WIND ENERGY FORECASTS IN CALCULATION OF EXPECTED ENERGY NOT SERVED

By

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Wind Energy Forecasts In Calculation of Expected Energy Not Served Master of Applied Science 2014 Richard Sun Electrical and Computer Engineering Ryerson University

ABSTRACT

The stochastic nature of wind energy generation introduces uncertainties and risk in generation schedules computed using optimal power flow (OPF). This risk is quantified as expected energy not served (EENS) and computed via an error distribution found for each hourly forecast. This thesis produces an accurate method of estimating EENS that is also suitable for real-time OPF calculation.

This thesis examines two statistical predictive models used to forecast hourly production of wind energy generators (WEGs), Markov chain model, and auto-regressive moving-average (ARMA) model, and their effects on EENS. Persistence model is used as a benchmark for comparison. For persistence and ARMA models, both Gaussian and Cauchy error distributions are used to compute EENS via a closed-form solution that reduces computational complexity..

Markov chain and ARMA both provide accurate forecasts of WEG power generation though Markov Chain model performs significantly better. The Markov chain model also produces the most accurate EENS estimate of the three models.

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List of Symbols

General Terminology

 \hat{X}_t : a time series of the forecasted wind energy generation.

 X_i : a time series of the actual wind energy generation.

 PG_t : A random variable that describes WEG generation at time t.

n: the number of elements within the training data.

m: the number of elements within the validation data.

 $PG_{nominal}$: nominal wind power. For this case it is the maximum wind power a generator is capable of outputting.

 $\overline{\overline{PG_t}}$: the forecasted power generation of a WEG at time t.

 β : the PDF scale parameter in the general case.

PG_{sched}: the power generation scheduled for a given point of time.

 Δt : the time interval used between forecasts. For this case it is one hour.

Markov Chain Model Terminology N: the number of states used in the Markov chain model

 S_i : the i^{th} state of a Markov chain

 P_i : the amount of power generation that corresponds to the i^{th} state of a Markov chain

 $\mathbf{P}(t_h)$: the first-order Markov chain transition matrix

 $\hat{P}(t_h)$: the estimate of the first-order Markov chain transition matrix

 $p_{ij}(t_h)$: the generic element of $\mathbf{P}(t_h)$

 $p_i(t_h)$: the generic column of $\mathbf{P}(t_h)$

 $p_j(t_h)$: the generic row of $\mathbf{P}(t_h)$

<u>ARMA Model Terminology</u> ARMA(p,q): an ARMA process with orders p and q *p*: the order of the auto-regressive part of an ARMA process

q: the order of the moving-average part of an ARMA process

a_j: the coefficients of the auto-regressive part of an ARMA process

 b_k : the coefficients of the moving-average part of an ARMA process

List of Abbreviations

WEG: Wind Energy Generator OPF: Optimal Power Flow AENS: Actual Energy Not Served EENS: Expected Energy Not Served PDF: Probability Distribution Function ARMA: Autoregressive-moving average ANN: Artificial Neural Network NRMSE: Normalized Root-Mean-Square

1. INTRODUCTION

1.1. Introduction

When wind energy generators (WEGs) are incorporated into the power supply mix, the uncertainties associated with wind energy increases the risk of power shortages and failure to supply a contracted load. This risk is also carried into determining optimal power flow (OPF) and is quantified by expected energy not served (EENS). EENS is an estimate of actual energy not served (AENS) which is the actual energy shortfall of a WEG at a given point in time. At any given time, a certain amount of power generation is scheduled from every WEG which is denoted here as PG_{sched} . EENS is the expected energy shortfall from the scheduled power. This shortfall is probabilistic because of the stochastic nature of wind energy and the uncertainties of the wind energy forecast.

Having an accurate forecast of WEG output and being able to calculate EENS in a timely fashion is very important for estimating the costs associated with uncertainties from WEGs as they become a larger part of the power grid.

1.2. Survey of Recent Work in WEG Forecasting and EENS

In the past, Monte Carlo simulation has been used to stochastically model WEG integration to the grid and to estimate the costs associated with the uncertainty introduced by the WEGs as in [1]. Ref. [2] uses Monte Carlo simulation in conjunction with OPF to maximize social welfare as it pertains to uncertainties in WEG generation. Ref. [3] uses Monte Carlo simulation to stochastically model locational marginal prices (LMP) and examine the effect that

the introduction of WEG has on LMP. Monte Carlo simulation however, can be very taxing computationally, especially in systems with large numbers of WEGs as it scales exponentially with the number of buses in the system. Alternative ways of quantifying EENS have been developed for OPF as a result. Ref. [4] introduces a triangular-approximation for modeling WEG for OPF. Approximating the probability distribution of WEG generation effectively linearizes it, making it readily usable with OPF and does not require time-consuming Monte Carlo simulation. Thus, the method introduced in [4] is suitable for real-time OPF applications where the methods using Monte Carlo simulation are not. One shortcoming of this method however is that it uses an estimate of the WEG forecast's PDF and thus the accuracy of EENS estimation will suffer.

1.3. Objective

The main motivation of this thesis is to develop a methodology to estimate EENS from a predictive model that is suitable for real-time OPF. The relative accuracy of two statistical-only predictive models, autoregressive-moving-average (ARMA), and Markov chain as well as their effect on EENS calculations will also be examined. The effects of using Gaussian error distributions and Cauchy distributions to calculate EENS will also be analyzed.

This thesis will develop a way of estimating EENS using closed-form or pseudo-closedform equations for EENS calculations. This will produce a more accurate estimate of EENS than in [4] because it dispenses with the approximation and will also be suited for real-time OPF applications.

1.4. Chapter-wise Introduction

Chapter 2:

Chapter 2 discusses the background of WEG forecasting and introduces the two models that are to be studied, Markov chain and ARMA as well as persistence model which is to be used as a benchmark. Background and calculation of EENS is discussed in the general case. For each model, the forecasting mechanism is explored in detail as well as the method by which a PDF is derived for EENS calculation. Finally, calculation of EENS is discussed for each model.

Chapter 3:

Chapter 3 presents the simulation results for each model. The accuracy of the forecast produced by each model is evaluated. The EENS estimated by each model is also examined and evaluated. Three case studies are considered: Amaranth wind farm, Wolfe Island wind farm, and ERCOT system-wide.

Chapter 4:

Chapter 4 presents the conclusions that can be drawn from this work. Recommendations for which model and PