	11.666	KW	-24.211	KBTU/H

* * * * *

* * *

VENTILATION AIR

THE LOCATION *

ASSUMING A *

* +

* * * *

SPACE EII West Perim Spc (M.WL4)

SPACE TEMPERATURE USED FOR THE LOADS CALCULATION IS 70 F / 21 C

MULTIPLIER	1.0	FLOOR MULTIPLIER	1.0
FLOOR AREA	1507 SQFT	140 M2	
VOLUME	15068 CUFT	427 M3	

TIME	COOLING LOAD			HEATING LOAD		
	APR 14	6PM		JAN 1	6AM	
DRY-BULB TEMP	63 F	17 C		-3 F	-19 C	
WET-BULB TEMP	47 F	8 C		-3 F	-19 C	
TOT HORIZONTAL SOLAR RAD	13.7 BTU/H.SQFT	431 W/M2		0 BTU/H.SQFT	0 W/M2	
WIND SPEED AT SPACE	19.4 KTS	10.0 M/S		7.4 KTS	3.8 M/S	
CLOUD AMOUNT 0 (CLEAR) -10	2			7		

	SENSIBLE		LATENT	SENSIBLE	
	(BTU/H)	(KW)	(BTU/H)	(KW)	(BTU/H)
WALL CONDUCTION	-0.166	-0.049	0.000	0.000	-2.176
ROOF CONDUCTION	0.000	0.000	0.000	0.000	0.000
WINDOW GLASS-FRM COND	-1.490	-0.437	0.000	0.000	-12.906
WINDOW GLASS SOLAR	36.701	10.753	0.000	0.000	0.065
DOOR CONDUCTION	0.000	0.000	0.000	0.000	0.000
INTERNAL SURFACE COND	0.000	0.000	0.000	0.000	0.000
UNDERGROUND SURF COND	0.000	0.000	0.000	0.000	0.000
OCCUPANTS TO SPACE	2.658	0.779	1.391	0.407	0.000
LIGHT TO SPACE	0.063	0.019	0.000	0.000	0.024
EQUIPMENT TO SPACE	1.637	0.480	0.000	0.000	0.052
PROCESS TO SPACE	0.000	0.000	0.000	0.000	0.000
INFILTRATION	-0.397	-0.116	0.000	0.000	-1.650
TOTAL	39.007	11.429	1.391	0.407	-16.251
TOTAL / AREA	0.026	0.082	0.001	0.003	-0.011
TOTAL LOAD	40.397	KBTU/H	11.836 KW		-16.251 KBTU/H
TOTAL LOAD / AREA	26.81	BTU/H.SQFT	84.557 W/M2		10.786 BTU/H.SQFT

* NOTE 1) THE ABOVE LOADS EXCLUDE OUTSIDE VENTILATION AIR

* --- LOADS

* 2) TIMES GIVEN IN STANDARD TIME FOR THE LOCATION

* IN CONSIDERATION

* 3) THE ABOVE LOADS ARE CALCULATED ASSUMING A

* CONSTANT INDOOR SPACE TEMPERATURE

SPACE EII Core Spc (M.C15)
SPACE TEMPERATURE USED FOR THE LOADS CALCULATION IS 70 F / 21 C

MULTIPLIER	1.0	FLOOR MULTIPLIER	1.0
FLOOR AREA	12236 SQFT	1.137 M2	
VOLUME	122364 CUFT	3465 M3	
TIME	COOLING LOAD	HEATING LOAD	
	JUL 8 4PM		=====

DRY-BULB TEMP 90 F 32 C
WET-BULB TEMP 75 F 24 C
TOT HORIZONTAL SOLAR RAD 223 BTU/H.SQFT 703 W/M2
WIND SPEED AT SPACE 6.7 KTS 3.4 M/S
CLOUD AMOUNT 0 (CLEAR) -10 4

	SENSIBLE (BTU/H)	(KW)	LATENT (BTU/H)	(KW)	SENSIBLE (BTU/H)	(KW)
WALL CONDUCTION	0.000	0.000	0.000	0.000	0.000	0.000
ROOF CONDUCTION	0.000	0.000	0.000	0.000	0.000	0.000
WINDOW GLASS-FRM COND	0.000	0.000	0.000	0.000	0.000	0.000
WINDOW GLASS SOLAR	0.000	0.000	0.000	0.000	0.000	0.000
DOOR CONDUCTION	0.000	0.000	0.000	0.000	0.000	0.000
INTERNAL SURFACE COND	0.000	0.000	0.000	0.000	0.000	0.000
INTERNAL SURFACE COND	0.000	0.000	0.000	0.000	0.000	0.000
UNDERGROUND SURF COND	149.447	43.788	127.571	37.378		
OCCUPANTS TO SPACE						
LIGHT TO SPACE	40.170	11.770	0.000	0.000	0.000	0.000
EQUIPMENT TO SPACE	27.433	8.038	0.000	0.000	0.000	0.000
PROCESS TO SPACE	0.000	0.000	0.000	0.000	0.000	0.000
INFILTRATION	0.127	0.037	0.183	0.054	0.000	0.000
TOTAL	217.177	63.633	127.754	37.432		
TOTAL / AREA	0.018	0.056	0.010	0.033	0.000	0.000
TOTAL LOAD	344.931	KBTU/H	101.065 KW		0.000 KBTU/H	0.000 KW
TOTAL LOAD / AREA	28.19	BTU/H.SQFT	88.903 W/M2		0.000 BTU/H.SQFT	0.000 W/M2

* * NOTE 1) THE ABOVE LOADS EXCLUDE OUTSIDE VENTILATION AIR
* * --- LOADS *
* * 2) TIMES GIVEN IN STANDARD TIME FOR THE LOCATION *
* * IN CONSIDERATION *
* * 3) THE ABOVE LOADS ARE CALCULATED ASSUMING A *
* * CONSTANT INDOOR SPACE TEMPERATURE *

Base Case Model 1-1

DOE-2.2-48r 5/01/2016 20:26:47 BDL RUN 3

REPORT- U.S.-R Space peak Load Components E.I. East Perim Blm (M E17)

卷之三

SPACE ELL East Perim Plmn (M.E17)
SPACE TEMPERATURE USED FOR THE LOADS CALCULATION IS 70 F / 21 C

卷之三

MULTIPLIER	1.0	FLOOR MULTIPLIER	1.0
FLOOR AREA	1507	SOFT	140
	1507		M2

TIME	COOLING LOAD			HEATING LOAD		
	JUL 8	5PM		JAN 27	8AM	
DRY-BULB TEMP	88 F		31 C	-3 F		-19 C
WET-BULB TEMP	75 F		24 C	-4 F		-20 C
TOT HORIZONTAL SOLAR RAD	172 BTU/H. SQFT		542 W/M2	4 BTU/H. SQFT		12 W/M2
WIND SPEED AT 8' (CLEAR)	8.5 KTS		4.4 M/S	5.6 KTS		2.9 M/S
CLOUD COUNT (CLEAR)	10			1		

	SENSIBLE (BTU/H)	LATENT (BTU/H)	SENSIBLE (BTU/H)	LATENT (BTU/H)
	(kW)	(kW)	(kW)	(kW)
WALL CONDUCTION	0.723	0.212	0.000	0.000
ROOF CONDUCTION	0.000	0.000	0.000	-1.330
WINDOW GLASS+FRM COND	0.000	0.000	0.000	0.000
WINDOW GLASS SOLAR	0.000	0.000	0.000	0.000
DOOR CONDUCTION	0.000	0.000	0.000	0.000
INTERNAL SURFACE COND	0.000	0.000	0.000	0.000
UNDERGROUND SURF COND	0.000	0.000	0.000	0.000
OCCUPANTS TO SPACE	0.000	0.000	0.000	0.000
LIGHT TO SPACE	0.000	0.000	0.000	0.000
EQUIPMENT TO SPACE	0.000	0.000	0.000	0.000
PROCESS TO SPACE	0.000	0.000	0.000	0.000
INFILTRATION	0.307	0.090	0.535	0.157
TOTAL / AREA	1.030	0.302	0.535	0.157
TOTAL LOAD	1.565	KBTU/H	0.459	kW
			-2.597	KBTU/H
			-0.002	-0.005
			-0.761	-0.761

* * * * *

* * * * *

NOTE 1) THE ABOVE LOADS EXCLUDE OUTSIDE VENTILATION AIR
TONS

* * * * *

2) PATENTS CIVILIAN IN STANDARD TIME FOR THE LOCATION

LOAUS

U.S. CONSTITUTION FOR THE LOCATION *

* * * * * 3) THE ABOVE LOADS ARE CALCULATED ASSUMING A

* * * * *

* * * * *

SPACE EII North Perim Plnm (M.N18)
SPACE TEMPERATURE USED FOR THE LOADS CALCULATION IS 70 F / 21 C

MULTIPLIER 1.0 FLOOR MULTIPLIER 1.0

FLOOR AREA	2373 SQFT	220 M2
VOLUME	7119 CUFT	202 M3

COOLING LOAD

TIME	JUL 8 6PM	JAN 27 8AM
DRY-BULB TEMP	98 F	31 C
WET-BULB TEMP	75 F	24 C
TOT HORIZONTAL SOLAR RAD	126 BTU/H.SQFT	397 W/M2
WIND SPEED AT SPACE	7.1 KTS	3.6 M/S
CLOUD AMOUNT 0 (CLEAR)	10	1

HEATING LOAD

TIME	JUL 8 6PM	JAN 27 8AM
-3 F	-19 C	
-4 F	-20 C	
4 BTU/H.SQFT	12 W/M2	
5.6 KTS	2.9 M/S	

SENSIBLE

(BTU/H)

(KW)

(BTU/H)

(KW)

LATENT

(BTU/H)

(KW)

SENSIBLE

(BTU/H)

(KW)

(BTU/H)

(KW)

SENSIBLE

(BTU/H)

TOTAL LOAD / AREA	1.870 KBTU/H	0.548 KW	-3.944 KBTU/H
TOTAL LOAD / AREA	0.790 BTU/H.SQFT	2.455 W/M2	1.662 BTU/H.SQFT

---	---	---	---
---	---	---	---

---	---	---	---
---	---	---	---

---	---	---	---
---	---	---	---

---	---	---	---
---	---	---	---

---	---	---	---
---	---	---	---

---	---	---	---
---	---	---	---

---	---	---	---
---	---	---	---

---	---	---	---
---	---	---	---

---	---	---	---
---	---	---	---

---	---	---	---
---	---	---	---

---	---	---	---
---	---	---	---

---	---	---	---
---	---	---	---

---	---	---	---
---	---	---	---

---	---	---	---
---	---	---	---

<table border

SPACE EII West Perim Plm (M.W19)
SPACE TEMPERATURE USED FOR THE LOADS CALCULATION IS 70 F / 21 C

MULTIPLIER	1.0	FLOOR MULTIPLIER	1.0
FLOOR AREA	1507 SQFT	140 M2	
VOLUME	4520 CUFT	128 M3	

TIME	COOLING LOAD		HEATING LOAD	
	JUL 8	6PM	JAN 27	11AM
DRY-BULB TEMP	98 F	31 C	0 F	-18 C
WET-BULB TEMP	75 F	24 C	-1 F	-18 C
TOT HORIZONTAL SOLAR RAD	126 BTU/H.SQFT	397 W/M2	115 BTU/H.SQFT	362 W/M2
WIND SPEED AT SPACE	7.1 KTS	3.6 M/S	2.8 KTS	1.5 M/S
CLOUD AMOUNT 0 (CLEAR)	10	1	1	1

	SENSIBLE (BTU/H)	LATENT (BTU/H)	SENSIBLE (BTU/H)	LATENT (BTU/H)
	(KW)	(KW)	(KW)	(KW)
WALL CONDUCTION	0.516	0.151	0.000	0.000
ROOF CONDUCTION	0.000	0.000	0.000	0.000
WINDOW GLASS-FRM COND	0.000	0.000	0.000	0.000
WINDOW GLASS SOLAR	0.000	0.000	0.000	0.000
DOOR CONDUCTION	0.000	0.000	0.000	0.000
INTERNAL SURFACE COND	0.000	0.000	0.000	0.000
UNDERGROUND SURF COND	0.000	0.000	0.000	0.000
OCCUPANTS TO SPACE	0.000	0.000	0.000	0.000
LIGHT TO SPACE	0.000	0.000	0.000	0.000
EQUIPMENT TO SPACE	0.000	0.000	0.000	0.000
PROCESS TO SPACE	0.000	0.000	0.000	0.000
INFILTRATION	0.306	0.090	0.533	0.156
TOTAL	0.822	0.241	0.533	0.156
TOTAL / AREA	0.001	0.002	0.000	0.001
TOTAL LOAD	1.355	KBTU/H	0.397 KW	-2.589 KBTU/H
TOTAL LOAD / AREA	0.90	BTU/H.SQFT	2.836 W/M2	1.718 BTU/H.SQFT

* * NOTE 1) THE ABOVE LOADS EXCLUDE OUTSIDE VENTILATION AIR
* * --- LOADS
* * 2) TIMES GIVEN IN STANDARD TIME FOR THE LOCATION
* * IN CONSIDERATION
* * 3) THE ABOVE LOADS ARE CALCULATED ASSUMING A
* * CONSTANT INDOOR SPACE TEMPERATURE
* *

* * *****
* * *****

SPACE EII Core Plnm (M.C20)
SPACE TEMPERATURE USED FOR THE LOADS CALCULATION IS 70 F / 21 C

MULTIPLIER 1.0 FLOOR MULTIPLIER 1.0

FLOOR AREA 12236 SQFT 1137 M²
VOLUME 36709 CUFT 1040 M³

COOLING LOAD

TIME AUG 3 3PM

DRY-BULB TEMP 91 F 33 C
WET-BULB TEMP 71 F 22 C

TOT HORIZONTAL SOLAR RAD 263 BTU/H.SQFT 829 W/M²

WIND SPEED AT SPACE 7.1 KTS 3.6 M/S

CLOUD AMOUNT 0 (CLEAR) -10 4

HEATING LOAD

JAN 27 9AM

DRY-BULB TEMP -3 F -19 C
WET-BULB TEMP -4 F -20 C

TOT HORIZONTAL SOLAR RAD 30 BTU/H.SQFT 94 W/M²

WIND SPEED AT SPACE 6.4 KTS 3.3 M/S

CLOUD AMOUNT 1

SENSIBLE (BTU/H) (KW) LATENT (BTU/H) (KW)

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

*

SPACE EII East Perim Spc (T.E22)
SPACE TEMPERATURE USED FOR THE LOADS CALCULATION IS 70 F / 21 C

MULTIPLIER	1.0	FLOOR MULTIPLIER	1.0
FLOOR AREA	1507 SQFT	140 M2	
VOLUME	15068 CUFT	427 M3	

TIME	COOLING LOAD			HEATING LOAD		
	MAY 7 10AM			JAN 1 6AM		
DRY-BULB TEMP	54 F	12 C		-3 F	-19 C	
WET-BULB TEMP	42 F	6 C		-3 F	-19 C	
TOT HORIZONTAL SOLAR RAD	19.4 BTU/H.SQFT	611 W/M2		0 BTU/H.SQFT	0 W/M2	
WIND SPEED AT SPACE	4.0 KTS	2.1 M/S		7.4 KTS	3.8 M/S	
CLOUD AMOUNT 0 (CLEAR) -10	1			7		

	SENSIBLE (BTU/H)	LATENT (BTU/H)	SENSIBLE (BTU/H)	LATENT (BTU/H)
---	---	---	---	---
WALL CONDUCTION	-0.130	-0.138	0.000	0.000
ROOF CONDUCTION	0.000	0.000	0.000	0.000
WINDOW GLASS-FRM COND	-3.173	-0.930	0.000	0.000
WINDOW GLASS SOLAR	40.279	11.502	0.000	0.000
DOOR CONDUCTION	0.000	0.000	0.000	0.000
INTERNAL SURFACE COND	0.000	0.000	0.000	0.000
UNDERGROUND SURF COND	0.000	0.000	0.000	0.000
OCCUPANTS TO SPACE	4.512	1.322	4.214	1.235
LIGHT TO SPACE	0.051	0.015	0.000	0.000
EQUIPMENT TO SPACE	2.551	0.747	0.000	0.000
PROCESS TO SPACE	0.000	0.000	0.000	0.000
INFILTRATION	-0.365	-0.107	0.000	0.000
---	---	---	---	---
TOTAL	43.725	12.811	4.214	1.235
TOTAL / AREA	0.029	0.092	0.003	0.009
TOTAL LOAD	47.939 BTU/H	14.046 KW		
TOTAL LOAD / AREA	31.82 BTU/H.SQFT	100.342 W/M2		

	HEATING LOAD	VENTILATION AIR	W/M2
		*	*
		* NOTE 1) THE ABOVE LOADS EXCLUDE OUTSIDE VENTILATION AIR * --- LOADS	*

- * --- LOADS
- * 2) TIMES GIVEN IN STANDARD TIME FOR THE LOCATION
- * IN CONSIDERATION
- * 3) THE ABOVE LOADS ARE CALCULATED ASSUMING A
- * CONSTANT INDOOR SPACE TEMPERATURE

Base Case Model-1

DOE-2.2-48r 5/01/2016 20:26:47 BDL RUN 3

REPORT- LS-B Space Peak Load Components EII North Perim Spc (T.N23) WEATHER FILE- Toronto ON CWEC

SPACE EII North Perim Spc (T.N23)
SPACE TEMPERATURE USED FOR THE LOADS CALCULATION IS 70 F / 21 C

MULTIPLIER	1.0	FLOOR MULTIPLIER	1.0
FLOOR AREA	2373 SQFT	220 M2	
VOLUME	23730 CUFT	672 M3	
		COOLING LOAD	HEATING LOAD
TIME	JUN 11 4PM		JAN 1 6AM
DRY-BULB TEMP	96 F	30 C	-3 F
WET-BULB TEMP	69 F	21 C	-3 F
TOT HORIZONTAL SOLAR RAD	216 BTU/H.SQFT	680 W/M2	0 BTU/H.SQFT
WIND SPEED AT SPACE	10.0 KTS	5.2 M/S	7.4 KTS
CLOUD AMOUNT 0 (CLEAR)	10	6	7

	SENSIBLE (BTU/H)	LATENT (BTU/H)	SENSIBLE (BTU/H)	LATENT (BTU/H)
---	---	---	---	---
WALL CONDUCTION	0.748	0.219	0.000	0.000
ROOF CONDUCTION	0.000	0.000	0.000	0.000
WINDOW GLASS-FRM COND	3.529	1.034	0.000	0.000
WINDOW GLASS SOLAR	14.948	4.380	0.000	0.000
DOOR CONDUCTION	0.000	0.000	0.000	0.000
INTERNAL SURFACE COND	0.000	0.000	0.000	0.000
UNDERGROUND SURF COND	0.000	0.000	0.000	0.000
OCCUPANTS TO SPACE	7.939	2.326	6.637	1.945
LIGHT TO SPACE	0.044	0.013	0.000	0.000
EQUIPMENT TO SPACE	4.182	1.225	0.000	0.000
PROCESS TO SPACE	0.000	0.000	0.000	0.000
INFILTRATION	1.024	0.300	0.767	0.225
TOTAL	32.413	9.497	7.404	2.169
TOTAL / AREA	0.014	0.043	0.003	0.010
TOTAL LOAD	39.817 KBTU/H	11.666 KW	-24.211 KBTU/H	-7.094 KW
TOTAL LOAD / AREA	16.78 BTU/H.SQFT	52.919 W/M2	10.203 BTU/H.SQFT	32.175 W/M2

- *****
* * NOTE 1) THE ABOVE LOADS EXCLUDE OUTSIDE VENTILATION AIR
* * --- LOADS
* * 2) TIMES GIVEN IN STANDARD TIME FOR THE LOCATION
* * IN CONSIDERATION
* * 3) THE ABOVE LOADS ARE CALCULATED ASSUMING A
* * CONSTANT INDOOR SPACE TEMPERATURE
* * *****

SPACE EII West Perim Spc (T.W24)
SPACE TEMPERATURE USED FOR THE LOADS CALCULATION IS 70 F / 21 C

MULTIPLIER	1.0	FLOOR MULTIPLIER	1.0
FLOOR AREA	1507 SQFT	140 M ²	
VOLUME	15068 CUFT	427 M ³	

TIME	COOLING LOAD			HEATING LOAD		
	APR 14 6PM			JAN 1 6AM		
DRY-BULB TEMP	63 F	17 C		-3 F	-19 C	
WET-BULB TEMP	47 F	8 C		-3 F	-19 C	
TOT HORIZONTAL SOLAR RAD	13.7 BTU/H.SQFT	431 W/M ²		0 BTU/H.SQFT	0 W/M ²	
WIND SPEED AT SPACE	19.4 KTS	10.0 M/S		7.4 KTS	3.8 M/S	
CLOUD AMOUNT 0 (CLEAR) -10	2			7		

	SENSIBLE (BTU/H)	(KW)	LATENT (BTU/H)	(KW)	SENSIBLE (BTU/H)	(KW)
---	---	---	---	---	---	---
WALL CONDUCTION	-0.166	-0.049	0.000	0.000	-2.176	-0.638
ROOF CONDUCTION	0.000	0.000	0.000	0.000	0.000	0.000
WINDOW GLASS-FRM COND	-1.490	-0.437	0.000	0.000	-12.906	-3.781
WINDOW GLASS SOLAR	36.701	10.753	0.000	0.000	0.020	0.065
DOOR CONDUCTION	0.000	0.000	0.000	0.000	0.000	0.000
INTERNAL SURFACE COND	0.000	0.000	0.000	0.000	0.000	0.000
UNDERGROUND SURF COND	0.000	0.000	0.000	0.000	0.000	0.000
OCCUPANTS TO SPACE	2.658	0.779	1.391	0.407	0.000	0.000
LIGHT TO SPACE	0.063	0.019	0.000	0.000	0.082	0.024
EQUIPMENT TO SPACE	1.637	0.480	0.000	0.000	0.178	0.052
PROCESS TO SPACE	0.000	0.000	0.000	0.000	0.000	0.000
INFILTRATION	-0.397	-0.116	0.000	0.000	-1.650	-0.483
TOTAL	39.007	11.429	1.391	0.407	-16.251	-4.762
TOTAL / AREA	0.026	0.082	0.001	0.003	-0.011	-0.034
TOTAL LOAD	40.397	KBTU/H	11.836 KW		-16.251 KBTU/H	-4.762 KW
TOTAL LOAD / AREA	26.81 BTU/H.SQFT		84.557 W/M²		10.786 BTU/H.SQFT	34.016 W/M²

* * NOTE 1) THE ABOVE LOADS EXCLUDE OUTSIDE VENTILATION AIR
* * --- LOADS
* * 2) TIMES GIVEN IN STANDARD TIME FOR THE LOCATION
* * IN CONSIDERATION
* * 3) THE ABOVE LOADS ARE CALCULATED ASSUMING A
* * CONSTANT INDOOR SPACE TEMPERATURE
* * *****

SPACE EII Core Spc (T.C25)
SPACE TEMPERATURE USED FOR THE LOADS CALCULATION IS 70 F / 21 C

MULTIPLIER	1.0	FLOOR MULTIPLIER	1.0
FLOOR AREA	12236 SQFT	1.137 M2	
VOLUME	122364 CUFT	3465 M3	

TIME	COOLING LOAD			HEATING LOAD		
	JUL 6	4PM		JAN 1	5AM	
DRY-BULB TEMP	94 F	29 C		-1 F	-18 C	
WET-BULB TEMP	69 F	21 C		-2 F	-19 C	
TOT HORIZONTAL SOLAR RAD	245 BTU/H.SQFT	772 W/M2		0 BTU/H.SQFT	0 W/M2	
WIND SPEED AT SPACE	2.0 KTS	1.0 M/S		11.4 KTS	5.9 M/S	
CLOUD AMOUNT 0 (CLEAR) -10	3			6		

	SENSIBLE (BTU/H)	LATENT (BTU/H)	SENSIBLE (BTU/H)	LATENT (BTU/H)
	(KW)	(KW)	(KW)	(KW)
WALL CONDUCTION	0.000	0.000	0.000	0.000
ROOF CONDUCTION	0.039	0.012	0.000	0.000
WINDOW GLASS-FRM COND	7.125	2.088	0.000	0.000
WINDOW GLASS SOLAR	31.907	9.349	0.000	0.000
DOOR CONDUCTION	0.000	0.000	0.000	0.000
INTERNAL SURFACE COND	0.000	0.000	0.000	0.000
UNDERGROUND SURF COND	0.000	0.000	0.000	0.000
OCCUPANTS TO SPACE	151.370	44.352	127.571	37.378
LIGHT TO SPACE	40.261	11.797	0.000	0.000
EQUIPMENT TO SPACE	27.443	8.041	0.000	0.000
PROCESS TO SPACE	0.000	0.000	0.000	0.000
INFILTRATION	0.089	0.026	0.032	0.027
TOTAL	258.234	75.663	127.662	37.405
TOTAL / AREA	0.021	0.067	0.010	0.033
TOTAL LOAD	385.896 BTU/H	113.068 KW		-24.984 BTU/H
TOTAL LOAD / AREA	31.54 BTU/H.SQFT	99.461 W/M2		2.042 BTU/H.SQFT
				-7.320 KW
				6.439 W/M2

- *****
* * NOTE 1) THE ABOVE LOADS EXCLUDE OUTSIDE VENTILATION AIR
* * --- LOADS
* * 2) TIMES GIVEN IN STANDARD TIME FOR THE LOCATION
* * IN CONSIDERATION
* * 3) THE ABOVE LOADS ARE CALCULATED ASSUMING A
* * CONSTANT INDOOR SPACE TEMPERATURE
* * *****

SPACE EII South Perim Plnm (T.S26)
SPACE TEMPERATURE USED FOR THE LOADS CALCULATION IS 70 F / 21 C

MULTIPLIER 1.0 FLOOR MULTIPLIER 1.0

FLOOR AREA 2373 SQFT 220 M2
VOLUME 7119 CUFT 202 M3

COOLING LOAD

TIME AUG 3 7PM

DRY-BULB TEMP 87 F 31 C 0 F -18 C
WET-BULB TEMP 68 F 20 C -1 F -18 C
TOT HORIZONTAL SOLAR RAD 37 BTU/H.SQFT 116 W/M2 115 BTU/H.SQFT 362 W/M2
WIND SPEED AT SPACE 4.2 KTS 2.2 M/S 2.8 KTS 1.5 M/S
CLOUD AMOUNT 0 (CLEAR) -10 9 1

HEATING LOAD

TIME JAN 27 11AM

SENSIBLE (BTU/H) (KW)

LATENT (BTU/H) (KW)

COOLING LOAD

TIME AUG 3 7PM

DRY-BULB TEMP 87 F 31 C 0 F -18 C
WET-BULB TEMP 68 F 20 C -1 F -18 C
TOT HORIZONTAL SOLAR RAD 37 BTU/H.SQFT 116 W/M2 115 BTU/H.SQFT 362 W/M2
WIND SPEED AT SPACE 4.2 KTS 2.2 M/S 2.8 KTS 1.5 M/S
CLOUD AMOUNT 0 (CLEAR) -10 9 1

HEATING LOAD

TIME JAN 27 11AM

TOTAL 3.136 0.919 0.151 0.044 -8.148 -2.387
TOTAL / AREA 0.001 0.004 0.000 0.000 -0.003 -0.011

TOTAL LOAD 3.287 KBTU/H 0.963 KW -8.148 KBTU/H -2.387 KW
TOTAL LOAD / AREA 1.39 BTU/H.SQFT 4.369 W/M2 3.434 BTU/H.SQFT 10.829 W/M2

* NOTE 1) THE ABOVE LOADS EXCLUDE OUTSIDE VENTILATION AIR

* --- LOADS

* 2) TIMES GIVEN IN STANDARD TIME FOR THE LOCATION

* IN CONSIDERATION

* 3) THE ABOVE LOADS ARE CALCULATED ASSUMING A

* CONSTANT INDOOR SPACE TEMPERATURE

SPACE EII East Perim Plm (T.E27)
SPACE TEMPERATURE USED FOR THE LOADS CALCULATION IS 70 F / 21 C

MULTIPLIER	1.0	FLOOR MULTIPLIER	1.0
------------	-----	------------------	-----

FLOOR AREA	1507 SQFT	140 M ²
VOLUME	4520 CUFT	128 M ³

COOLING LOAD		
--------------	--	--

TIME	JUL 6 7PM	HEATING LOAD
------	-----------	--------------

DRY-BULB TEMP	90 F	27 C
WET-BULB TEMP	70 F	21 C
TOT HORIZONTAL SOLAR RAD	80 BTU/H.SQFT	252 W/M ²
WIND SPEED AT SPACE	4.2 KTS	2.2 M/S
CLOUD AMOUNT 0 (CLEAR) -10	6	2

SENSIBLE		
(BTU/H)	(KW)	(BTU/H)

---	---	---
-----	-----	-----

WALL CONDUCTION	0.634	0.186	0.000	0.000
ROOF CONDUCTION	1.317	0.386	0.000	0.000
WINDOW GLASS-FRM COND	0.000	0.000	0.000	0.000
WINDOW GLASS SOLAR	0.000	0.000	0.000	0.000
DOOR CONDUCTION	0.000	0.000	0.000	0.000
INTERNAL SURFACE COND	0.000	0.000	0.000	0.000
UNDERGROUND SURF COND	0.000	0.000	0.000	0.000
OCCUPANTS TO SPACE	0.000	0.000	0.000	0.000
LIGHT TO SPACE	0.000	0.000	0.000	0.000
EQUIPMENT TO SPACE	0.000	0.000	0.000	0.000
PROCESS TO SPACE	0.000	0.000	0.000	0.000
INFILTRATION	0.128	0.038	0.289	0.085

LATENT		
(BTU/H)	(KW)	(BTU/H)

---	---	---
-----	-----	-----

TOTAL	2.079	0.609	0.289	0.085
TOTAL / AREA	0.001	0.004	0.000	0.001
TOTAL LOAD	2.369	KBTU/H	0.694 KW	-5.409 KBTU/H
TOTAL LOAD / AREA	1.57	BTU/H.SQFT	4.938 W/M ²	3.590 BTU/H.SQFT

SENSIBLE		
(BTU/H)	(KW)	(BTU/H)

---	---	---
-----	-----	-----

WALL CONDUCTION	0.634	0.186	-1.348	-0.395
ROOF CONDUCTION	1.317	0.386	-2.897	-0.849
WINDOW GLASS-FRM COND	0.000	0.000	0.000	0.000
WINDOW GLASS SOLAR	0.000	0.000	0.000	0.000
DOOR CONDUCTION	0.000	0.000	0.000	0.000
INTERNAL SURFACE COND	0.000	0.000	0.000	0.000
UNDERGROUND SURF COND	0.000	0.000	0.000	0.000
OCCUPANTS TO SPACE	0.000	0.000	0.000	0.000
LIGHT TO SPACE	0.000	0.000	0.000	0.000
EQUIPMENT TO SPACE	0.000	0.000	0.000	0.000
PROCESS TO SPACE	0.000	0.000	0.000	0.000
INFILTRATION	0.128	0.038	0.289	0.085

LATENT		
(BTU/H)	(KW)	(BTU/H)

---	---	---
-----	-----	-----

TOTAL	2.079	0.609	0.289	0.085
TOTAL / AREA	0.001	0.004	0.000	0.001
TOTAL LOAD	2.369	KBTU/H	0.694 KW	-5.409 KBTU/H
TOTAL LOAD / AREA	1.57	BTU/H.SQFT	4.938 W/M ²	3.590 BTU/H.SQFT

* NOTE 1) THE ABOVE LOADS EXCLUDE OUTSIDE VENTILATION AIR
* --- LOADS
* 2) TIMES GIVEN IN STANDARD TIME FOR THE LOCATION
* IN CONSIDERATION
* 3) THE ABOVE LOADS ARE CALCULATED ASSUMING A
* CONSTANT INDOOR SPACE TEMPERATURE
* *****

SPACE ELL North Perim Plnm (T.N28)
SPACE TEMPERATURE USED FOR THE LOADS CALCULATION IS 70 F / 21 C

MULTIPLIER 1.0 FLOOR MULTIPLIER 1.0

FLOOR AREA	2373 SQFT	220 M ²
VOLUME	7119 CUFT	202 M ³

COOLING LOAD

TIME	AUG 5 7PM	JAN 27 11AM
DRY-BULB TEMP	96 F	30 C
WET-BULB TEMP	73 F	23 C
TOT HORIZONTAL SOLAR RAD	71 BTU/H.SQFT	223 W/M ²
WIND SPEED AT SPACE	3.5 KTS	1.8 M/S
CLOUD AMOUNT 0 (CLEAR)	2	1

HEATING LOAD

TIME	AUG 5 7PM	JAN 27 11AM
0 F	-18 C	-18 C
-1 F	-18 C	-18 C
115 BTU/H.SQFT	362 W/M ²	362 W/M ²
2.8 KTS	1.5 M/S	1

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

LATENT (BTU/H) (KW)

(BTU/H) (KW)

SENSIBLE (BTU/H) (KW)

(BTU/H) (KW)

SPACE EII West Perim Plm (T.W29)

SPACE TEMPERATURE USED FOR THE LOADS CALCULATION IS 70 F / 21 C

MULTIPLIER 1.0

FLOOR AREA 1507 SQFT 140 M2

VOLUME 4520 CUFT 128 M3

COOLING LOAD

TIME JUL 6 9PM

DRY-BULB TEMP 74 F 23 C

WET-BULB TEMP 68 F 20 C

TOT HORIZONTAL SOLAR RAD 13 BTU/H.SQFT 40 W/M2

WIND SPEED AT SPACE 4.2 KTS 2.2 M/S

CLOUD AMOUNT 0 (CLEAR) -10 5

FLOOR MULTIPLIER 1.0

HEATING LOAD

TIME JAN 27 11AM

DRY-BULB TEMP 0 F -18 C

WET-BULB TEMP -1 F -18 C

TOT HORIZONTAL SOLAR RAD 115 BTU/H.SQFT 362 W/M2

WIND SPEED AT SPACE 2.8 KTS 1.5 M/S

SENSIBLE LATENT

(BTU/H) (KWH) (BTU/H) (KWH)

WALL CONDUCTION 0.649 0.190 0.000 0.000

ROOF CONDUCTION 1.375 0.403 0.000 0.000

WINDOW GLASS-FRM COND 0.000 0.000 0.000 0.000

WINDOW GLASS SOLAR 0.000 0.000 0.000 0.000

DOOR CONDUCTION 0.000 0.000 0.000 0.000

INTERNAL SURFACE COND 0.000 0.000 0.000 0.000

UNDERGROUND SURF COND 0.000 0.000 0.000 0.000

OCCUPANTS TO SPACE 0.000 0.000 0.000 0.000

LIGHT TO SPACE 0.000 0.000 0.000 0.000

EQUIPMENT TO SPACE 0.000 0.000 0.000 0.000

PROCESS TO SPACE 0.000 0.000 0.000 0.000

INFILTRATION 0.027 0.008 0.153 0.045

TOTAL 2.051 0.601 0.153 0.045

TOTAL / AREA 0.001 0.004 0.000 0.000

TOTAL LOAD 2.205 BTU/H 0.646 KW

TOTAL LOAD / AREA 1.46 BTU/H.SQFT 4.615 W/M2

FLOOR MULTIPLIER 1.0

HEATING LOAD

TIME JAN 27 11AM

DRY-BULB TEMP 0 F -18 C

WET-BULB TEMP -1 F -18 C

TOT HORIZONTAL SOLAR RAD 115 BTU/H.SQFT 362 W/M2

WIND SPEED AT SPACE 2.8 KTS 1.5 M/S

* NOTE 1) THE ABOVE LOADS EXCLUDE OUTSIDE VENTILATION AIR

* --- LOADS

* 2) TIMES GIVEN IN STANDARD TIME FOR THE LOCATION

* IN CONSIDERATION

* 3) THE ABOVE LOADS ARE CALCULATED ASSUMING A

* CONSTANT INDOOR SPACE TEMPERATURE

REPORT- LS-B Space Peak Load Components EII Core PlnM (T.C30)

WEATHER FILE - Toronto ON CWEC

SPACE E11 Core P1nm (T.C30) SPACE TEMPERATURE USED FOR THE LOADS CALCULATION IS 70 F / 21 C

TIME	DRY-BULB TEMP	WET-BULB TEMP	TEMP	FLOOR MULTIPLIER
	TOT. HORIZONTAL SOLAR RAD	WINDSPEED AT SPACE	WINDCLOUD AMOUNT 0 (CLEAR) - 10	
JUL 6 9PM	74 F	68 F	13 BTU / H. SQFT	23 C
			4.2 KWS	20 C
				40 W/M2
				2.2 M/S
				5

COOLING LOAD		HEATING LOAD	
JUL	6 9PM	JAN	1 12NOON
74 F	23 C	1 F	-17 C
68 F	20 C	0 F	-18 C
1.3 BTU/H. SQFT	40 W/M ²	109 BTU/H. SQFT	343 W/M ²
4.12 KTS	2.2 M/S	14.8 KTS	7.6 M/S
5		5	

	SENSIBLE (BTU/H)	LATENT (BTU/H)	SENSIBLE (BTU/H)	LATENT (BTU/H)
	(KW)	(KW)	(KW)	(KW)
WALL CONDUCTION	0.000	0.000	0.000	0.000
ROOF CONDUCTION	11.251	3.296	0.000	0.000
WINDOW GLASS+FRM COND	0.000	0.000	0.000	-25.214
WINDOW GLASS SOLAR	0.000	0.000	0.000	-7.388
DOOR CONDUCTION	0.000	0.000	0.000	0.000
INTERNAL SURFACE COND	0.000	0.000	0.000	0.000
UNDERGROUND SURF COND	0.000	0.000	0.000	0.000
OCCUPANTS TO SPACE	0.000	0.000	0.000	0.000
LIGHT TO SPACE	0.000	0.000	0.000	0.000
EQUIPMENT TO SPACE	0.000	0.000	0.000	0.000
PROCESS TO SPACE	0.000	0.000	0.000	0.000
INFILTRATION	0.025	0.007	0.143	0.042
TOTAL / AREA	11.276	3.304	0.143	0.042
TOTAL LOAD	11.419	3.346	0.143	0.042
TOTAL ZONE	11.419	3.346	0.143	0.042

* NOTE 1) THE ABOVE LOADS EXCLUDE OUTSIDE VENTILATION AIR
 * - - - LOADS
 * 2) TIMES GIVEN IN STANDARD TIME FOR THE LOCATION
 * IN CONSIDERATION
 * 3) THE ABOVE LOADS ARE CALCULATED ASSUMING A
 * CONSTANT INDOOR SPACE TEMPERATURE

*** BUILDING ***

TIME	COOLING LOAD			HEATING LOAD		
	JUN 11	4PM		JAN 1	6AM	
DRY-BULB TEMP	86 F		30 C	-3 F		-19 C
WET-BULB TEMP	69 F		21 C	-3 F		-19 C
TOT HORIZONTAL SOLAR RAD	21.6 BTU/H.SQFT		680 W/M2	0 BTU/H.SQFT		0 W/M2
WIND SPEED AT SPACE	10.6 KTS		5.4 M/S	7.8 KTS		4.0 M/S
CLOUD AMOUNT 0 (CLEAR) -10	6			7		
<hr/>						
	SENSIBLE (KBTU/H)	(KW)	LATENT (KBTU/H)	(KW)	SENSIBLE (KBTU/H)	(KW)
WALL CONDUCTION	9.663	2.831	0.000	0.000	-32.411	-9.496
ROOF CONDUCTION	0.146	0.043	0.000	0.000	-0.886	-0.260
WINDOW GLASS-TERM COND	40.602	11.896	0.000	0.000	-212.944	-62.393
WINDOW GLASS SOLAR	231.593	67.857	0.000	0.000	11.301	3.487
DOOR CONDUCTION	0.000	0.000	0.000	0.000	0.000	0.000
INTERNAL SURFACE COND	0.000	0.000	0.000	0.000	0.000	0.000
UNDERGROUND SURF COND	-6.851	-2.007	0.000	0.000	-10.515	-3.081
OCCUPANTS TO SPACE	492.914	144.424	441.087	129.-239		
LIGHT TO SPACE	115.762	33.918	0.000	0.000	2.675	0.784
EQUIPMENT TO SPACE	115.049	33.709	0.000	0.000	5.980	1.752
PROCESS TO SPACE	0.000	0.000	0.000	0.000	0.000	0.000
INFILTRATION	10.543	3.089	7.891	2.312	-25.667	-7.520
TOTAL / AREA	1009.421	295.760	448.979	131.551	-261.868	-76.727
TOTAL LOAD / AREA	0.017	0.053	0.007	0.024	-0.004	-0.014
TOTAL LOAD / H	1458.399	KBTU/H	427.311	KW	-261.868 KBTU/H	-76.727 KW
TOTAL LOAD / SQFT	24.31	BTU/H.SQFT	76.675	W/M2	4.365 BTU/H.SQFT	13.768 W/M2

* * NOTE 1) THE ABOVE LOADS EXCLUDE OUTSIDE VENTILATION AIR
* * --- LOADS
* * 2) TIMES GIVEN IN STANDARD TIME FOR THE LOCATION
* * IN CONSIDERATION
* * 3) THE ABOVE LOADS ARE CALCULATED ASSUMING A
* * CONSTANT INDOOR SPACE TEMPERATURE
* *

	C O O L I N G - - - - -						H E A T I N G - - - - -						E L E C - - - - -		
MONTH	COOLING ENERGY (MBTU)	TIME OF MAX DY	DRY- BLDG TEMP	WET- BLDG TEMP	MAXIMUM COOLING LOAD (KBTU/HR)	HEATING ENERGY (MBTU)	TIME OF MAX DY	DRY- BLDG TEMP	WET- BLDG TEMP	MAXIMUM HEATING LOAD (KBTU/HR)	HEATING ENERGY (KWH)	ELEC-TRICAL ENERGY (KWH)	ELEC-TRICAL ENERGY (KWH)	MAXIMUM ELEC-LOAD (KW)	
JAN	141.23062	22	16	39.F	34.F	846.599	-80.802	1	6	-3.F	-3.F	-261.868	21452.	95.947	
FEB	142.70102	10	16	51.F	47.F	839.949	-64.850	3	6	1.F	0.F	-226.130	20872.	95.947	
MAR	182.72125	24	15	55.F	47.F	902.533	-48.221	11	6	4.F	4.F	-206.212	24355.	95.947	
APR	194.04678	14	15	65.F	47.F	969.939	-25.595	4	6	14.F	12.F	-186.782	22909.	95.947	
MAY	205.18846	27	15	69.F	56.F	950.009	-11.951	1	5	30.F	27.F	-119.789	20351.	95.947	
JUN	244.13289	11	15	86.F	69.F	1009.421	-3.660	20	5	42.F	41.F	-80.354	21981.	95.947	
JUL	248.76683	8	15	90.F	75.F	989.209	-0.966	22	5	47.F	46.F	-43.460	21479.	95.947	
AUG	247.86031	3	15	90.F	71.F	999.860	-1.752	8	5	45.F	44.F	-67.379	22004.	95.947	
SEP	219.59392	24	15	69.F	58.F	992.255	-6.479	26	6	33.F	32.F	-96.458	21837.	95.947	
OCT	182.05438	5	15	60.F	52.F	946.203	-22.491	23	7	18.F	17.F	-162.732	21696.	95.947	
NOV	156.09367	9	15	58.F	51.F	852.514	-41.894	13	5	19.F	18.F	-155.841	23050.	95.947	
DEC	154.39960	8	15	30.F	28.F	818.880	-68.493	24	8	12.F	11.F	-209.991	23924.	95.947	
TOTAL	2318.792					-377.154							265911.		
MAX						1009.421							-261.868	95.947	

Base Case Model-1

DOE-2.2-48r

WEATHER FILE- Toronto ON CWEC

REPORT- IS-E Space Monthly Load Components EII South Perim Spc (G.S1)

5/01/2016 20:26:47 BDL RUN 3

(UNITS=MBTU)	WALLS	ROOFS	INT SUR.	UND SUR.	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL	
<hr/>													
JAN SEN CL	-1.201	0.000	0.000	-1.184	-1.264	-7.477	3.726	0.441	0.714	0.340	0.000	-5.903	
LAT CL	-0.226	0.000	0.000	-0.287	-0.466	-1.731	3.496	0.460	0.284	0.268	0.000	1.798	
FEB SEN CL	-1.007	0.000	0.000	-1.128	-1.137	-6.419	3.252	0.471	0.751	0.347	0.000	-4.870	
LAT CL	-0.252	0.000	0.000	-0.344	-0.458	-1.882	3.834	0.430	0.216	0.251	0.000	1.794	
MAR SEN CL	-0.767	0.000	0.000	-1.107	-0.923	-5.303	3.043	0.416	0.645	0.319	0.000	-3.677	
LAT CL	-0.279	0.000	0.000	-0.537	-0.537	-2.257	4.792	0.667	0.386	0.392	0.000	2.627	
APR SEN CL	-0.397	0.000	0.000	-0.782	-0.520	-3.128	2.110	0.246	0.331	0.206	0.000	-1.932	
LAT CL	-0.242	0.000	0.000	-0.735	-0.457	-2.148	5.111	0.797	0.518	0.477	0.000	3.320	
MAY SEN CL	-0.171	0.000	0.000	-0.464	-0.286	-1.776	1.316	0.121	0.164	0.122	0.000	-0.974	
LAT CL	-0.089	0.000	0.000	-0.799	-0.281	-1.667	5.419	0.836	0.351	0.514	0.000	4.284	
JUN SEN CL	-0.035	0.000	0.000	-0.151	-0.096	-0.619	0.520	0.028	0.049	0.040	0.000	-0.264	
LAT CL	0.155	0.000	0.000	-0.778	-0.065	-0.861	5.548	1.007	0.472	0.641	0.000	6.120	
JUL SEN CL	-0.007	0.000	0.000	-0.035	-0.026	-0.161	0.134	0.018	0.029	0.018	0.000	-0.031	
LAT CL	0.361	0.000	0.000	-0.661	0.037	-0.347	5.722	0.985	0.582	0.645	0.000	7.325	
AUG SEN CL	-0.006	0.000	0.000	-0.018	-0.020	-0.128	0.106	0.004	0.010	0.009	0.000	1.384	
LAT CL	0.403	0.000	0.000	-0.510	-0.028	-0.719	6.651	1.033	0.541	0.677	0.000	8.049	
SEP SEN CL	-0.044	0.000	0.000	-0.058	-0.078	-0.473	0.396	0.025	0.050	0.030	0.000	-0.152	
LAT CL	0.155	0.000	0.000	-0.439	-0.296	-1.766	7.718	0.971	0.710	0.627	0.000	7.681	
OCT SEN CL	-0.237	0.000	0.000	-0.219	-0.314	-2.021	1.405	0.110	0.189	0.105	0.000	-0.982	
LAT CL	-0.192	0.000	0.000	-0.429	-0.492	-2.448	6.623	0.848	0.712	0.531	0.000	5.154	
NOV SEN CL	-0.649	0.000	0.000	-0.566	-0.679	-4.084	1.723	0.291	0.649	0.387	0.000	0.892	
LAT CL	-0.225	0.000	0.000	-0.309	-0.418	-1.799	3.117	0.649	0.794	0.387	0.000	1.369	
DEC SEN CL	-1.110	0.000	0.000	-0.973	-1.165	-6.597	2.368	0.548	0.929	0.399	0.000	-5.601	
LAT CL	-0.238	0.000	0.000	-0.225	-0.392	-1.539	2.693	0.455	0.417	0.264	0.000	1.436	
TOT	HEATING	-5.631	0.000	0.000	-6.684	-6.509	-38.186	20.099	2.719	4.481	2.177	0.000	-27.533
	SEN CL	-0.669	0.000	0.000	-6.054	-3.853	-19.165	60.724	9.139	5.985	5.675	0.000	51.782
	LAT CL				1.375	0.000		0.501	0.710	0.000	0.000	0.000	10.543

Base Case Model-1

DOE-2.2-48r

5/01/2016

20:26:47

BDL RUN

3

REPORT- LS-E Space Monthly Load Components EII East Perim Spc (G.E2)

WEATHER FILE- Toronto ON CWEC

(UNITS=MBTU)	WALLS	ROOFS	INT SUR	UND SUR	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL
HEATING	-1.109	0.000	0.000	-0.951	-1.116	-5.936	1.506	0.519	0.692	0.357	0.000	-6.39
JAN SEN CL	-0.029	0.000	0.000	-0.029	-0.037	-0.156	0.165	0.052	0.043	0.029	0.000	0.039
LAT CL					0.000			0.059			0.000	0.059
HEATING	-0.924	0.000	0.000	-0.922	-0.992	-5.170	1.687	0.494	0.651	0.336	0.000	-4.840
FEB SEN CL	-0.058	0.000	0.000	-0.058	-0.072	-0.321	0.421	0.078	0.042	0.043	0.000	0.076
LAT CL					0.000			0.090			0.000	0.090
HEATING	-0.632	0.000	0.000	-0.845	-0.716	-3.941	1.845	0.347	0.487	0.255	0.000	-3.199
MAR SEN CL	-0.152	0.000	0.000	-0.250	-0.257	-1.054	1.902	0.340	0.161	0.197	0.000	0.886
LAT CL					0.000			0.383			0.000	0.383
HEATING	-0.298	0.000	0.000	-0.555	-0.365	-2.179	1.385	0.160	0.236	0.136	0.000	-1.479
APR SEN CL	-0.138	0.000	0.000	-0.456	-0.287	-1.299	3.032	0.502	0.290	0.298	0.000	1.941
LAT CL					0.004			0.539			0.000	0.543
HEATING	-0.081	0.000	0.000	-0.214	-0.131	-0.856	0.723	0.043	0.069	0.049	0.000	-0.400
MAY SEN CL	0.002	0.000	0.000	-0.628	-0.246	-1.396	5.368	0.565	0.236	0.395	0.000	4.257
LAT CL					0.020			0.551			0.000	0.570
HEATING	-0.013	0.000	0.000	-0.063	-0.039	-0.267	0.271	0.009	0.015	0.016	0.000	-0.071
JUN SEN CL	0.194	0.000	0.000	-0.556	-0.068	-0.693	5.374	0.648	0.289	0.417	0.000	5.605
LAT CL					0.180			0.611			0.000	0.791
HEATING	-0.004	0.000	0.000	-0.012	-0.008	-0.058	0.047	0.006	0.010	0.007	0.000	-0.012
JUL SEN CL	0.341	0.000	0.000	-0.451	0.016	-0.265	5.392	0.630	0.354	0.413	0.000	6.431
LAT CL					0.312			0.584			0.000	0.896
HEATING	-0.003	0.000	0.000	-0.009	-0.010	-0.064	0.058	0.002	0.005	0.004	0.000	-0.018
AUG SEN CL	0.301	0.000	0.000	-0.343	-0.022	-0.491	4.824	0.656	0.278	0.431	0.000	5.634
LAT CL					0.271			0.611			0.000	0.882
HEATING	-0.050	0.000	0.000	-0.065	-0.082	-0.304	0.382	0.030	0.056	0.034	0.000	-0.198
SEP SEN CL	0.058	0.000	0.000	-0.266	-0.168	-0.985	3.903	0.601	0.426	0.383	0.000	3.953
LAT CL					0.096			0.581			0.000	0.677
HEATING	-0.288	0.000	0.000	-0.232	-0.320	-1.943	0.902	0.142	0.245	0.123	0.000	-1.373
OCT SEN CL	-0.134	0.000	0.000	-0.200	-0.217	-1.024	1.969	0.466	0.399	0.281	0.000	1.540
LAT CL					0.025			0.491			0.000	0.516
HEATING	-0.590	0.000	0.000	-0.471	-0.578	-3.271	0.795	0.300	0.379	0.229	0.000	-3.008
NOV SEN CL	-0.105	0.000	0.000	-0.112	-0.153	-0.621	0.521	0.296	0.359	0.171	0.000	0.356
LAT CL					0.04			0.337			0.000	0.340
HEATING	-0.983	0.000	0.000	-0.767	-0.999	-5.191	1.011	0.563	0.856	0.381	0.000	-5.128
DEC SEN CL	-0.036	0.000	0.000	-0.032	-0.039	-0.186	0.138	0.074	0.085	0.039	0.000	0.043
LAT CL					0.000			0.084			0.000	0.084
HEATING	-4.976	0.000	0.000	-5.105	-5.358	-29.380	10.611	2.617	3.899	1.927	0.000	-25.766
TOT SEN CL	0.244	0.000	0.000	-3.382	-1.548	-8.490	33.009	4.908	2.963	3.057	0.000	30.762
LAT CL					0.912			4.921			0.000	5.833

Base Case Model-1

DOE-2.2-48r

5/01/2016

20:26:47

BDL

RUN

3

REPORT- LS-E Space Monthly Load Components EII North Perim Spc (G.N3)

WEATHER FILE- Toronto ON CWEC

(UNITS=MBTU)	WALLS	ROOFS	INT SUR.	UND SUR.	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL
HEATING JAN SEN CL -0.022	0.000	0.000	-1.449	-1.710	-9.051	1.157	0.857	1.467	0.585	0.000	-9.950	
HEATING FEB SEN CL -0.021	0.000	0.000	-1.446	-1.574	-8.170	0.857	1.103	0.573	0.000	0.017	0.017	
HEATING MAR SEN CL -0.048	0.000	0.000	-1.569	-1.403	-7.285	2.132	0.960	0.885	0.644	0.000	-7.003	
HEATING APR SEN CL -0.183	0.000	0.000	-1.136	-0.163	-4.299	1.826	0.487	0.485	0.362	0.000	-3.783	
HEATING MAY SEN CL -0.181	0.000	0.000	-0.647	-0.344	-2.184	1.331	0.170	0.214	0.163	0.000	0.622	
HEATING JUN SEN CL 0.050	0.000	0.000	-0.182	-0.103	-0.679	0.507	0.037	0.049	0.050	0.000	0.616	
HEATING JUL SEN CL 0.224	0.000	0.000	-0.061	-0.037	-0.245	0.173	0.029	0.040	0.028	0.000	0.847	
HEATING AUG SEN CL 0.151	0.000	0.000	-0.196	-0.121	-1.327	0.591	0.126	0.185	0.122	0.000	-0.368	
HEATING SEP SEN CL -0.114	0.000	0.000	-0.087	-0.072	-0.464	0.304	0.043	0.056	0.049	0.000	4.568	
HEATING OCT SEN CL -0.194	0.000	0.000	-0.452	-0.580	-3.477	1.065	0.327	0.493	0.264	0.000	5.386	
HEATING NOV SEN CL -0.151	0.000	0.000	-0.140	-0.180	-0.755	0.314	0.400	0.603	0.227	0.000	1.381	
HEATING DEC SEN CL -0.041	0.000	0.000	-1.162	-1.520	-7.903	0.862	0.916	1.574	0.615	0.000	-4.936	
HEATING TOT SEN CL -0.530	0.000	0.000	-9.122	-9.234	-50.163	12.281	5.351	7.533	3.858	0.000	-48.676	
			-3.621	-1.127	-6.855	18.244	6.512	4.205	3.995	0.000	20.823	
			1.311	1.311	6.657				0.000	0.000	7.968	

Base Case Model-1

DOE-2.2-48r

5/01/2016

20:26:47

BDL RUN

3

REPORT- IS-E Space Monthly Load Components EII West Perim Spc (G.W4) WEATHER FILE- Toronto ON CWEC

(UNITS=MBTU)	WALLS	ROOFS	INT SUR.	UND SUR.	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL
HEATING	-1.092	0.000	0.000	-0.930	-1.089	-5.879	1.411	0.484	0.697	0.339	0.000	-6.059
JAN SEN CL	-0.050	0.000	0.000	-0.050	-0.064	-0.277	0.375	0.088	0.056	0.047	0.000	0.124
LAT CL					0.000			0.097			0.000	0.097
HEATING	-0.922	0.000	0.000	-0.897	-0.967	-5.141	1.722	0.463	0.618	0.319	0.000	-4.804
FEB SEN CL	-0.073	0.000	0.000	-0.083	-0.097	-0.418	0.639	0.109	0.070	0.061	0.000	0.207
LAT CL					0.000			0.117			0.000	0.117
HEATING	-0.734	0.000	0.000	-0.921	-0.817	-4.357	1.975	0.470	0.541	0.329	0.000	-3.514
MAR SEN CL	-0.117	0.000	0.000	-0.174	-0.156	-0.700	1.167	0.217	0.157	0.122	0.000	0.517
LAT CL					0.000			0.227			0.000	0.227
HEATING	-0.337	0.000	0.000	-0.574	-0.400	-2.306	1.473	0.205	0.252	0.164	0.000	-1.523
APR SEN CL	-0.174	0.000	0.000	-0.437	-0.252	-1.208	2.653	0.457	0.317	0.270	0.000	1.626
LAT CL					0.004			0.478			0.000	0.482
HEATING	-0.117	0.000	0.000	-0.293	-0.180	-1.125	0.847	0.066	0.106	0.070	0.000	-0.625
MAY SEN CL	-0.092	0.000	0.000	-0.549	-0.198	-1.152	3.771	0.541	0.255	0.334	0.000	2.909
LAT CL					0.018			0.536			0.000	0.555
HEATING	-0.017	0.000	0.000	-0.061	-0.040	-0.260	0.250	0.010	0.018	0.016	0.000	-0.084
JUN SEN CL	0.117	0.000	0.000	-0.558	-0.067	-0.700	4.963	0.647	0.341	0.417	0.000	5.161
LAT CL					0.180			0.610			0.000	0.790
HEATING	-0.002	0.000	0.000	-0.007	-0.006	-0.033	0.026	0.004	0.007	0.004	0.000	-0.007
JUL SEN CL	0.257	0.000	0.000	-0.457	0.014	-0.287	4.964	0.633	0.458	0.416	0.000	5.998
LAT CL					0.312			0.583			0.000	0.895
HEATING	-0.003	0.000	0.000	-0.010	-0.011	-0.070	0.064	0.002	0.005	0.005	0.000	-0.017
AUG SEN CL	0.243	0.000	0.000	-0.342	-0.021	-0.490	4.509	0.656	0.370	0.431	0.000	5.356
LAT CL					0.270			0.611			0.000	0.881
HEATING	-0.005	0.000	0.000	-0.070	-0.087	-0.348	0.396	0.033	0.059	0.037	0.000	-0.237
SEP SEN CL	-0.008	0.000	0.000	-0.261	-0.162	-0.949	3.350	0.599	0.493	0.380	0.000	3.442
LAT CL					0.097			0.581			0.000	0.677
HEATING	-0.291	0.000	0.000	-0.239	-0.321	-1.972	1.012	0.145	0.221	0.127	0.000	-1.319
OCT SEN CL	-0.155	0.000	0.000	-0.193	-0.216	-1.009	1.878	0.463	0.423	0.277	0.000	1.467
LAT CL					0.023			0.486			0.000	0.509
HEATING	-0.599	0.000	0.000	-0.475	-0.593	-3.335	0.871	0.322	0.606	0.243	0.000	-2.960
NOV SEN CL	-0.105	0.000	0.000	-0.108	-0.138	-0.590	0.541	0.274	0.366	0.156	0.000	0.396
LAT CL					0.003			0.311			0.000	0.315
HEATING	-0.990	0.000	0.000	-0.764	-0.997	-5.244	0.965	0.556	0.866	0.378	0.000	-5.229
DEC SEN CL	-0.039	0.000	0.000	-0.034	-0.041	-0.204	0.179	0.080	0.081	0.042	0.000	0.063
LAT CL					0.000			0.091			0.000	0.091
HEATING	-5.158	0.000	0.000	-5.241	-5.507	-30.270	11.012	2.758	3.998	2.030	0.000	-26.378
TOT SEN CL	-0.197	0.000	0.000	-3.246	-1.399	-7.985	28.987	4.766	3.385	2.954	0.000	27.266
LAT CL					0.908			4.729			0.000	5.637

Base Case Model-1

DOE-2.2-48r

5/01/2016

20:26:47

BDL RUN

3

REPORT- LS-E Space Monthly Load Components EII Core Spec (G.CS)

WEATHER FILE- Toronto ON CWEC

(UNITS=MBTU)	WALLS	ROOFS	INT SUR.	UND SUR.	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL
HEATING	0.000	0.000	0.000	-0.346	-0.030	0.000	0.000	0.013	0.063	0.163	0.000	-0.137
JAN SEN CL	0.000	0.000	0.000	-2.577	-0.199	0.000	0.000	28.430	9.360	7.504	0.000	42.519
LAT CL					0.000			23.172		0.000	0.000	23.172
HEATING	0.000	0.000	0.000	-0.092	-0.005	0.000	0.000	0.019	0.020	0.040	0.000	-0.017
FEB SEN CL	0.000	0.000	0.000	-2.834	-0.200	0.000	0.000	28.458	9.365	7.498	0.000	42.287
LAT CL					0.000			23.172		0.000	0.000	23.172
HEATING	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
MAR SEN CL	0.000	0.000	0.000	-3.267	-0.185	0.000	0.000	34.107	11.205	8.967	0.000	50.827
LAT CL					0.000			28.050		0.000	0.000	28.050
HEATING	0.000	0.000	0.000	-3.017	-0.127	0.000	0.000	32.966	10.824	8.618	0.000	49.265
APR SEN CL	0.000	0.000	0.000	0.001	0.001			26.831		0.000	0.000	26.831
HEATING	0.000	0.000	0.000	-0.013	0.000	0.000	0.000	0.002	0.003	0.008	0.000	0.000
MAY SEN CL	0.000	0.000	0.000	-2.500	-0.078	0.000	0.000	30.372	10.021	8.036	0.000	45.850
LAT CL					0.004			24.391		0.000	0.000	24.396
HEATING	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
JUN SEN CL	0.000	0.000	0.000	-1.848	-0.028	0.000	0.000	32.584	10.710	8.585	0.000	50.02
LAT CL					0.030			26.831		0.000	0.000	26.861
HEATING	0.000	0.000	0.000	-1.385	-0.003	0.000	0.000	31.759	10.459	8.357	0.000	49.188
JUL SEN CL	0.000	0.000	0.000	0.059				25.611		0.000	0.000	25.670
HEATING	0.000	0.000	0.000	-1.052	-0.011	0.000	0.000	32.711	10.765	8.644	0.000	51.058
AUG SEN CL	0.000	0.000	0.000	0.053				26.831		0.000	0.000	26.884
HEATING	0.000	0.000	0.000	0.000	0.000	0.000	0.000	31.447	10.349	8.287	0.000	49.046
SEP SEN CL	0.000	0.000	0.000	-0.988	-0.050	0.000	0.000	25.611		0.000	0.000	25.631
HEATING	0.000	0.000	0.000	-1.288	-0.108	0.000	0.000	30.349	10.016	8.037	0.000	47.006
OCT SEN CL	0.000	0.000	0.000	0.006				24.391		0.000	0.000	24.398
HEATING	0.000	0.000	0.000	-1.739	-0.144	0.000	0.000	29.611	9.776	7.920	0.000	45.424
NOV SEN CL	0.000	0.000	0.000	-1.331	0.001			24.391		0.000	0.000	24.392
DEC SEN CL	0.000	0.000	0.000	-2.366	-0.199	0.000	0.000	31.749	10.453	8.351	0.000	47.989
LAT CL				0.175				25.611		0.000	0.000	25.611
HEATING	0.000	0.000	0.000	-0.467	-0.037	0.000	0.000	0.037	0.091	0.220	0.000	-0.155
TOT SEN CL	0.000	0.000	0.000	-24.861	-1.331	0.000	0.000	374.545	123.306	98.804	0.000	570.465
LAT CL				0.175				304.895		0.000	0.000	305.070

Base Case Model-1

DOE-2.2-48r

WEATHER FILE- Toronto ON CWEC

REPORT- LS-E Space Monthly Load Components EII South Perim Plnm (G.S6)

5/01/2016 20:26:47 BDL RUN 3

(UNITS=MBTU)	WALLS	ROOFS	INT SUR.	UND SUR.	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL
JAN SEN CL	-0.952 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.519 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-1.471
JAN LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
FEB SEN CL	-0.842 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.479 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-1.321
FEB LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
MAR SEN CL	-0.699 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.438 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-1.137
MAR LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
APR SEN CL	-0.433 0.003	0.000 0.000	0.000 0.000	0.000 0.000	-0.292 0.001	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.725
APR LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
MAY SEN CL	-0.201 0.023	0.000 0.000	0.000 0.000	0.000 0.000	-0.164 0.006	0.000 0.001	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.365
MAY LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
JUN SEN CL	-0.049 0.125	0.000 0.000	0.000 0.000	0.000 0.000	-0.059 0.011	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.108
JUN LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
JUL SEN CL	-0.011 0.242	0.000 0.000	0.000 0.000	0.000 0.000	-0.021 0.025	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.032
JUL LAT CL					0.126	0.126	0.000	0.000	0.000	0.000	0.000	0.000
AUG SEN CL	-0.005 0.265	0.000 0.000	0.000 0.000	0.000 0.000	-0.025 0.011	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.267
AUG LAT CL					0.113	0.113	0.000	0.000	0.000	0.000	0.000	0.000
SEP SEN CL	-0.063 0.131	0.000 0.000	0.000 0.000	0.000 0.000	-0.093 -0.020	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.136
SEP LAT CL					0.028	0.028	0.000	0.000	0.000	0.000	0.000	0.000
OCT SEN CL	-0.304 0.014	0.000 0.000	0.000 0.000	0.000 0.000	-0.237 -0.005	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.541
OCT LAT CL					0.002	0.002	0.000	0.000	0.000	0.000	0.000	0.000
NOV SEN CL	-0.584 0.001	0.000 0.000	0.000 0.000	0.000 0.000	-0.328 -0.001	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.912
NOV LAT CL					0.100	0.100	0.000	0.000	0.000	0.000	0.000	0.000
DEC SEN CL	-0.899 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.467 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-1.366
DEC LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
TOT SEN CL	-5.042 0.805	0.000 0.000	0.000 0.000	0.000 0.000	-3.123 0.014	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-8.164
TOT LAT CL					0.335	0.335	0.000	0.000	0.000	0.000	0.000	0.000

Base Case Model-1

DOE-2.2-48r

5/01/2016 20:26:47 BDL RUN 3

REPORT- LS-E Space Monthly Load Components EII East Perim Plm (G.E7)

WEATHER FILE- Toronto ON CWEC

(UNITS=MBTU)	WALLS	ROOFS	INT SUR	UND SUR	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL
JAN SEN CL	-0.748 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.346 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-1.94 0.000
JAN LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
FEB SEN CL	-0.647 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.319 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.966 0.000
FEB LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
MAR SEN CL	-0.518 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.292 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.810 0.000
MAR LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
APR SEN CL	-0.292 0.003	0.000 0.000	0.000 0.000	0.000 0.000	-0.195 -0.001	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.487 0.002
APR LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
MAY SEN CL	-0.093 0.038	0.000 0.000	0.000 0.000	0.000 0.000	-0.104 -0.001	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.198 0.029
MAY LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
JUN SEN CL	-0.016 0.131	0.000 0.000	0.000 0.000	0.000 0.000	-0.035 0.003	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.050 0.134
JUN LAT CL					0.044	0.000	0.000	0.000	0.000	0.000	0.000	0.000
JUL SEN CL	-0.005 0.224	0.000 0.000	0.000 0.000	0.000 0.000	-0.013 0.015	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.018 0.239
JUL LAT CL					0.085	0.000	0.000	0.000	0.000	0.000	0.000	0.000
AUG SEN CL	-0.002 0.195	0.000 0.000	0.000 0.000	0.000 0.000	-0.017 0.008	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.019 0.203
AUG LAT CL					0.077	0.000	0.000	0.000	0.000	0.000	0.000	0.000
SEP SEN CL	-0.057 0.060	0.000 0.000	0.000 0.000	0.000 0.000	-0.069 -0.005	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.127 0.055
SEP LAT CL					0.015	0.000	0.000	0.000	0.000	0.000	0.000	0.000
OCT SEN CL	-0.280 0.001	0.000 0.000	0.000 0.000	0.000 0.000	-0.161 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.441 0.001
OCT LAT CL					0.001	0.000	0.000	0.000	0.000	0.000	0.000	0.000
NOV SEN CL	-0.457 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.219 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.677 0.000
NOV LAT CL					0.100	0.000	0.000	0.000	0.000	0.000	0.000	0.000
DEC SEN CL	-0.669 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.311 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.981 0.223
DEC LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
TOT SEN CL	-3.785 0.653	0.000 0.000	0.000 0.000	0.000 0.000	-2.083 0.10	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-5.867 0.663 0.223
TOT LAT CL					0.223	0.000	0.000	0.000	0.000	0.000	0.000	0.000

Base Case Model-1

DOE-2.2-48r

WEATHER FILE- Toronto ON CWEC

REPORT- IS-E Space Monthly Load Components EII North Perim Plnm (G.N8)

5/01/2016 20:26:47 BDL RUN 3

(UNITS=MBTU)	WALLS	ROOFS	INT SUR.	UND SUR.	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL
<hr/>												
JAN SEN CL	-1.185 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.519 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-1.705 0.000
LAT CL												0.000 0.000
FEB SEN CL	-1.045 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.479 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-1.523 0.000
LAT CL												0.000 0.000
MAR SEN CL	-0.919 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.438 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-1.357 0.000
LAT CL												0.000 0.000
APR SEN CL	-0.603 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.293 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.896 0.000
LAT CL												0.000 0.000
MAY SEN CL	-0.302 0.001	0.000 0.000	0.000 0.000	0.000 0.000	-0.170 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.472 0.002
LAT CL												0.000 0.000
JUN SEN CL	-0.073 0.070	0.000 0.000	0.000 0.000	0.000 0.000	-0.066 0.018	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.138 0.087
LAT CL												0.000 0.000
JUL SEN CL	-0.018 0.152	0.000 0.000	0.000 0.000	0.000 0.000	-0.025 0.029	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.043 0.181
LAT CL												0.000 0.000
AUG SEN CL	-0.029 0.110	0.000 0.000	0.000 0.000	0.000 0.000	-0.036 0.022	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.065 0.132
LAT CL												0.000 0.000
SEP SEN CL	-0.202 0.017	0.000 0.000	0.000 0.000	0.000 0.000	-0.116 0.003	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.318 0.020
LAT CL												0.000 0.000
OCT SEN CL	-0.521 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.242 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.763 0.000
LAT CL												0.000 0.000
NOV SEN CL	-0.730 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.329 0.100	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-1.059 0.000
LAT CL												0.000 0.000
DEC SEN CL	-1.040 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.467 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-1.507 0.000
LAT CL												0.000 0.000
TOT	HEATING SEN CL	-6.666 0.350	0.000 0.000	0.000 0.000	-3.181 0.072	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-9.847 0.423
	LAT CL				0.304							0.304

Base Case Model-1

DOE-2.2-48r

WEATHER FILE- Toronto ON CWEC

REPORT- IS-E Space Monthly Load Components EII West Perim Plm (G.W9)

5/01/2016 20:26:47 BDL RUN 3

(UNITS=MBTU)	WALLS	ROOFS	INT SUR	UND SUR	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL
JAN SEN CL	-0.752 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.346 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-1.98
JAN LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
FEB SEN CL	-0.655 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.319 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.975
FEB LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
MAR SEN CL	-0.561 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.292 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.853
MAR LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
APR SEN CL	-0.340 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.195 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.535
APR LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
MAY SEN CL	-0.153 0.011	0.000 0.000	0.000 0.000	0.000 0.000	-0.110 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.263
MAY LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
JUN SEN CL	-0.030 0.091	0.000 0.000	0.000 0.000	0.000 0.000	-0.036 0.004	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.066
JUN LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
JUL SEN CL	-0.006 0.169	0.000 0.000	0.000 0.000	0.000 0.000	-0.011 0.014	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.017
JUL LAT CL					0.087							
AUG SEN CL	-0.002 0.157	0.000 0.000	0.000 0.000	0.000 0.000	-0.015 0.006	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.087
AUG LAT CL					0.075							
SEP SEN CL	-0.085 0.040	0.000 0.000	0.000 0.000	0.000 0.000	-0.072 0.003	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.157
SEP LAT CL					0.015							
OCT SEN CL	-0.295 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.161 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.457
OCT LAT CL					0.000							
NOV SEN CL	-0.463 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.219 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.682
NOV LAT CL					0.000							
DEC SEN CL	-0.677 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.311 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.988
DEC LAT CL					0.000							
TOT SEN CL	-4.019 0.468	0.000 0.000	0.000 0.000	0.000 0.000	-2.089 0.017	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-6.108 0.485
TOT LAT CL					0.220							0.220

Base Case Model-1

REPORT- LS-E Space Monthly Load Components EII Core Plnm (G.C10)

DOE-2.2-48r

5/01/2016

20:26:47

BDL RUN

3

WEATHER FILE- Toronto ON CWEC

(UNITS=MBTU)	WALLS	ROOFS	INT SUR	UND SUR	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL
HEATING	0.000	0.000	0.000	0.000	-0.229	0.000	0.000	0.000	0.000	0.000	0.000	-0.229
JAN SEN CL	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
LAT CL												
HEATING	0.000	0.000	0.000	0.000	-0.205	0.000	0.000	0.000	0.000	0.000	0.000	-0.205
FEB SEN CL	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
LAT CL												
HEATING	0.000	0.000	0.000	0.000	-0.185	0.000	0.000	0.000	0.000	0.000	0.000	-0.185
MAR SEN CL	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
LAT CL												
HEATING	0.000	0.000	0.000	0.000	-0.127	0.000	0.000	0.000	0.000	0.000	0.000	-0.127
APR SEN CL	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
LAT CL												
HEATING	0.000	0.000	0.000	0.000	-0.079	0.000	0.000	0.000	0.000	0.000	0.000	-0.079
MAY SEN CL	0.000	0.000	0.000	0.000	0.001	0.000	0.000	0.000	0.000	0.000	0.000	0.001
LAT CL												
HEATING	0.000	0.000	0.000	0.000	-0.036	0.000	0.000	0.000	0.000	0.000	0.000	-0.036
JUN SEN CL	0.000	0.000	0.000	0.000	0.008	0.000	0.000	0.000	0.000	0.000	0.000	0.000
LAT CL					0.016							
HEATING	0.000	0.000	0.000	0.000	-0.017	0.000	0.000	0.000	0.000	0.000	0.000	-0.017
JUL SEN CL	0.000	0.000	0.000	0.000	0.015	0.000	0.000	0.000	0.000	0.000	0.000	0.015
LAT CL					0.034							0.034
HEATING	0.000	0.000	0.000	0.000	-0.022	0.000	0.000	0.000	0.000	0.000	0.000	-0.022
AUG SEN CL	0.000	0.000	0.000	0.000	0.011	0.000	0.000	0.000	0.000	0.000	0.000	0.011
LAT CL					0.032							0.032
HEATING	0.000	0.000	0.000	0.000	-0.054	0.000	0.000	0.000	0.000	0.000	0.000	-0.054
SEP SEN CL	0.000	0.000	0.000	0.000	0.003	0.000	0.000	0.000	0.000	0.000	0.000	0.003
LAT CL					0.005							0.005
HEATING	0.000	0.000	0.000	0.000	-0.108	0.000	0.000	0.000	0.000	0.000	0.000	-0.108
OCT SEN CL	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
LAT CL					0.001							0.001
HEATING	0.000	0.000	0.000	0.000	-0.144	0.000	0.000	0.000	0.000	0.000	0.000	-0.144
NOV SEN CL	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
LAT CL					0.100							
HEATING	0.000	0.000	0.000	0.000	-0.200	0.000	0.000	0.000	0.000	0.000	0.000	-0.200
DEC SEN CL	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
LAT CL					0.000							
HEATING	0.000	0.000	0.000	0.000	-1.406	0.000	0.000	0.000	0.000	0.000	0.000	-1.406
TOT SEN CL	0.000	0.000	0.000	0.000	0.039	0.000	0.087	0.000	0.000	0.000	0.000	0.087
LAT CL												

Base Case Model-1

DOE-2.2-48r

5/01/2016

20:26:47

BDL RUN

3

REPORT- IS-E Space Monthly Load Components EII South Perim Spc (M.S11)

WEATHER FILE- Toronto ON CWEC

(UNITS=MBTU)	WALLS	ROOFS	INT SUR.	UND SUR.	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL
HEATING	-1.093	0.000	0.000	0.000	-1.046	-6.616	1.618	0.362	0.434	0.436	0.000	-5.905
JAN SEN CL	-0.369	0.000	0.000	0.000	-0.684	-2.696	5.676	1.213	0.438	0.746	0.000	4.323
LAT CL					0.000			0.997		0.000	0.000	0.997
HEATING	-0.905	0.000	0.000	0.000	-0.925	-5.622	1.521	0.418	0.434	0.447	0.000	-4.633
FEB SEN CL	-0.388	0.000	0.000	0.000	-0.670	-2.802	5.978	1.156	0.409	0.714	0.000	4.398
LAT CL					0.000			0.949		0.000	0.000	0.949
HEATING	-0.709	0.000	0.000	0.000	-0.785	-4.768	1.404	0.384	0.406	0.448	0.000	-3.621
MAR SEN CL	-0.368	0.000	0.000	0.000	-0.676	-2.899	6.634	1.520	0.470	0.939	0.000	5.620
LAT CL					0.000			1.244		0.000	0.000	1.244
HEATING	-0.369	0.000	0.000	0.000	-0.451	-2.856	0.893	0.202	0.228	0.300	0.000	-2.054
APR SEN CL	-0.285	0.000	0.000	0.000	-0.526	-2.475	6.415	1.622	0.501	1.029	0.000	6.280
LAT CL					0.006			1.311		0.000	0.000	1.317
HEATING	-0.173	0.000	0.000	0.000	-0.277	-1.830	0.674	0.104	0.137	0.213	0.000	-1.151
MAY SEN CL	-0.092	0.000	0.000	0.000	-0.290	-1.649	6.272	1.557	0.304	1.022	0.000	7.124
LAT CL					0.022			1.234		0.000	0.000	1.256
HEATING	-0.041	0.000	0.000	0.000	-0.108	-0.760	0.308	0.026	0.051	0.090	0.000	-0.433
JUN SEN CL	0.165	0.000	0.000	0.000	-0.053	-0.736	5.894	1.795	0.411	1.238	0.000	8.714
LAT CL					0.266			1.391		0.000	0.000	1.657
HEATING	-0.004	0.000	0.000	0.000	-0.045	-0.321	0.130	0.025	0.036	0.057	0.000	-0.122
JUL SEN CL	0.369	0.000	0.000	0.000	0.056	-0.197	5.883	1.719	0.499	1.228	0.000	9.558
LAT CL					0.459			1.330		0.000	0.000	1.789
HEATING	-0.003	0.000	0.000	0.000	-0.057	-0.408	0.182	0.018	0.035	0.062	0.000	-0.170
AUG SEN CL	0.410	0.000	0.000	0.000	0.009	-0.451	6.772	1.803	0.410	1.273	0.000	10.225
LAT CL					0.394			1.392		0.000	0.000	1.786
HEATING	-0.067	0.000	0.000	0.000	-0.141	-0.324	0.386	0.045	0.079	0.118	0.000	-0.502
SEP SEN CL	0.179	0.000	0.000	0.000	-0.233	-1.357	8.101	1.695	0.562	1.160	0.000	10.106
LAT CL					0.140			1.323		0.000	0.000	1.463
HEATING	-0.270	0.000	0.000	0.000	-0.352	-2.344	0.840	0.124	0.178	0.235	0.000	-1.590
OCT SEN CL	-0.173	0.000	0.000	0.000	-0.454	-2.200	7.313	1.537	0.614	0.999	0.000	7.637
LAT CL					0.032			1.232		0.000	0.000	1.264
HEATING	-0.625	0.000	0.000	0.000	-0.598	-3.863	0.795	0.269	0.377	0.359	0.000	-3.285
NOV SEN CL	-0.278	0.000	0.000	0.000	-0.499	-2.111	3.908	1.385	0.855	0.866	0.000	4.127
LAT CL					0.106			1.154		0.000	0.000	1.160
HEATING	-0.999	0.000	0.000	0.000	-0.948	-5.824	1.044	0.444	0.542	0.491	0.000	-5.251
DEC SEN CL	-0.386	0.000	0.000	0.000	-0.609	-2.433	4.402	1.301	0.628	0.795	0.000	3.697
LAT CL					0.000			1.085		0.000	0.000	1.085
HEATING	-5.259	0.000	0.000	0.000	-5.731	-36.135	9.795	2.420	2.938	3.256	0.000	-28.716
TOT SEN CL	-1.215	0.000	0.000	0.000	-4.630	-22.006	73.247	18.303	6.102	12.008	0.000	81.809
LAT CL					1.326			14.643		0.000	0.000	15.969

Base Case Model-1

DOE-2.2-48r

5/01/2016

20:26:47

BDL RUN

3

REPORT- LS-E Space Monthly Load Components EII East Perim Spc (M.E12)

WEATHER FILE- Toronto ON CWEC

(UNITS=MBTU)	WALLS	ROOFS	INT SUR	UND SUR	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL
HEATING	-0.912	0.000	0.000	0.000	-0.845	-5.132	0.727	0.363	0.387	0.371	0.000	-5.041
JAN SEN CL	-0.215	0.000	0.000	0.000	-0.308	-1.222	1.014	0.636	0.236	0.319	0.000	0.520
LAT CL					0.000			0.548		0.000	0.000	0.548
HEATING	-0.753	0.000	0.000	0.000	-0.742	-4.408	0.833	0.375	0.388	0.362	0.000	-3.945
FEB SEN CL	-0.222	0.000	0.000	0.000	-0.321	-1.338	1.465	0.623	0.212	0.375	0.000	0.794
LAT CL					0.000			0.537		0.000	0.000	0.537
HEATING	-0.537	0.000	0.000	0.000	-0.565	-3.490	0.847	0.285	0.297	0.315	0.000	-2.848
MAR SEN CL	-0.242	0.000	0.000	0.000	-0.408	-1.732	3.197	0.922	0.257	0.565	0.000	2.559
LAT CL					0.000			0.771		0.000	0.000	0.771
HEATING	-0.264	0.000	0.000	0.000	-0.305	-2.019	0.574	0.124	0.154	0.190	0.000	-1.546
APR SEN CL	-0.168	0.000	0.000	0.000	-0.347	-1.604	4.084	1.032	0.291	0.652	0.000	3.941
LAT CL					0.004			0.848		0.000	0.000	0.852
HEATING	-0.089	0.000	0.000	0.000	-0.149	-1.068	0.391	0.049	0.071	0.114	0.000	-0.679
MAY SEN CL	0.013	0.000	0.000	0.000	-0.229	-1.279	6.149	1.003	0.191	0.669	0.000	6.518
LAT CL					0.015			0.799		0.000	0.000	0.813
HEATING	-0.017	0.000	0.000	0.000	-0.060	-0.440	0.185	0.014	0.027	0.051	0.000	-0.240
JUN SEN CL	0.196	0.000	0.000	0.000	-0.047	-0.560	5.753	1.140	0.233	0.792	0.000	7.507
LAT CL					0.177			0.885		0.000	0.000	1.062
HEATING	-0.003	0.000	0.000	0.000	-0.024	-0.181	0.069	0.013	0.019	0.032	0.000	-0.074
JUL SEN CL	0.339	0.000	0.000	0.000	0.031	-0.157	5.682	1.092	0.291	0.783	0.000	8.062
LAT CL					0.307			0.846		0.000	0.000	1.153
HEATING	-0.003	0.000	0.000	0.000	-0.041	-0.300	0.126	0.015	0.026	0.046	0.000	-0.131
AUG SEN CL	0.297	0.000	0.000	0.000	0.009	-0.281	5.021	1.139	0.218	0.801	0.000	7.204
LAT CL					0.262			0.884		0.000	0.000	1.146
HEATING	-0.062	0.000	0.000	0.000	-0.113	-0.764	0.255	0.043	0.070	0.103	0.000	-0.468
SEP SEN CL	0.068	0.000	0.000	0.000	-0.136	-0.799	4.296	1.060	0.318	0.677	0.000	5.156
LAT CL					0.089			0.838		0.000	0.000	0.927
HEATING	-0.274	0.000	0.000	0.000	-0.293	-1.969	0.483	0.132	0.168	0.198	0.000	-1.554
OCT SEN CL	-0.147	0.000	0.000	0.000	-0.245	-1.141	2.471	0.921	0.387	0.585	0.000	2.830
LAT CL					0.019			0.756		0.000	0.000	0.776
HEATING	-0.510	0.000	0.000	0.000	-0.458	-2.981	0.445	0.216	0.293	0.267	0.000	-2.728
NOV SEN CL	-0.182	0.000	0.000	0.000	-0.274	-1.093	0.872	0.833	0.514	0.510	0.000	1.180
LAT CL					0.104			0.707		0.000	0.000	0.711
HEATING	-0.805	0.000	0.000	0.000	-0.754	-4.493	0.512	0.429	0.442	0.412	0.000	-4.256
DEC SEN CL	-0.206	0.000	0.000	0.000	-0.284	-1.133	0.748	0.677	0.360	0.403	0.000	0.564
LAT CL					0.000			0.579		0.000	0.000	0.579
HEATING	-4.226	0.000	0.000	0.000	-4.348	-27.245	5.447	2.059	2.340	2.463	0.000	-23.511
TOT SEN CL	-0.468	0.000	0.000	0.000	-2.558	-12.339	40.752	11.079	3.508	7.223	0.000	47.195
LAT CL					0.874			8.998		0.000	0.000	9.874

Base Case Model-1

DOE-2.2-48r

5/01/2016

20:26:47

BDL RUN

3

REPORT- LS-E Space Monthly Load Components EII North Perim Spc (M.N.13)

WEATHER FILE- Toronto ON CWEC

(UNITS=MBTU)	WALLS	ROOFS	INT SUR.	UND SUR.	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL
HEATING JAN SEN CL -0.196	0.000	0.000	0.000	-1.500	-8.511	0.939	0.969	0.802	0.831	0.000	-8.101	
LAT CL	0.000	0.000	0.000	-0.230	-0.957	0.313	0.606	0.449	0.351	0.000	0.335	
0.000	0.000	0.000	0.000	0.515	0.515	0.000	0.000	0.000	0.000	0.000	0.515	
HEATING FEB SEN CL -0.196	0.000	0.000	0.000	-1.349	-7.578	1.213	0.930	0.656	0.782	0.000	-6.765	
LAT CL	0.000	0.000	0.000	-0.246	-1.004	0.427	0.645	0.354	0.380	0.000	0.360	
0.000	0.000	0.000	0.000	0.554	0.554	0.000	0.000	0.000	0.000	0.000	0.554	
HEATING MAR SEN CL -0.355	0.000	0.000	0.000	-0.994	-5.962	1.193	0.617	0.490	0.613	0.000	-5.106	
LAT CL	0.000	0.000	0.000	-0.466	-1.845	1.235	1.287	0.409	0.773	0.000	1.037	
0.000	0.000	0.000	0.000	1.087	1.087	0.000	0.000	0.000	0.000	0.000	1.087	
HEATING APR SEN CL -0.359	0.000	0.000	0.000	-0.538	-3.496	0.831	0.268	0.267	0.358	0.000	-2.876	
LAT CL	0.000	0.000	0.000	-0.440	-1.920	2.231	1.555	0.455	0.970	0.000	2.493	
0.006	0.006	0.006	0.006	1.280	1.280	0.000	0.000	0.000	0.000	0.000	1.286	
HEATING MAY SEN CL -0.217	0.000	0.000	0.000	-0.296	-1.993	0.666	0.115	0.147	0.233	0.000	-1.365	
LAT CL	0.000	0.000	0.000	-0.271	-1.525	3.640	1.546	0.272	1.002	0.000	4.447	
0.021	0.021	0.021	0.021	1.241	1.241	0.000	0.000	0.000	0.000	0.000	1.263	
HEATING JUN SEN CL 0.051	0.000	0.000	0.000	-0.101	-0.735	0.263	0.029	0.048	0.096	0.000	-0.450	
LAT CL	0.000	0.000	0.000	-0.059	-0.763	4.515	1.792	0.374	1.232	0.000	7.142	
0.265	0.265	0.265	0.265	1.394	1.394	0.000	0.000	0.000	0.000	0.000	1.658	
HEATING JUL SEN CL 0.222	0.000	0.000	0.000	-0.046	-0.341	0.119	0.028	0.036	0.063	0.000	-0.150	
LAT CL	0.000	0.000	0.000	0.057	-0.182	4.120	1.716	0.454	1.222	0.000	7.610	
0.455	0.455	0.455	0.455	1.331	1.331	0.000	0.000	0.000	0.000	0.000	1.786	
HEATING AUG SEN CL 0.153	0.000	0.000	0.000	-0.079	-0.564	0.179	0.037	0.056	0.098	0.000	-0.295	
LAT CL	0.000	0.000	0.000	-0.031	-0.336	3.373	1.784	0.315	1.237	0.000	6.556	
0.387	0.387	0.387	0.387	1.389	1.389	0.000	0.000	0.000	0.000	0.000	1.776	
HEATING SEP SEN CL -0.129	0.000	0.000	0.000	-0.197	-1.324	0.307	0.090	0.128	0.194	0.000	-0.959	
LAT CL	0.000	0.000	0.000	-0.178	-1.020	2.341	1.651	0.522	1.083	0.000	4.271	
0.129	0.129	0.129	0.129	1.315	1.315	0.000	0.000	0.000	0.000	0.000	1.444	
HEATING OCT SEN CL -0.271	0.000	0.000	0.000	-0.471	-3.192	0.643	0.212	0.269	0.327	0.000	-2.747	
LAT CL	0.000	0.000	0.000	-0.335	-1.431	1.452	1.449	0.648	0.907	0.000	2.418	
0.027	0.027	0.027	0.027	1.200	1.200	0.000	0.000	0.000	0.000	0.000	1.227	
HEATING NOV SEN CL -0.305	0.000	0.000	0.000	-0.693	-4.472	0.511	0.343	0.465	0.425	0.000	-4.246	
LAT CL	0.000	0.000	0.000	-0.405	-1.590	0.677	1.311	0.910	0.800	0.000	1.399	
0.105	0.105	0.105	0.105	1.118	1.118	0.000	0.000	0.000	0.000	0.000	1.123	
HEATING DEC SEN CL -0.269	0.000	0.000	0.000	-1.236	-7.069	0.597	0.840	0.774	0.754	0.000	-6.682	
LAT CL	0.000	0.000	0.000	-0.320	-1.334	0.376	0.904	0.666	0.532	0.000	0.554	
0.000	0.000	0.000	0.000	0.774	0.774	0.000	0.000	0.000	0.000	0.000	0.774	
HEATING TOT SEN CL -1.871	0.000	0.000	0.000	-7.499	-45.238	7.462	4.477	4.137	4.775	0.000	-39.743	
LAT CL	1.295	1.295	1.295	-2.863	-13.906	24.699	16.246	5.827	10.489	0.000	38.620	
13.199	13.199	13.199	13.199	0.000	0.000	0.000	0.000	0.000	0.000	0.000	14.494	

Base Case Model-1

DOE-2.2-48r

5/01/2016

20:26:47

BDL RUN

3

REPORT- LS-E Space Monthly Load Components EII West Perim Spc (M.WL4)

WEATHER FILE- Toronto ON CWEC

(UNITS=MBTU)	WALLS	ROOFS	INT SUR	UND SUR	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL
HEATING	-0.972	0.000	0.000	0.000	-0.934	-5.524	0.934	0.526	0.415	0.477	0.000	-5.078
JAN SEN CL	-0.159	0.000	0.000	0.000	-0.219	-0.895	0.961	0.473	0.214	0.273	0.000	0.647
LAT CL					0.000			0.393			0.000	0.393
HEATING	-0.796	0.000	0.000	0.000	-0.798	-4.591	1.075	0.479	0.387	0.431	0.000	-3.914
FEB SEN CL	-0.191	0.000	0.000	0.000	-0.265	-1.125	1.527	0.519	0.194	0.306	0.000	0.965
LAT CL					0.000			0.430			0.000	0.430
HEATING	-0.570	0.000	0.000	0.000	-0.590	-3.607	0.968	0.333	0.300	0.346	0.000	-2.820
MAR SEN CL	-0.275	0.000	0.000	0.000	-0.384	-1.682	2.388	0.874	0.296	0.534	0.000	1.752
LAT CL					0.000			0.713			0.000	0.713
HEATING	-0.269	0.000	0.000	0.000	-0.302	-1.591	0.675	0.125	0.154	0.187	0.000	-1.420
APR SEN CL	-0.236	0.000	0.000	0.000	-0.350	-1.670	3.632	1.031	0.338	0.656	0.000	3.400
LAT CL					0.004			0.838			0.000	0.842
HEATING	-0.110	0.000	0.000	0.000	-0.168	-1.147	0.471	0.052	0.081	0.117	0.000	-0.705
MAY SEN CL	-0.095	0.000	0.000	0.000	-0.210	-1.225	4.526	1.000	0.217	0.666	0.000	4.881
LAT CL					0.016			0.793			0.000	0.809
HEATING	-0.021	0.000	0.000	0.000	-0.058	-0.406	0.211	0.012	0.026	0.044	0.000	-0.192
JUN SEN CL	0.121	0.000	0.000	0.000	-0.049	-0.594	5.294	1.142	0.276	0.798	0.000	6.988
LAT CL					0.178			0.883			0.000	1.061
HEATING	-0.003	0.000	0.000	0.000	-0.018	-0.126	0.059	0.009	0.015	0.021	0.000	-0.042
JUL SEN CL	0.256	0.000	0.000	0.000	0.026	-0.211	5.211	1.096	0.387	0.794	0.000	7.560
LAT CL					0.308			0.845			0.000	1.153
HEATING	-0.001	0.000	0.000	0.000	-0.029	-0.210	0.108	0.007	0.016	0.028	0.000	-0.080
AUG SEN CL	0.239	0.000	0.000	0.000	-0.003	-0.375	4.715	1.147	0.294	0.819	0.000	6.836
LAT CL					0.262			0.884			0.000	1.147
HEATING	-0.063	0.000	0.000	0.000	-0.106	-0.715	0.277	0.036	0.060	0.089	0.000	-0.422
SEP SEN CL	-0.001	0.000	0.000	0.000	-0.143	-0.856	3.661	1.068	0.390	0.721	0.000	4.840
LAT CL					0.092			0.839			0.000	0.930
HEATING	-0.264	0.000	0.000	0.000	-0.279	-1.913	0.584	0.107	0.140	0.182	0.000	-1.444
OCT SEN CL	-0.180	0.000	0.000	0.000	-0.259	-1.212	2.422	0.946	0.405	0.601	0.000	2.724
LAT CL					0.019			0.769			0.000	0.788
HEATING	-0.504	0.000	0.000	0.000	-0.458	-2.979	0.483	0.230	0.291	0.274	0.000	-2.662
NOV SEN CL	-0.195	0.000	0.000	0.000	-0.274	-1.131	0.941	0.818	0.546	0.503	0.000	1.208
LAT CL					0.004			0.690			0.000	0.694
HEATING	-0.845	0.000	0.000	0.000	-0.813	-4.755	0.592	0.524	0.472	0.477	0.000	-4.348
DEC SEN CL	-0.177	0.000	0.000	0.000	-0.225	-0.946	0.658	0.582	0.340	0.339	0.000	0.570
LAT CL					0.000			0.496			0.000	0.496
HEATING	-4.418	0.000	0.000	0.000	-4.552	-28.064	6.436	2.440	2.357	2.673	0.000	-23.126
TOT SEN CL	-0.894	0.000	0.000	0.000	-2.355	-11.923	35.937	10.697	3.896	7.012	0.000	42.370
LAT CL					0.882			8.573			0.000	9.455

Base Case Model-1

DOE-2.2-48r

5/01/2016

20:26:47

BDL RUN

3

REPORT- LS-E Space Monthly Load Components EII Core Spec (M.C115)

WEATHER FILE- Toronto ON CWEC

(UNITS=MBTU)	WALLS	ROOFS	INT SUR	UND SUR	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL
HEATING	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
JAN SEN CL	0.000	0.000	0.000	0.000	-0.229	0.000	0.000	28.940	9.581	7.723	0.000	46.015
LAT CL					0.000			23.172	0.000	0.000		23.172
HEATING	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
FEB SEN CL	0.000	0.000	0.000	0.000	-0.205	0.000	0.000	28.940	9.531	7.590	0.000	45.856
LAT CL					0.000			23.172	0.000	0.000		23.172
HEATING	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
MAR SEN CL	0.000	0.000	0.000	0.000	-0.185	0.000	0.000	35.009	11.483	9.061	0.000	55.368
LAT CL					0.000			28.050	0.000	0.000		28.050
HEATING	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
APR SEN CL	0.000	0.000	0.000	0.000	-0.127	0.000	0.000	33.510	10.995	8.678	0.000	53.056
LAT CL					0.001			26.831	0.000	0.000		26.831
HEATING	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
MAY SEN CL	0.000	0.000	0.000	0.000	-0.078	0.000	0.000	30.487	10.067	8.064	0.000	48.540
LAT CL					0.004			24.391	0.000	0.000		24.396
HEATING	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
JUN SEN CL	0.000	0.000	0.000	0.000	-0.028	0.000	0.000	33.486	10.988	8.678	0.000	53.125
LAT CL					0.030			26.831	0.000	0.000		26.831
HEATING	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
JUL SEN CL	0.000	0.000	0.000	0.000	-0.003	0.000	0.000	32.010	10.542	8.391	0.000	50.941
LAT CL					0.059			25.611	0.000	0.000		25.670
HEATING	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
AUG SEN CL	0.000	0.000	0.000	0.000	-0.011	0.000	0.000	33.486	11.006	8.726	0.000	53.208
LAT CL					0.053			26.831	0.000	0.000		26.884
HEATING	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
SEP SEN CL	0.000	0.000	0.000	0.000	-0.050	0.000	0.000	31.987	10.519	8.347	0.000	50.802
LAT CL					0.020			25.611	0.000	0.000		25.631
HEATING	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
OCT SEN CL	0.000	0.000	0.000	0.000	-0.108	0.000	0.000	30.487	10.066	8.060	0.000	48.506
LAT CL					0.006			24.391	0.000	0.000		24.398
HEATING	0.000	0.000	0.000	0.000	-0.144	0.000	0.000	30.432	10.030	8.005	0.000	48.323
NOV SEN CL	0.000	0.000	0.000	0.000	-0.001	0.000	0.000	30.432	10.030	8.005	0.000	48.323
LAT CL					0.001			24.391	0.000	0.000		24.392
HEATING	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
DEC SEN CL	0.000	0.000	0.000	0.000	-0.200	0.000	0.000	32.018	10.546	8.396	0.000	50.760
LAT CL					0.175			25.611	0.000	0.000		25.611
HEATING	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
TOT SEN CL	0.000	0.000	0.000	0.000	-1.368	0.000	0.000	380.794	125.354	99.719	0.000	604.499
LAT CL					0.175			304.895	0.000	0.000		305.070

Base Case Model-1

DOE-2.2-48r

WEATHER FILE- Toronto ON CWEC

REPORT- LS-E Space Monthly Load Components EII South Perim Plnm (M.S16)

5/01/2016 20:26:47 BDL RUN 3

(UNITS=MBTU)	WALLS	ROOFS	INT SUR.	UND SUR.	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL
HEATING JAN SEN CL 0.000 0.000 0.000 0.000 -0.519 0.000 0.000 0.000 0.000 0.000 0.000 -1.471												
HEATING FEB SEN CL 0.000 0.000 0.000 0.000 -0.479 0.000 0.000 0.000 0.000 0.000 0.000 0.000												
HEATING MAR SEN CL 0.000 0.000 0.000 0.000 -0.438 0.000 0.000 0.000 0.000 0.000 0.000 0.000												
HEATING APR SEN CL 0.003 0.000 0.000 0.000 -0.292 0.000 0.000 0.000 0.000 0.000 0.000 0.000												
HEATING MAY SEN CL 0.023 0.000 0.000 0.000 -0.164 0.000 0.000 0.000 0.000 0.000 0.000 0.000												
HEATING JUN SEN CL 0.125 0.000 0.000 0.000 -0.059 0.000 0.000 0.000 0.000 0.000 0.000 0.000												
HEATING JUL SEN CL 0.242 0.000 0.000 0.000 -0.021 0.000 0.000 0.000 0.000 0.000 0.000 0.000												
HEATING AUG SEN CL 0.265 0.000 0.000 0.000 -0.025 0.000 0.000 0.000 0.000 0.000 0.000 0.000												
HEATING SEP SEN CL 0.131 0.000 0.000 0.000 -0.093 0.000 0.000 0.000 0.000 0.000 0.000 0.000												
HEATING OCT SEN CL 0.014 0.000 0.000 0.000 -0.237 0.000 0.000 0.000 0.000 0.000 0.000 0.000												
HEATING NOV SEN CL 0.001 0.000 0.000 0.000 -0.328 0.000 0.000 0.000 0.000 0.000 0.000 0.000												
HEATING DEC SEN CL 0.000 0.000 0.000 0.000 -0.467 0.000 0.000 0.000 0.000 0.000 0.000 0.000												
HEATING TOT SEN CL 0.805 0.000 0.000 0.000 -3.123 0.000 0.000 0.000 0.000 0.000 0.000 -8.164												
HEATING LAT CL 0.335 0.000 0.000 0.000 0.14 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.335												

Base Case Model-1

DOE-2.2-48r

5/01/2016

20:26:47

BDL RUN

3

REPORT- LS-E Space Monthly Load Components EII East Perim Plm (M.E.I7)

WEATHER FILE- Toronto ON CWEC

(UNITS=MBTU)	WALLS	ROOFS	INT SUR	UND SUR	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL
HEATING JAN SEN CL 0.000	0.000	0.000	0.000	-0.346	0.000	0.000	0.000	0.000	0.000	0.000	-1.94	
HEATING FEB SEN CL 0.000	0.000	0.000	0.000	-0.319	0.000	0.000	0.000	0.000	0.000	0.000	-0.966	
HEATING MAR SEN CL 0.000	0.000	0.000	0.000	-0.292	0.000	0.000	0.000	0.000	0.000	0.000	-0.810	
HEATING APR SEN CL 0.003	0.000	0.000	0.000	-0.195	0.000	0.000	0.000	0.000	0.000	0.000	-0.487	
HEATING MAY SEN CL 0.038	0.000	0.000	0.000	-0.104	0.000	0.000	0.000	0.000	0.000	0.000	0.002	
HEATING JUN SEN CL 0.131	0.000	0.000	0.000	-0.035	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
HEATING JUL SEN CL 0.224	0.000	0.000	0.000	-0.013	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
HEATING AUG SEN CL 0.195	0.000	0.000	0.000	-0.017	0.000	0.000	0.000	0.000	0.000	0.000	-0.198	
HEATING SEP SEN CL 0.060	0.000	0.000	0.000	-0.008	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
HEATING OCT SEN CL 0.001	0.000	0.000	0.000	-0.005	0.000	0.000	0.000	0.000	0.000	0.000	-0.019	
HEATING NOV SEN CL 0.000	0.000	0.000	0.000	-0.019	0.000	0.000	0.000	0.000	0.000	0.000	-0.050	
HEATING DEC SEN CL 0.000	0.000	0.000	0.000	-0.311	0.000	0.000	0.000	0.000	0.000	0.000	-0.981	
HEATING TOT SEN CL 0.653	0.000	0.000	0.000	-2.083	0.000	0.000	0.000	0.000	0.000	0.000	-5.867	
				0.010	0.000	0.000	0.000	0.000	0.000	0.000	0.663	
				0.223							0.223	

Base Case Model-1

DOE-2.2-48r

5/01/2016

20:26:47

BDL RUN

3

REPORT- LS-E Space Monthly Load Components ELL North Perim Plnm (M.N18)

WEATHER FILE- Toronto ON CWEC

(UNITS=MBTU)	WALLS	ROOFS	INT SUR.	UND SUR.	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL
HEATING JAN SEN CL 0.000	0.000	0.000	0.000	-0.519	0.000	0.000	0.000	0.000	0.000	0.000	-1.705	
HEATING FEB SEN CL 0.000	0.000	0.000	0.000	-0.479	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
HEATING MAR SEN CL 0.000	0.000	0.000	0.000	-0.438	0.000	0.000	0.000	0.000	0.000	0.000	-1.523	
HEATING APR SEN CL 0.000	0.000	0.000	0.000	-0.293	0.000	0.000	0.000	0.000	0.000	0.000	-0.896	
HEATING MAY SEN CL 0.001	0.000	0.000	0.000	-0.170	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
HEATING JUN SEN CL 0.070	0.000	0.000	0.000	-0.066	0.000	0.000	0.000	0.000	0.000	0.000	-0.472	
HEATING JUL SEN CL 0.152	0.000	0.000	0.000	-0.025	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
HEATING AUG SEN CL 0.110	0.000	0.000	0.000	-0.036	0.000	0.000	0.000	0.000	0.000	0.000	-0.138	
HEATING SEP SEN CL 0.017	0.000	0.000	0.000	-0.022	0.000	0.000	0.000	0.000	0.000	0.000	0.087	
HEATING OCT SEN CL 0.000	0.000	0.000	0.000	-0.116	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
HEATING NOV SEN CL 0.000	0.000	0.000	0.000	-0.329	0.000	0.000	0.000	0.000	0.000	0.000	-0.318	
HEATING DEC SEN CL 0.000	0.000	0.000	0.000	-0.467	0.000	0.000	0.000	0.000	0.000	0.000	-1.507	
HEATING TOT SEN CL 0.350	0.000	0.000	0.000	-3.181	0.000	0.000	0.000	0.000	0.000	0.000	-9.847	
				0.072	0.000	0.000	0.000	0.000	0.000	0.000	0.423	
				0.304							0.304	

Base Case Model-1

DOE-2.2-48r

5/01/2016

20:26:47

BDL RUN

3

REPORT- IS-E Space Monthly Load Components EII West Perim Plm (M.W19)

WEATHER FILE- Toronto ON CWEC

(UNITS=MBTU)	WALLS	ROOFS	INT SUR	UND SUR	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL
JAN SEN CL	-0.752 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.346 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-1.98
JAN LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
FEB SEN CL	-0.655 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.319 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.975
FEB LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
MAR SEN CL	-0.561 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.292 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.853
MAR LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
APR SEN CL	-0.340 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.195 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.535
APR LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
MAY SEN CL	-0.153 0.011	0.000 0.000	0.000 0.000	0.000 0.000	-0.110 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.263
MAY LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
JUN SEN CL	-0.030 0.091	0.000 0.000	0.000 0.000	0.000 0.000	-0.036 0.004	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.066
JUN LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
JUL SEN CL	-0.006 0.169	0.000 0.000	0.000 0.000	0.000 0.000	-0.011 0.014	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.017
JUL LAT CL					0.087							
AUG SEN CL	-0.002 0.157	0.000 0.000	0.000 0.000	0.000 0.000	-0.015 0.006	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.087
AUG LAT CL					0.075							
SEP SEN CL	-0.085 0.040	0.000 0.000	0.000 0.000	0.000 0.000	-0.072 0.003	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.157
SEP LAT CL					0.015							
OCT SEN CL	-0.295 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.161 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.457
OCT LAT CL					0.000							
NOV SEN CL	-0.463 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.219 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.682
NOV LAT CL					0.100							
DEC SEN CL	-0.677 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.311 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.988
DEC LAT CL					0.000							
TOT SEN CL	-4.019 0.468	0.000 0.000	0.000 0.000	0.000 0.000	-2.089 0.017	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-6.108 0.485
TOT LAT CL					0.220							0.220

Base Case Model-1

REPORT- LS-E Space Monthly Load Components EII Core Plnm (M.C20)

DOE-2.2-48r

5/01/2016

20:26:47

BDL RUN

3

WEATHER FILE- Toronto ON CWEC

(UNITS=MBTU)	WALLS	ROOFS	INT SUR	UND SUR	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL
HEATING	0.000	0.000	0.000	0.000	-0.229	0.000	0.000	0.000	0.000	0.000	0.000	-0.229
JAN SEN CL	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
LAT CL												
HEATING	0.000	0.000	0.000	0.000	-0.205	0.000	0.000	0.000	0.000	0.000	0.000	-0.205
FEB SEN CL	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
LAT CL												
HEATING	0.000	0.000	0.000	0.000	-0.185	0.000	0.000	0.000	0.000	0.000	0.000	-0.185
MAR SEN CL	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
LAT CL												
HEATING	0.000	0.000	0.000	0.000	-0.127	0.000	0.000	0.000	0.000	0.000	0.000	-0.127
APR SEN CL	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
LAT CL												
HEATING	0.000	0.000	0.000	0.000	-0.079	0.000	0.000	0.000	0.000	0.000	0.000	-0.079
MAY SEN CL	0.000	0.000	0.000	0.000	0.001	0.000	0.000	0.000	0.000	0.000	0.000	0.001
LAT CL												
HEATING	0.000	0.000	0.000	0.000	-0.036	0.000	0.000	0.000	0.000	0.000	0.000	-0.036
JUN SEN CL	0.000	0.000	0.000	0.000	0.008	0.000	0.000	0.000	0.000	0.000	0.000	0.000
LAT CL					0.016							
HEATING	0.000	0.000	0.000	0.000	-0.017	0.000	0.000	0.000	0.000	0.000	0.000	-0.017
JUL SEN CL	0.000	0.000	0.000	0.000	0.015	0.000	0.000	0.000	0.000	0.000	0.000	0.015
LAT CL					0.034							0.034
HEATING	0.000	0.000	0.000	0.000	-0.022	0.000	0.000	0.000	0.000	0.000	0.000	-0.022
AUG SEN CL	0.000	0.000	0.000	0.000	0.011	0.000	0.000	0.000	0.000	0.000	0.000	0.011
LAT CL					0.032							0.032
HEATING	0.000	0.000	0.000	0.000	-0.054	0.000	0.000	0.000	0.000	0.000	0.000	-0.054
SEP SEN CL	0.000	0.000	0.000	0.000	0.003	0.000	0.000	0.000	0.000	0.000	0.000	0.003
LAT CL					0.005							0.005
HEATING	0.000	0.000	0.000	0.000	-0.108	0.000	0.000	0.000	0.000	0.000	0.000	-0.108
OCT SEN CL	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
LAT CL					0.001							0.001
HEATING	0.000	0.000	0.000	0.000	-0.144	0.000	0.000	0.000	0.000	0.000	0.000	-0.144
NOV SEN CL	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
LAT CL					0.100							
HEATING	0.000	0.000	0.000	0.000	-0.200	0.000	0.000	0.000	0.000	0.000	0.000	-0.200
DEC SEN CL	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
LAT CL					0.000							
HEATING	0.000	0.000	0.000	0.000	-1.406	0.000	0.000	0.000	0.000	0.000	0.000	-1.406
TOT SEN CL	0.000	0.000	0.000	0.000	0.039	0.000	0.087	0.000	0.000	0.000	0.000	0.087
LAT CL												

Base Case Model-1

DOE-2.2-48r

5/01/2016

20:26:47

BDL RUN

3

REPORT- LS-E Space Monthly Load Components EII South Perim Spc (T.S21)

WEATHER FILE- Toronto ON CWEC

(UNITS=MBTU)	WALLS	ROOFS	INT SUR.	UND SUR.	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL
HEATING	-1.093	0.000	0.000	0.000	-1.046	-6.616	1.618	0.362	0.434	0.436	0.000	-5.905
JAN SEN CL	-0.369	0.000	0.000	0.000	-0.684	-2.696	5.676	1.213	0.438	0.746	0.000	4.323
LAT CL					0.000			0.997		0.000	0.000	0.997
HEATING	-0.905	0.000	0.000	0.000	-0.925	-5.622	1.521	0.418	0.434	0.447	0.000	-4.633
FEB SEN CL	-0.388	0.000	0.000	0.000	-0.670	-2.802	5.978	1.156	0.409	0.714	0.000	4.398
LAT CL					0.000			0.949		0.000	0.000	0.949
HEATING	-0.709	0.000	0.000	0.000	-0.785	-4.768	1.404	0.384	0.406	0.448	0.000	-3.621
MAR SEN CL	-0.368	0.000	0.000	0.000	-0.676	-2.899	6.634	1.520	0.470	0.939	0.000	5.620
LAT CL					0.000			1.244		0.000	0.000	1.244
HEATING	-0.369	0.000	0.000	0.000	-0.451	-2.856	0.893	0.202	0.228	0.300	0.000	-2.054
APR SEN CL	-0.285	0.000	0.000	0.000	-0.526	-2.475	6.415	1.622	0.501	1.029	0.000	6.280
LAT CL					0.006			1.311		0.000	0.000	1.317
HEATING	-0.173	0.000	0.000	0.000	-0.277	-1.830	0.674	0.104	0.137	0.213	0.000	-1.151
MAY SEN CL	-0.092	0.000	0.000	0.000	-0.290	-1.649	6.272	1.557	0.304	1.022	0.000	7.124
LAT CL					0.022			1.234		0.000	0.000	1.256
HEATING	-0.041	0.000	0.000	0.000	-0.108	-0.760	0.308	0.026	0.051	0.090	0.000	-0.433
JUN SEN CL	0.165	0.000	0.000	0.000	-0.053	-0.736	5.894	1.795	0.411	1.238	0.000	8.714
LAT CL					0.266			1.391		0.000	0.000	1.657
HEATING	-0.004	0.000	0.000	0.000	-0.045	-0.321	0.130	0.025	0.036	0.057	0.000	-0.122
JUL SEN CL	0.369	0.000	0.000	0.000	0.056	-0.197	5.883	1.719	0.499	1.228	0.000	9.558
LAT CL					0.459			1.330		0.000	0.000	1.789
HEATING	-0.003	0.000	0.000	0.000	-0.057	-0.408	0.182	0.018	0.035	0.062	0.000	-0.170
AUG SEN CL	0.410	0.000	0.000	0.000	0.009	-0.451	6.772	1.803	0.410	1.273	0.000	10.225
LAT CL					0.394			1.392		0.000	0.000	1.786
HEATING	-0.067	0.000	0.000	0.000	-0.141	-0.324	0.386	0.045	0.079	0.118	0.000	-0.502
SEP SEN CL	0.179	0.000	0.000	0.000	-0.233	-1.357	8.101	1.695	0.562	1.160	0.000	10.106
LAT CL					0.140			1.323		0.000	0.000	1.463
HEATING	-0.270	0.000	0.000	0.000	-0.352	-2.344	0.840	0.124	0.178	0.235	0.000	-1.590
OCT SEN CL	-0.173	0.000	0.000	0.000	-0.454	-2.200	7.313	1.537	0.614	0.999	0.000	7.637
LAT CL					0.032			1.232		0.000	0.000	1.264
HEATING	-0.625	0.000	0.000	0.000	-0.598	-3.863	0.795	0.269	0.377	0.359	0.000	-3.285
NOV SEN CL	-0.278	0.000	0.000	0.000	-0.499	-2.111	3.908	1.385	0.855	0.866	0.000	4.127
LAT CL					0.106			1.154		0.000	0.000	1.160
HEATING	-0.999	0.000	0.000	0.000	-0.948	-5.824	1.044	0.444	0.542	0.491	0.000	-5.251
DEC SEN CL	-0.386	0.000	0.000	0.000	-0.609	-2.433	4.402	1.301	0.628	0.795	0.000	3.697
LAT CL					0.000			1.085		0.000	0.000	1.085
HEATING	-5.259	0.000	0.000	0.000	-5.731	-36.135	9.795	2.420	2.938	3.256	0.000	-28.716
TOT SEN CL	-1.215	0.000	0.000	0.000	-4.630	-22.006	73.247	18.303	6.102	12.008	0.000	81.809
LAT CL					1.326			14.643		0.000	0.000	15.969

Base Case Model-1

DOE-2.2-48r

5/01/2016

20:26:47

BDL RUN

3

REPORT- LS-E Space Monthly Load Components EII East Perim Spc (T.E22)

WEATHER FILE- Toronto ON CWEC

(UNITS=MBTU)	WALLS	ROOFS	INT SUR	UND SUR	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL
HEATING	-0.912	0.000	0.000	0.000	-0.845	-5.132	0.727	0.363	0.387	0.371	0.000	-5.041
JAN SEN CL	-0.215	0.000	0.000	0.000	-0.308	-1.222	1.014	0.636	0.236	0.319	0.000	0.520
LAT CL					0.000			0.548		0.000	0.000	0.548
HEATING	-0.753	0.000	0.000	0.000	-0.742	-4.408	0.833	0.375	0.388	0.362	0.000	-3.945
FEB SEN CL	-0.222	0.000	0.000	0.000	-0.321	-1.338	1.465	0.623	0.212	0.375	0.000	0.794
LAT CL					0.000			0.537		0.000	0.000	0.537
HEATING	-0.537	0.000	0.000	0.000	-0.565	-3.490	0.847	0.285	0.297	0.315	0.000	-2.848
MAR SEN CL	-0.242	0.000	0.000	0.000	-0.408	-1.732	3.197	0.922	0.257	0.565	0.000	2.559
LAT CL					0.000			0.771		0.000	0.000	0.771
HEATING	-0.264	0.000	0.000	0.000	-0.305	-2.019	0.574	0.124	0.154	0.190	0.000	-1.546
APR SEN CL	-0.168	0.000	0.000	0.000	-0.347	-1.604	4.084	1.032	0.291	0.652	0.000	3.941
LAT CL					0.004			0.848		0.000	0.000	0.852
HEATING	-0.089	0.000	0.000	0.000	-0.149	-1.068	0.391	0.049	0.071	0.114	0.000	-0.679
MAY SEN CL	0.013	0.000	0.000	0.000	-0.229	-1.279	6.149	1.003	0.191	0.669	0.000	6.518
LAT CL					0.015			0.799		0.000	0.000	0.813
HEATING	-0.017	0.000	0.000	0.000	-0.060	-0.440	0.185	0.014	0.027	0.051	0.000	-0.240
JUN SEN CL	0.196	0.000	0.000	0.000	-0.047	-0.560	5.753	1.140	0.233	0.792	0.000	7.507
LAT CL					0.177			0.885		0.000	0.000	1.062
HEATING	-0.003	0.000	0.000	0.000	-0.024	-0.181	0.069	0.013	0.019	0.032	0.000	-0.074
JUL SEN CL	0.339	0.000	0.000	0.000	0.031	-0.157	5.682	1.092	0.291	0.783	0.000	8.062
LAT CL					0.307			0.846		0.000	0.000	1.153
HEATING	-0.003	0.000	0.000	0.000	-0.041	-0.300	0.126	0.015	0.026	0.046	0.000	-0.131
AUG SEN CL	0.297	0.000	0.000	0.000	-0.009	-0.281	5.021	1.139	0.218	0.801	0.000	7.204
LAT CL					0.262			0.884		0.000	0.000	1.146
HEATING	-0.062	0.000	0.000	0.000	-0.113	-0.764	0.255	0.043	0.070	0.103	0.000	-0.468
SEP SEN CL	0.068	0.000	0.000	0.000	-0.136	-0.799	4.296	1.060	0.318	0.627	0.000	5.156
LAT CL					0.089			0.838		0.000	0.000	0.927
HEATING	-0.274	0.000	0.000	0.000	-0.293	-1.969	0.483	0.132	0.168	0.198	0.000	-1.554
OCT SEN CL	-0.147	0.000	0.000	0.000	-0.245	-1.141	2.471	0.921	0.387	0.585	0.000	2.830
LAT CL					0.019			0.756		0.000	0.000	0.776
HEATING	-0.510	0.000	0.000	0.000	-0.458	-2.981	0.445	0.216	0.293	0.267	0.000	-2.728
NOV SEN CL	-0.182	0.000	0.000	0.000	-0.274	-1.093	0.872	0.833	0.514	0.510	0.000	1.180
LAT CL					0.104			0.707		0.000	0.000	0.711
HEATING	-0.805	0.000	0.000	0.000	-0.754	-4.493	0.512	0.429	0.442	0.412	0.000	-4.256
DEC SEN CL	-0.206	0.000	0.000	0.000	-0.284	-1.133	0.748	0.677	0.360	0.403	0.000	0.564
LAT CL					0.000			0.579		0.000	0.000	0.579
HEATING	-4.226	0.000	0.000	0.000	-4.348	-27.245	5.447	2.059	2.340	2.463	0.000	-23.511
TOT SEN CL	-0.468	0.000	0.000	0.000	-2.558	-12.339	40.752	11.079	3.508	7.223	0.000	47.195
LAT CL					0.874			8.998		0.000	0.000	9.874

Base Case Model-1

DOE-2.2-48r

5/01/2016

20:26:47

BDL RUN

3

REPORT- IS-E Space Monthly Load Components EII North Perim Spc (T.N23)

WEATHER FILE- Toronto ON CWEC

(UNITS=MBTU)	WALLS	ROOFS	INT SUR.	UND SUR.	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL
HEATING JAN SEN CL -0.196	0.000	0.000	0.000	-1.500	-8.511	0.939	0.969	0.802	0.831	0.000	-8.101	
LAT CL	0.000	0.000	0.000	-0.230	-0.957	0.313	0.606	0.449	0.351	0.000	0.335	
0.000	0.000	0.000	0.000	0.515	0.515	0.000	0.000	0.000	0.000	0.000	0.515	
HEATING FEB SEN CL -0.196	0.000	0.000	0.000	-1.349	-7.578	1.213	0.930	0.656	0.782	0.000	-6.765	
LAT CL	0.000	0.000	0.000	-0.246	-1.004	0.427	0.645	0.354	0.380	0.000	0.360	
0.000	0.000	0.000	0.000	0.554	0.554	0.000	0.000	0.000	0.000	0.000	0.554	
HEATING MAR SEN CL -0.355	0.000	0.000	0.000	-0.994	-5.962	1.193	0.617	0.490	0.613	0.000	-5.106	
LAT CL	0.000	0.000	0.000	-0.466	-1.845	1.235	1.287	0.409	0.773	0.000	1.037	
0.000	0.000	0.000	0.000	1.087	1.087	0.000	0.000	0.000	0.000	0.000	1.087	
HEATING APR SEN CL -0.359	0.000	0.000	0.000	-0.538	-3.496	0.831	0.268	0.267	0.358	0.000	-2.876	
LAT CL	0.000	0.000	0.000	-0.440	-1.920	2.231	1.555	0.455	0.970	0.000	2.493	
0.006	0.006	0.006	0.006	1.280	1.280	0.000	0.000	0.000	0.000	0.000	1.286	
HEATING MAY SEN CL -0.217	0.000	0.000	0.000	-0.296	-1.993	0.666	0.115	0.147	0.233	0.000	-1.365	
LAT CL	0.000	0.000	0.000	-0.271	-1.525	3.640	1.546	0.272	1.002	0.000	4.447	
0.021	0.021	0.021	0.021	1.241	1.241	0.000	0.000	0.000	0.000	0.000	1.263	
HEATING JUN SEN CL 0.051	0.000	0.000	0.000	-0.101	-0.735	0.263	0.029	0.048	0.096	0.000	-0.450	
LAT CL	0.000	0.000	0.000	-0.059	-0.763	4.515	1.792	0.374	1.232	0.000	7.142	
0.265	0.265	0.265	0.265	1.394	1.394	0.000	0.000	0.000	0.000	0.000	1.658	
HEATING JUL SEN CL 0.222	0.000	0.000	0.000	-0.046	-0.341	0.119	0.028	0.036	0.063	0.000	-0.150	
LAT CL	0.000	0.000	0.000	0.057	-0.182	4.120	1.716	0.454	1.222	0.000	7.610	
0.455	0.455	0.455	0.455	1.331	1.331	0.000	0.000	0.000	0.000	0.000	1.786	
HEATING AUG SEN CL 0.153	0.000	0.000	0.000	-0.079	-0.564	0.179	0.037	0.056	0.098	0.000	-0.295	
LAT CL	0.000	0.000	0.000	-0.031	-0.336	3.373	1.784	0.315	1.237	0.000	6.556	
0.387	0.387	0.387	0.387	1.389	1.389	0.000	0.000	0.000	0.000	0.000	1.776	
HEATING SEP SEN CL -0.129	0.000	0.000	0.000	-0.197	-1.324	0.307	0.090	0.128	0.194	0.000	-0.959	
LAT CL	0.000	0.000	0.000	-0.178	-1.020	2.341	1.651	0.522	1.083	0.000	4.271	
0.129	0.129	0.129	0.129	1.315	1.315	0.000	0.000	0.000	0.000	0.000	1.444	
HEATING OCT SEN CL -0.271	0.000	0.000	0.000	-0.471	-3.192	0.643	0.212	0.269	0.327	0.000	-2.747	
LAT CL	0.000	0.000	0.000	-0.335	-1.431	1.452	1.449	0.648	0.907	0.000	2.418	
0.027	0.027	0.027	0.027	1.200	1.200	0.000	0.000	0.000	0.000	0.000	1.227	
HEATING NOV SEN CL -0.305	0.000	0.000	0.000	-0.693	-4.472	0.511	0.343	0.465	0.425	0.000	-4.246	
LAT CL	0.000	0.000	0.000	-0.405	-1.590	0.677	1.311	0.910	0.800	0.000	1.399	
0.105	0.105	0.105	0.105	1.118	1.118	0.000	0.000	0.000	0.000	0.000	1.123	
HEATING DEC SEN CL -0.269	0.000	0.000	0.000	-1.236	-7.069	0.597	0.840	0.774	0.754	0.000	-6.682	
LAT CL	0.000	0.000	0.000	-0.320	-1.334	0.376	0.904	0.666	0.532	0.000	0.554	
0.000	0.000	0.000	0.000	0.774	0.774	0.000	0.000	0.000	0.000	0.000	0.774	
HEATING TOT SEN CL -1.871	0.000	0.000	0.000	-7.499	-45.238	7.462	4.477	4.137	4.775	0.000	-39.743	
LAT CL	1.295	1.295	1.295	-2.863	-13.906	24.699	16.246	5.827	10.489	0.000	38.620	
13.199	13.199	13.199	13.199	0.000	0.000	0.000	0.000	0.000	0.000	0.000	14.494	

Base Case Model-1

DOE-2.2-48r

5/01/2016

20:26:47

BDL RUN

3

REPORT- LS-E Space Monthly Load Components EII West Perim Spc (T_W24)

WEATHER FILE- Toronto ON CWEC

(UNITS=MBTU)	WALLS	ROOFS	INT SUR	UND SUR	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL
HEATING	-0.972	0.000	0.000	0.000	-0.934	-5.524	0.934	0.526	0.415	0.477	0.000	-5.078
JAN SEN CL	-0.159	0.000	0.000	0.000	-0.219	-0.895	0.961	0.473	0.214	0.273	0.000	0.647
LAT CL					0.000			0.393			0.000	0.393
HEATING	-0.796	0.000	0.000	0.000	-0.798	-4.591	1.075	0.479	0.387	0.431	0.000	-3.914
FEB SEN CL	-0.191	0.000	0.000	0.000	-0.265	-1.125	1.527	0.519	0.194	0.306	0.000	0.965
LAT CL					0.000			0.430			0.000	0.430
HEATING	-0.570	0.000	0.000	0.000	-0.590	-3.607	0.968	0.333	0.300	0.346	0.000	-2.820
MAR SEN CL	-0.275	0.000	0.000	0.000	-0.384	-1.682	2.388	0.874	0.296	0.534	0.000	1.752
LAT CL					0.000			0.713			0.000	0.713
HEATING	-0.269	0.000	0.000	0.000	-0.302	-1.591	0.675	0.125	0.154	0.187	0.000	-1.420
APR SEN CL	-0.236	0.000	0.000	0.000	-0.350	-1.670	3.632	1.031	0.338	0.656	0.000	3.400
LAT CL					0.004			0.838			0.000	0.842
HEATING	-0.110	0.000	0.000	0.000	-0.168	-1.147	0.471	0.052	0.081	0.117	0.000	-0.705
MAY SEN CL	-0.095	0.000	0.000	0.000	-0.210	-1.225	4.526	1.000	0.217	0.666	0.000	4.881
LAT CL					0.016			0.793			0.000	0.809
HEATING	-0.021	0.000	0.000	0.000	-0.058	-0.406	0.211	0.012	0.026	0.044	0.000	-0.192
JUN SEN CL	0.121	0.000	0.000	0.000	-0.049	-0.594	5.294	1.142	0.276	0.798	0.000	6.988
LAT CL					0.178			0.883			0.000	1.061
HEATING	-0.003	0.000	0.000	0.000	-0.018	-0.126	0.059	0.009	0.015	0.021	0.000	-0.042
JUL SEN CL	0.256	0.000	0.000	0.000	0.026	-0.211	5.211	1.096	0.387	0.794	0.000	7.560
LAT CL					0.308			0.845			0.000	1.153
HEATING	-0.001	0.000	0.000	0.000	-0.029	-0.210	0.108	0.007	0.016	0.028	0.000	-0.080
AUG SEN CL	0.239	0.000	0.000	0.000	-0.003	-0.375	4.715	1.147	0.294	0.819	0.000	6.836
LAT CL					0.262			0.884			0.000	1.147
HEATING	-0.063	0.000	0.000	0.000	-0.106	-0.715	0.277	0.036	0.060	0.089	0.000	-0.422
SEP SEN CL	-0.001	0.000	0.000	0.000	-0.143	-0.856	3.661	1.068	0.390	0.721	0.000	4.840
LAT CL					0.092			0.839			0.000	0.930
HEATING	-0.264	0.000	0.000	0.000	-0.279	-1.913	0.584	0.107	0.140	0.182	0.000	-1.444
OCT SEN CL	-0.180	0.000	0.000	0.000	-0.259	-1.212	2.422	0.946	0.405	0.601	0.000	2.724
LAT CL					0.019			0.769			0.000	0.788
HEATING	-0.504	0.000	0.000	0.000	-0.458	-2.979	0.483	0.230	0.291	0.274	0.000	-2.662
NOV SEN CL	-0.195	0.000	0.000	0.000	-0.274	-1.131	0.941	0.818	0.546	0.503	0.000	1.208
LAT CL					0.004			0.690			0.000	0.694
HEATING	-0.845	0.000	0.000	0.000	-0.813	-4.755	0.592	0.524	0.472	0.477	0.000	-4.348
DEC SEN CL	-0.177	0.000	0.000	0.000	-0.225	-0.946	0.658	0.582	0.340	0.339	0.000	0.570
LAT CL					0.000			0.496			0.000	0.496
HEATING	-4.418	0.000	0.000	0.000	-4.552	-28.064	6.436	2.440	2.357	2.673	0.000	-23.126
TOT SEN CL	-0.894	0.000	0.000	0.000	-2.355	-11.923	35.937	10.697	3.896	7.012	0.000	42.370
LAT CL					0.882			8.573			0.000	9.455

Base Case Model-1

DOE-2.2-48r

5/01/2016

20:26:47

BDL RUN

3

REPORT- LS-E Space Monthly Load Components EII Core Spec (T.C25)

WEATHER FILE- Toronto ON CWEC

(UNITS=MBTU)	WALLS	ROOFS	INT SUR.	UND SUR.	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL
HEATING	0.000	-0.244	0.000	0.000	-0.124	-6.837	0.474	0.388	0.581	1.298	0.000	-4.464
JAN SEN CL	0.000	-0.212	0.000	0.000	-0.105	-5.672	1.386	28.339	8.931	6.401	0.000	39.069
LAT CL					0.000			23.172		0.000	0.000	23.172
HEATING	0.000	-0.196	0.000	0.000	-0.098	-5.389	0.499	0.438	0.541	1.158	0.000	-3.048
FEB SEN CL	0.000	-0.214	0.000	0.000	-0.107	-5.965	2.106	28.289	8.922	6.409	0.000	39.440
LAT CL					0.000			23.172		0.000	0.000	23.172
HEATING	0.000	-0.143	0.000	0.000	-0.072	-4.081	0.466	0.304	0.459	1.029	0.000	-2.038
MAR SEN CL	0.000	-0.230	0.000	0.000	-0.113	-6.200	3.633	34.456	10.945	8.004	0.000	50.495
LAT CL					0.000			28.050		0.000	0.000	28.050
HEATING	0.000	-0.084	0.000	0.000	-0.041	-2.339	0.335	0.156	0.269	0.617	0.000	-1.087
APR SEN CL	0.000	-0.182	0.000	0.000	-0.086	-4.641	5.109	33.106	10.648	8.033	0.000	51.988
LAT CL					0.001			26.831		0.000	0.000	26.831
HEATING	0.000	-0.051	0.000	0.000	-0.024	-1.416	0.226	0.075	0.180	0.433	0.000	-0.578
MAY SEN CL	0.000	-0.137	0.000	0.000	-0.054	-3.008	7.013	30.177	9.813	7.604	0.000	51.408
LAT CL					0.004			24.391		0.000	0.000	24.395
HEATING	0.000	-0.024	0.000	0.000	-0.011	-0.696	0.139	0.023	0.092	0.235	0.000	-0.242
JUN SEN CL	0.000	-0.068	0.000	0.000	-0.017	-1.065	7.537	33.225	10.821	8.417	0.000	58.850
LAT CL					0.030			26.831		0.000	0.000	26.861
HEATING	0.000	-0.007	0.000	0.000	-0.003	-0.206	0.047	0.020	0.029	0.063	0.000	-0.056
JUL SEN CL	0.000	-0.040	0.000	0.000	0.000	-0.304	7.786	31.744	10.435	8.300	0.000	57.921
LAT CL					0.058			25.611		0.000	0.000	25.669
HEATING	0.000	-0.011	0.000	0.000	-0.004	-0.330	0.067	0.014	0.040	0.096	0.000	-0.129
AUG SEN CL	0.000	-0.059	0.000	0.000	-0.006	-0.769	6.590	33.234	10.891	8.604	0.000	58.485
LAT CL					0.051			26.831		0.000	0.000	26.882
HEATING	0.000	-0.026	0.000	0.000	-0.013	-0.760	0.109	0.046	0.100	0.235	0.000	-0.309
SEP SEN CL	0.000	-0.100	0.000	0.000	-0.038	-2.237	5.027	31.704	10.344	8.085	0.000	52.786
LAT CL					0.019			25.611		0.000	0.000	25.630
HEATING	0.000	-0.079	0.000	0.000	-0.039	-2.269	0.243	0.127	0.251	0.587	0.000	-1.178
OCT SEN CL	0.000	-0.150	0.000	0.000	-0.069	-3.928	3.046	30.125	9.740	7.446	0.000	46.212
LAT CL					0.005			24.391		0.000	0.000	24.396
HEATING	0.000	-0.133	0.000	0.000	-0.066	-3.687	0.360	0.194	0.384	0.900	0.000	-2.047
NOV SEN CL	0.000	-0.161	0.000	0.000	-0.078	-4.421	1.232	30.024	9.579	7.081	0.000	43.255
LAT CL					0.001			24.391		0.000	0.000	24.392
HEATING	0.000	-0.191	0.000	0.000	-0.097	-5.562	0.315	0.421	0.576	1.259	0.000	-3.278
DEC SEN CL	0.000	-0.204	0.000	0.000	-0.103	-5.781	1.039	31.348	9.891	7.108	0.000	43.299
LAT CL					0.000			25.611		0.000	0.000	25.611
HEATING	0.000	-1.191	0.000	0.000	-0.591	-33.573	3.280	2.206	3.503	7.910	0.000	-18.454
TOT SEN CL	0.000	-1.757	0.000	0.000	-0.777	-43.990	51.504	375.772	120.961	91.492	0.000	593.206
LAT CL					0.169			304.895		0.000	0.000	305.064

Base Case Model-1

DOE-2.2-48r

5/01/2016

20:26:47

BDL RUN

3

REPORT- LS-E Space Monthly Load Components ELL South Perim Plnm (T.S26)

WEATHER FILE- Toronto ON CWEC

(UNITS=MBTU)	WALLS	ROOFS	INT SUR.	UND SUR.	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL
HEATING JAN SEN CL -0.940 0.000 0.000 0.000 -0.519 0.000 0.000 0.000 0.000 0.000 0.000 -4.300												
HEATING JAN LAT CL 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000												
HEATING FEB SEN CL -0.832 0.000 0.000 0.000 -0.479 0.000 0.000 0.000 0.000 0.000 0.000 -3.559												
HEATING FEB LAT CL 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000												
HEATING MAR SEN CL -0.690 0.000 0.000 0.000 -0.438 0.000 0.000 0.000 0.000 0.000 0.000 -3.041												
HEATING MAR LAT CL 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000												
HEATING APR SEN CL -0.426 -0.001 0.000 0.000 -0.293 0.000 0.000 0.000 0.000 0.000 0.000 -1.928												
HEATING APR LAT CL 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000												
HEATING MAY SEN CL -0.198 0.032 0.000 0.000 -0.160 0.000 0.000 0.000 0.000 0.000 0.000 -0.908												
HEATING MAY LAT CL 0.127 0.249 0.000 0.000 -0.050 0.000 0.000 0.000 0.000 0.000 0.000 0.045												
HEATING JUN SEN CL -0.052 0.127 0.000 0.000 -0.103 0.000 0.000 0.000 0.000 0.000 0.000 0.001												
HEATING JUN LAT CL 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000												
HEATING JUL SEN CL -0.013 0.424 0.041 0.000 0.000 -0.015 0.000 0.000 0.000 0.000 0.000 0.069												
HEATING JUL LAT CL 0.494 0.000 0.000 0.000 0.019 0.000 0.000 0.000 0.000 0.000 0.000 0.755												
HEATING AUG SEN CL -0.007 0.264 0.035 0.000 0.000 -0.020 0.000 0.000 0.000 0.000 0.000 0.128												
HEATING AUG LAT CL 0.440 0.000 0.000 0.000 0.005 0.000 0.000 0.000 0.000 0.000 0.000 0.000												
HEATING SEP SEN CL -0.037 0.105 0.037 0.000 0.000 -0.103 0.000 0.000 0.000 0.000 0.000 0.229												
HEATING SEP LAT CL 0.088 0.000 0.000 -0.010 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.378												
HEATING OCT SEN CL -0.287 0.001 0.081 0.000 0.000 -0.242 0.000 0.000 0.000 0.000 0.000 0.620												
HEATING OCT LAT CL 0.001 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000												
HEATING NOV SEN CL -0.575 0.000 1.580 0.000 0.000 -0.329 0.000 0.000 0.000 0.000 0.000 0.485												
HEATING NOV LAT CL 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000												
HEATING DEC SEN CL -0.888 0.000 2.267 0.000 0.000 -0.467 0.000 0.000 0.000 0.000 0.000 3.621												
HEATING DEC LAT CL 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000												
HEATING TOT SEN CL -4.946 0.763 -13.958 1.302 0.000 0.000 -3.115 0.000 0.000 0.000 0.000 0.000 -22.019												
HEATING TOT LAT CL 0.000 0.329 0.000 0.000 0.007 0.000 0.000 0.000 0.000 0.000 0.000 0.329												

Base Case Model-1

DOE-2.2-48r

5/01/2016

20:26:47

BDL RUN

3

REPORT- LS-E Space Monthly Load Components EII East Perim Plm (T.E27)

WEATHER FILE- Toronto ON CWEC

(UNITS=MBTU)	WALLS	ROOFS	INT SUR	UND SUR	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL
HEATING JAN SEN CL 0.000	-1.632	0.000	0.000	-0.346	0.000	0.000	0.000	0.000	0.000	0.000	-2.717	
HEATING FEB SEN CL 0.000	-1.428	0.000	0.000	-0.319	0.000	0.000	0.000	0.000	0.000	0.000	-2.385	
HEATING MAR SEN CL 0.000	-1.214	0.000	0.000	-0.292	0.000	0.000	0.000	0.000	0.000	0.000	-2.017	
HEATING APR SEN CL 0.001	-0.768	0.000	0.000	-0.195	0.000	0.000	0.000	0.000	0.000	0.000	-1.250	
HEATING MAY SEN CL 0.027	-0.346	0.000	0.000	-0.106	0.000	0.000	0.000	0.000	0.000	0.000	-0.534	
HEATING JUN SEN CL 0.125	-0.078	0.000	0.000	-0.033	0.000	0.000	0.000	0.000	0.000	0.000	-0.121	
HEATING JUL SEN CL 0.220	-0.023	0.000	0.000	-0.011	0.000	0.000	0.000	0.000	0.000	0.000	0.043	
HEATING AUG SEN CL 0.192	-0.019	0.000	0.000	-0.013	0.000	0.000	0.000	0.000	0.000	0.000	-0.038	
HEATING SEP SEN CL 0.052	-0.214	0.000	0.000	-0.070	0.000	0.000	0.000	0.000	0.000	0.000	-0.544	
HEATING OCT SEN CL 0.001	-0.687	0.000	0.000	-0.161	0.000	0.000	0.000	0.000	0.000	0.000	-0.86	
HEATING NOV SEN CL 0.000	-1.003	0.000	0.000	-0.219	0.000	0.000	0.000	0.000	0.000	0.000	-1.674	
HEATING DEC SEN CL 0.000	-1.439	0.000	0.000	-0.311	0.000	0.000	0.000	0.000	0.000	0.000	-2.411	
HEATING TOT SEN CL 0.617	-3.710	-8.852	0.000	-2.077	0.000	0.000	0.000	0.000	0.000	0.000	-14.639	
	LAT CL	0.816	0.000	0.005	0.000	0.222	0.000	0.000	0.000	0.000	0.000	1.439
	LAT CL											0.222

Base Case Model-1

DOE-2.2-48r

5/01/2016

20:26:47

BDL RUN

3

REPORT- LS-E Space Monthly Load Components ELL North Perim Plnm (T.N28)

WEATHER FILE- Toronto ON CWEC

(UNITS=MBTU)	WALLS	ROOFS	INT SUR.	UND SUR.	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL
JAN SEN CL	-1.171 0.000	-2.571 0.000	0.000 0.000	0.000 0.000	-0.519 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-4.260
JAN LAT CL												0.000 0.000
FEB SEN CL	-1.031 0.000	-2.248 0.000	0.000 0.000	0.000 0.000	-0.479 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-3.758
FEB LAT CL												0.000 0.000
MAR SEN CL	-0.907 0.000	-1.912 0.000	0.000 0.000	0.000 0.000	-0.438 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-3.257
MAR LAT CL												0.000 0.000
APR SEN CL	-0.596 0.000	-1.210 0.000	0.000 0.000	0.000 0.000	-0.293 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-2.099
APR LAT CL												0.000 0.000
MAY SEN CL	-0.294 -0.002	-0.544 0.248	0.000 0.000	0.000 0.000	-0.165 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-1.004
MAY LAT CL												0.000 0.000
JUN SEN CL	-0.072 0.069	-0.125 0.247	0.000 0.000	0.000 0.000	-0.053 0.005	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.249
JUN LAT CL												0.000 0.000
JUL SEN CL	-0.020 0.152	-0.040 0.493	0.000 0.000	0.000 0.000	-0.017 0.020	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.076
JUL LAT CL												0.000 0.000
AUG SEN CL	-0.030 0.110	-0.032 0.437	0.000 0.000	0.000 0.000	-0.023 0.008	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.085
AUG LAT CL												0.000 0.000
SEP SEN CL	-0.199 0.016	-0.336 0.087	0.000 0.000	0.000 0.000	-0.110 -0.002	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.645
SEP LAT CL												0.000 0.000
OCT SEN CL	-0.514 0.000	-1.082 0.000	0.000 0.000	0.000 0.000	-0.242 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-1.838
OCT LAT CL												0.000 0.000
NOV SEN CL	-0.721 0.000	-1.580 0.000	0.000 0.000	0.000 0.000	-0.329 0.100	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-2.630
NOV LAT CL												0.000 0.000
DEC SEN CL	-1.027 0.000	-2.267 0.000	0.000 0.000	0.000 0.000	-0.467 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-3.761
DEC LAT CL												0.000 0.000
TOT SEN CL	-6.580 0.345	-13.947 1.291	0.000 0.000	0.000 0.000	-3.135 0.026	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-23.62
TOT LAT CL												0.319

Base Case Model-1

DOE-2.2-48r

5/01/2016

20:26:47

BDL RUN

3

REPORT- LS-E Space Monthly Load Components EII West Perim Plm (T.W29)

WEATHER FILE- Toronto ON CWEC

(UNITS=MBTU)	WALLS	ROOFS	INT SUR	UND SUR	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL
JAN SEN CL	-0.742 0.000	-1.632 0.000	0.000 0.000	0.000 0.000	-0.346 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-2.721
JAN LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
FEB SEN CL	-0.647 0.000	-1.428 0.000	0.000 0.000	0.000 0.000	-0.319 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-2.394
FEB LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
MAR SEN CL	-0.554 0.000	-1.214 0.000	0.000 0.000	0.000 0.000	-0.292 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-2.600
MAR LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
APR SEN CL	-0.335 0.000	-0.768 0.000	0.000 0.000	0.000 0.000	-0.195 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-1.299
APR LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
MAY SEN CL	-0.152 0.012	-0.348 0.020	0.000 0.000	0.000 0.000	-0.107 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.026	-0.608
MAY LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001
JUN SEN CL	-0.031 0.092	-0.082 0.160	0.000 0.000	0.000 0.000	-0.032 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.145
JUN LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.041
JUL SEN CL	-0.006 0.167	-0.026 0.314	0.000 0.000	0.000 0.000	-0.009 0.012	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.493	-0.042
JUL LAT CL					0.086							0.086
AUG SEN CL	-0.004 0.156	-0.023 0.280	0.000 0.000	0.000 0.000	-0.012 0.003	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.039
AUG LAT CL					0.077							0.077
SEP SEN CL	-0.084 0.040	-0.217 0.059	0.000 0.000	0.000 0.000	-0.070 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-0.370
SEP LAT CL					0.012							0.012
OCT SEN CL	-0.291 0.000	-0.687 0.000	0.000 0.000	0.000 0.000	-0.161 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-1.140
OCT LAT CL					0.000							0.000
NOV SEN CL	-0.457 0.000	-1.003 0.000	0.000 0.000	0.000 0.000	-0.219 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-1.680
NOV LAT CL					0.100							0.077
DEC SEN CL	-0.668 0.000	-1.439 0.000	0.000 0.000	0.000 0.000	-0.311 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-2.419
DEC LAT CL					0.000							0.218
TOT SEN CL	-3.973 0.467	-8.868 0.832	0.000 0.000	0.000 0.000	-2.075 0.003	0.000 0.218	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	-14.916 1.303 0.218

Base Case Model-1

REPORT- LS-E Space Monthly Load Components Ell Core Plnm (T.C30)

DOE-2.2-48r

5/01/2016

20:26:47

BDL RUN

3

WEATHER FILE- Toronto ON CWEC

(UNITS=MBTU)	WALLS	ROOFS	INT SUR	UND SUR	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL
HEATING	0.000	-13.307	0.000	0.000	-0.229	0.000	0.000	0.000	0.000	0.000	0.000	-13.356
JAN SEN CL	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
LAT CL												
HEATING	0.000	-11.640	0.000	0.000	-0.205	0.000	0.000	0.000	0.000	0.000	0.000	-11.845
FEB SEN CL	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
LAT CL												
HEATING	0.000	-9.901	0.000	0.000	-0.185	0.000	0.000	0.000	0.000	0.000	0.000	-10.086
MAR SEN CL	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
LAT CL												
HEATING	0.000	-6.265	0.000	0.000	-0.126	0.000	0.000	0.000	0.000	0.000	0.000	-6.391
APR SEN CL	0.000	0.001	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001
LAT CL												
HEATING	0.000	-2.851	0.000	0.000	-0.071	0.000	0.000	0.000	0.000	0.000	0.000	-2.923
MAY SEN CL	0.000	0.176	0.000	0.000	-0.07	0.000	0.000	0.000	0.000	0.000	0.000	0.170
LAT CL												
HEATING	0.000	-0.684	0.000	0.000	-0.020	0.000	0.000	0.000	0.000	0.000	0.000	-0.704
JUN SEN CL	0.000	1.317	0.000	0.000	-0.008	0.000	0.000	0.000	0.000	0.000	0.000	1.309
LAT CL					0.022	0.000	0.000	0.000	0.000	0.000	0.000	0.022
HEATING	0.000	-0.223	0.000	0.000	-0.005	0.000	0.000	0.000	0.000	0.000	0.000	-0.228
JUL SEN CL	0.000	2.569	0.000	0.000	0.003	0.000	0.000	0.000	0.000	0.000	0.000	2.572
LAT CL					0.054	0.000	0.000	0.000	0.000	0.000	0.000	0.054
HEATING	0.000	-0.196	0.000	0.000	-0.007	0.000	0.000	0.000	0.000	0.000	0.000	-0.203
AUG SEN CL	0.000	2.293	0.000	0.000	-0.004	0.000	0.000	0.000	0.000	0.000	0.000	2.289
LAT CL					0.050	0.000	0.000	0.000	0.000	0.000	0.000	0.050
HEATING	0.000	-1.773	0.000	0.000	-0.046	0.000	0.000	0.000	0.000	0.000	0.000	-1.819
SEP SEN CL	0.000	0.483	0.000	0.000	-0.005	0.000	0.000	0.000	0.000	0.000	0.000	0.478
LAT CL					0.009	0.000	0.000	0.000	0.000	0.000	0.000	0.009
HEATING	0.000	-5.602	0.000	0.000	-0.108	0.000	0.000	0.000	0.000	0.000	0.000	-5.710
OCT SEN CL	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
HEATING	0.000	-8.181	0.000	0.000	-0.144	0.000	0.000	0.000	0.000	0.000	0.000	-8.325
NOV SEN CL	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
LAT CL					0.100	0.000	0.000	0.000	0.000	0.000	0.000	0.000
HEATING	0.000	-11.736	0.000	0.000	-0.200	0.000	0.000	0.000	0.000	0.000	0.000	-11.936
DEC SEN CL	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
LAT CL					0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
HEATING	0.000	-72.359	0.000	0.000	-1.346	0.000	0.000	0.000	0.000	0.000	0.000	-73.706
TOT SEN CL	0.000	6.839	0.000	0.000	-0.021	0.000	0.000	0.000	0.000	0.000	0.000	6.818
LAT CL					0.136	0.000	0.000	0.000	0.000	0.000	0.000	0.136

Base Case Model-1

REPORT- IS-F Building Monthly Load Component

DOE-2.2-48r

5/01/2016

20:26:47

BDL RUN

3

WEATHER FILE- Toronto ON CWEC

(UNITS=MBTU)	WALLS	ROOFS	INT SUR.	UND SUR.	INFIL	WIN CON	WIN SOL	OCCUP	LIGHTS	EQUIP	SOURCE	TOTAL
HEATING	-14.424	-0.244	0.000	-4.858	-13.982	-86.745	16.710	7.140	8.289	7.313	0.000	-80.802
JAN SEN CL	-2.204	-0.212	0.000	-2.965	-4.005	-19.476	21.385	92.209	31.006	25.492	0.000	141.230
LAT CL				0.000				75.129		0.000	0.000	75.129
HEATING	-12.188	-0.196	0.000	-4.485	-12.404	-74.888	17.932	7.149	7.414	6.817	0.000	-64.850
FEB SEN CL	-2.397	-0.214	0.000	-3.346	-4.169	-21.218	25.827	92.236	30.553	25.428	0.000	142.701
LAT CL				0.000				75.186		0.000	0.000	75.186
HEATING	-9.257	-0.143	0.000	-4.441	-9.799	-60.623	18.285	5.733	6.004	6.021	0.000	-48.221
MAR SEN CL	-3.076	-0.230	0.000	-4.303	-5.357	-26.766	38.534	114.125	37.361	32.432	0.000	182.721
LAT CL				0.000				93.246		0.000	0.000	93.246
HEATING	-4.714	-0.084	0.000	-3.047	-5.280	-34.976	13.075	2.694	3.180	3.556	0.000	-25.595
APR SEN CL	-2.833	-0.182	0.000	-5.026	-4.874	-25.574	49.715	112.375	37.138	33.309	0.000	194.046
LAT CL				0.064				91.512		0.000	0.000	91.512
HEATING	-1.867	-0.051	0.000	-1.631	-2.744	-19.431	8.847	1.119	1.608	2.200	0.000	-11.951
MAY SEN CL	-1.142	-0.137	0.000	-5.095	-3.157	-19.197	65.447	103.051	32.989	32.099	0.000	205.188
LAT CL				0.246						0.000	0.000	84.297
HEATING	-0.367	-0.024	0.000	-0.456	-0.942	-7.204	3.620	0.267	0.526	0.919	0.000	-3.160
JUN SEN CL	1.584	-0.068	0.000	-4.488	-0.748	-9.397	70.367	114.334	36.642	35.908	0.000	244.133
LAT CL				2.758				92.740		0.000	0.000	95.498
HEATING	-0.058	-0.007	0.000	-0.115	-0.343	-2.642	1.180	0.226	0.327	0.466	0.000	-0.966
JUL SEN CL	3.555	-0.040	0.000	-3.589	0.453	-2.953	69.536	109.985	36.611	35.210	0.000	248.768
LAT CL				4.787				88.538		0.000	0.000	93.325
HEATING	-0.93	-0.011	0.000	-0.125	-0.528	-4.020	1.789	0.220	0.383	0.633	0.000	-1.752
AUG SEN CL	3.295	-0.059	0.000	-2.688	0.017	-5.759	65.427	114.515	36.701	36.411	0.000	247.860
LAT CL				4.110				92.736		0.000	0.000	96.846
HEATING	-1.018	-0.026	0.000	-0.389	-1.584	-11.067	4.324	0.688	1.124	1.469	0.000	-6.479
SEP SEN CL	0.326	-0.100	0.000	-2.255	1.430	-14.923	58.731	109.130	37.004	33.988	0.000	219.940
LAT CL				1.430				88.429		0.000	0.000	89.860
HEATING	-4.109	-0.079	0.000	-1.142	-4.366	-30.519	9.727	1.999	2.908	3.090	0.000	-22.491
OCT SEN CL	-2.219	-0.150	0.000	-2.307	-4.019	-21.344	41.786	103.074	36.041	31.190	0.000	182.054
LAT CL				0.327				83.611		0.000	0.000	83.938
HEATING	-7.742	-0.133	0.000	-2.247	-7.246	-48.045	9.065	3.767	6.022	4.665	0.000	-41.894
NOV SEN CL	-2.505	-0.161	0.000	-2.408	-4.161	-20.036	18.523	100.380	37.157	29.306	0.000	156.094
LAT CL				0.058				82.329		0.000	0.000	82.387
HEATING	-12.627	-0.191	0.000	-3.683	-12.281	-74.779	11.010	7.481	9.266	7.310	0.000	-68.493
DEC SEN CL	-2.431	-0.204	0.000	-2.695	-3.887	-19.591	16.460	102.740	35.622	28.384	0.000	154.399
LAT CL				0.001				83.480		0.000	0.000	83.481
HEATING	-68.464	-1.191	0.000	-26.623	-71.498	-454.936	115.565	38.484	47.050	44.455	0.000	-377.158
TOT SEN CL	-10.047	-1.757	0.000	-41.164	-36.215	-206.836	541.734	126.045	424.821	379.188	0.000	2318.769
LAT CL				13.781				103.954		0.000	0.000	1044.736

SPACE ELL East Perim Spc (G.E2)

REPORT SCHEDULE HOURS WITH SUN UP												
MONTH	TOTAL ZONE	PERCENT LIGHTING ENERGY REDUCTION BY DAYLIGHTING (ALL HOURS)		PERCENT LIGHTING ENERGY REDUCTION BY DAYLIGHTING (REPORT SCHEDULE HOURS)		AVERAGE DAYLIGHT ILLUMINANCE (FOOTCANDLES)		PERCENT HOURS DAYLIGHT ILLUMINANCE ABOVE SETPOINT		AVERAGE GLARE INDEX		
		REF	PT	REF	PT	REF	PT	REF	PT	REF	PT	
		1	2	1	2	1	2	1	2	1	2	
JAN	44.2	44.2	0.0	44.2	44.2	0.0	60.8	0.0	44.0	0.0	12.6	0.0
FEB	47.2	47.2	0.0	47.2	47.2	0.0	87.7	0.0	51.6	0.0	14.9	0.0
MAR	58.8	58.8	0.0	58.8	58.8	0.0	116.2	0.0	56.6	0.0	14.9	0.0
APR	65.1	65.1	0.0	65.1	65.1	0.0	126.3	0.0	61.3	0.0	15.7	0.0
MAY	78.3	78.3	0.0	78.3	78.3	0.0	157.9	0.0	69.1	0.0	16.8	0.0
JUN	79.7	79.7	0.0	79.7	79.7	0.0	152.4	0.0	69.4	0.0	17.7	0.0
JUL	75.0	75.0	0.0	75.0	75.0	0.0	142.9	0.0	68.7	0.0	17.4	0.0
AUG	81.2	81.2	0.0	81.2	81.2	0.0	137.4	0.0	69.9	0.0	17.6	0.0
SEP	66.6	66.6	0.0	66.6	66.6	0.0	131.8	0.0	63.7	0.0	16.6	0.0
OCT	53.7	53.7	0.0	53.7	53.7	0.0	95.2	0.0	54.8	0.0	14.9	0.0
NOV	31.4	31.4	0.0	31.4	31.4	0.0	52.9	0.0	36.7	0.0	12.1	0.0
DEC	35.7	35.7	0.0	35.7	35.7	0.0	48.2	0.0	33.5	0.0	10.7	0.0
ANNUAL	60.2	60.2	0.0	60.2	60.2	0.0	115.3	0.0	58.6	0.0	15.5	0.0

SPACE ELL West Perim Spc (G.W4)

REPORT SCHEDULE HOURS WITH SUN UP												
MONTH	PERCENT LIGHTING ENERGY REDUCTION BY DAYLIGHTING (ALL HOURS)			PERCENT LIGHTING ENERGY REDUCTION BY DAYLIGHTING (REPORT SCHEDULE HOURS)			AVERAGE DAYLIGHT ILLUMINANCE (FOOTCANDLES)			PERCENT HOURS DAYLIGHT ILLUMINANCE ABOVE SETPOINT		
	TOTAL	REF	PT	TOTAL	REF	PT	REF	PT	PT	REF	PT	PT
	ZONE	1	2	ZONE	1	2	1	2	1	2	1	2
JAN	42.8	42.8	0.0	42.8	42.8	0.0	64.3	0.0	42.8	0.0	12.2	0.0
FEB	47.5	47.5	0.0	47.5	47.5	0.0	94.4	0.0	53.2	0.0	14.9	0.0
MAR	55.7	55.7	0.0	55.7	55.7	0.0	99.3	0.0	56.4	0.0	14.6	0.0
APR	62.2	62.2	0.0	62.2	62.2	0.0	119.2	0.0	61.7	0.0	15.7	0.0
MAY	74.2	74.2	0.0	74.2	74.2	0.0	130.7	0.0	66.2	0.0	16.3	0.0
JUN	76.1	76.1	0.0	76.1	76.1	0.0	143.3	0.0	67.9	0.0	17.6	0.0
JUL	68.0	68.0	0.0	68.0	68.0	0.0	132.7	0.0	64.8	0.0	17.2	0.0
AUG	75.1	75.1	0.0	75.1	75.1	0.0	128.7	0.0	69.9	0.0	17.5	0.0
SEP	61.8	61.8	0.0	61.8	61.8	0.0	118.8	0.0	62.9	0.0	16.3	0.0
OCT	53.6	53.6	0.0	53.6	53.6	0.0	98.4	0.0	55.9	0.0	14.8	0.0
NOV	28.9	28.9	0.0	28.9	28.9	0.0	57.6	0.0	36.1	0.0	12.0	0.0
DEC	35.3	35.3	0.0	35.3	35.3	0.0	48.9	0.0	33.5	0.0	10.4	0.0
ANNUAL	57.2	57.2	0.0	57.2	57.2	0.0	107.9	0.0	57.8	0.0	15.3	0.0

SPACE EL1 South Perim Spc (M.S11)

REPORT SCHEDULE HOURS WITH SUN UP													
MONTH	TOTAL ZONE	PERCENT LIGHTING ENERGY REDUCTION BY DAYLIGHTING (ALL HOURS)			PERCENT LIGHTING ENERGY REDUCTION BY DAYLIGHTING (REPORT SCHEDULE HOURS)			AVERAGE DAYLIGHT ILLUMINANCE (FOOTCANDLES)			PERCENT HOURS DAYLIGHT ILLUMINANCE ABOVE SETPOINT		
		TOTAL	REF	PT	TOTAL	REF	PT	REF	PT	PT	REF	PT	PT
		ZONE	1	2	ZONE	1	2	1	2	1	1	2	
JAN	52.3	52.3	0.0	52.3	52.3	0.0	160.4	0.0	51.7	0.0	14.5	0.0	
FEB	53.7	53.7	0.0	53.7	53.7	0.0	178.0	0.0	59.7	0.0	16.6	0.0	
MAR	60.0	60.0	0.0	60.0	60.0	0.0	164.4	0.0	60.1	0.0	15.8	0.0	
APR	65.2	65.2	0.0	65.2	65.2	0.0	152.6	0.0	63.6	0.0	16.4	0.0	
MAY	77.1	77.1	0.0	77.1	77.1	0.0	144.2	0.0	66.4	0.0	16.7	0.0	
JUN	78.0	78.0	0.0	78.0	78.0	0.0	134.1	0.0	66.7	0.0	17.2	0.0	
JUL	73.4	73.4	0.0	73.4	73.4	0.0	128.7	0.0	65.8	0.0	17.1	0.0	
AUG	78.8	78.8	0.0	78.8	78.8	0.0	148.9	0.0	70.2	0.0	17.8	0.0	
SEP	68.0	68.0	0.0	68.0	68.0	0.0	183.1	0.0	66.4	0.0	17.7	0.0	
OCT	58.8	58.8	0.0	58.8	58.8	0.0	171.1	0.0	61.8	0.0	16.3	0.0	
NOV	35.5	35.5	0.0	35.5	35.5	0.0	115.4	0.0	42.3	0.0	13.4	0.0	
DEC	42.0	42.0	0.0	42.0	42.0	0.0	132.3	0.0	41.6	0.0	12.3	0.0	
ANNUAL	62.2	62.2	0.0	62.2	62.2	0.0	150.6	0.0	61.0	0.0	16.2	0.0	

SPACE ELL East Perim Spc (M.E12)

REPORT SCHEDULE HOURS WITH SUN UP											
MONTH	TOTAL ZONE	PERCENT LIGHTING ENERGY REDUCTION BY DAYLIGHTING (ALL HOURS)		PERCENT LIGHTING ENERGY REDUCTION BY DAYLIGHTING (REPORT SCHEDULE HOURS)		AVERAGE DAYLIGHT ILLUMINANCE (FOOTCANDLES)		PERCENT HOURS DAYLIGHT ILLUMINANCE ABOVE SETPOINT		AVERAGE GLARE INDEX	
		REF	PT	REF	PT	REF	PT	REF	PT	REF	PT
		1	2	1	2	1	2	1	2	1	2
JAN	46.3	46.3	0.0	46.3	46.3	0.0	64.9	0.0	45.8	0.0	12.2
FEB	48.0	48.0	0.0	48.0	48.0	0.0	93.6	0.0	52.6	0.0	14.7
MAR	60.2	60.2	0.0	60.2	60.2	0.0	124.0	0.0	58.1	0.0	14.7
APR	66.6	66.6	0.0	66.6	66.6	0.0	134.8	0.0	62.4	0.0	15.5
MAY	78.5	78.5	0.0	78.5	78.5	0.0	168.4	0.0	69.7	0.0	16.6
JUN	80.4	80.4	0.0	80.4	80.4	0.0	162.4	0.0	70.2	0.0	17.5
JUL	75.7	75.7	0.0	75.7	75.7	0.0	152.1	0.0	69.3	0.0	17.2
AUG	81.7	81.7	0.0	81.7	81.7	0.0	146.3	0.0	71.5	0.0	17.4
SEP	69.5	69.5	0.0	69.5	69.5	0.0	140.5	0.0	65.9	0.0	16.3
OCT	54.5	54.5	0.0	54.5	54.5	0.0	101.5	0.0	55.6	0.0	14.6
NOV	33.4	33.4	0.0	33.4	33.4	0.0	56.5	0.0	38.7	0.0	11.9
DEC	37.2	37.2	0.0	37.2	37.2	0.0	51.4	0.0	35.5	0.0	10.3
ANNUAL	61.5	61.5	0.0	61.5	61.5	0.0	122.9	0.0	59.9	0.0	15.2

References

ASHRAE, “ASHRAE Handbook-Fundamentals”, American Society of Heating, Refrigeration and Air-conditioning Engineering (ASHRAE), Atlanta, USA, 2005.

ASHRAE, “ANSI/ASHRAE/IESNA Standard 90.1, Energy Standard for Buildings Except Low-rise Residential Buildings” American Society of Heating, Refrigeration and Air Conditioning Engineers (ASHRAE), 2013.

ASHRAE, “Variable Refrigerant Flow Systems” ASHRAE Journal, April 2011.

ASHRAE, “ANSI/ASHRAE Standard 62.1-2007, Ventilation for Acceptable Indoor Air Quality” American Society of Heating, Refrigeration and Air Conditioning Engineers (ASHRAE), 2007.

City of Toronto, “Greenhouse Gases and Air Pollutants in the City of Toronto”, 2007.

Charneux, R., “Office Retrofit”, ASHRAE Journal, November 2010.

Clark, J., “Energy Simulation in Building Design”, Second Edition, Butterworth Heinemann, UK, 2001.

CEA Technologies Inc, “Heat Pump Energy Efficiency Reference Guide”.

Climate Master, “Tranquility 30 Digital Series” Climate Master Water-source Heat Pumps, 2014.

Chwieduk, D., “Solar Energy in Building Thermal Balance for Efficient Heating and Cooling”, Elsevier Publication, 2014.

Duncan, P., “How High Can You Go?” ASHRAE Journal, September 2009.

Environment and Climate Change Canada, “GHG Emissions Quantification Guidance”,

Government of Canada, 2011.

Gordon, V., Holness, R., “Sustaining Our Future by Rebuilding Our Past”, ASHRAE Journal, August 2009.

Hirsch, J., “eQuest Introductory Tutorial”, James J. Hirsch & Associates, 2009.

Hootman, T., “Net Zero Energy Design – a guide for Commercial Architecture”, Jon Wiley & Sons, 2013.

Lian, X., “Optimized Control Strategies for a Typical Water Loop Heat Pump System”, University of Nebraska-Lincoln, July 2011.

Liu, L., Qu, S., Ge, X., “Testing and Analysis of Thermal Performance for Water Source Heat Pump Systems”, University of Science and Technology Beijing, 2011.

Lussier, G., “Heat Recovery for Canadian Building”, ASHRAE Journal, December 2014.

McQuiston, Faye, C., “Heating, Ventilation and Air Conditioning Design & Analysis” John Wiley & Sons Inc. 1982.

McQuay Daikin International “McQuay Effinity Horizontal and Vertical Water Source Heat Pumps – $\frac{1}{2}$ to 5 tons”.

McQuay Inc., “Water-source heat pump design manual”, 1999.

McKeen, P., Fung, A., “The Effect of Building Aspect Ratio on Energy Efficiency: A Case Study for Multi-Unit Residential Building in Canada”, Ryerson University, July 2014.

Nall, D., Crawley, D., “Energy Simulation in the Building Design Process”. ASHRAE Journal, July 2011.

NRCAN, “Survey of Commercial and Institutional Energy Use-Buildings 2009”. Natural Resource Canada, 2012.

NRCAN, “Energy Efficiency-Buildings”, Natural Resource Canada, 2014. Available online at <http://www.nrcan.gc.ca/energy/efficiency/buildings/4261>

NRCAN, “Energy Efficiency Trends in Canada, 1990 to 2009”, Office of Energy Efficiency, Ottawa, February 2011.

NRCAN, “Internal Water-loop Heat Pumps-Commercial”, Office of Energy Efficiency, January 2016.

Shapiro, I., “Energy Audits in Large Commercial Office Buildings”, ASHRAE Journal, January 2009.

Southard, L., Liu, X., Spitzer, J., “Performance of HVAC Systems at ASHRAE HQ” ASHRAE Journal, September 2014.

Schneider Electric, “Leading Techniques for Energy Savings in Commercial Office Buildings” Schneider Electric, 2006.

Trane Inc., “Axiom Vertical/Horizontal: ½ to 6 ton Water Source Heat Pumps”, Trane Inc., 2013.

Rao, G., Sauer, H., “Energy Conservation Using the Closed Water Loop Heat Pump”, Missouri Academy of Science, 2002.

Zheng, G., Jing, Y., “Thermodynamic Performance Analysis of Water Source Heat Pump in Variant Operating Condition”, North China Electric Power University, 2009.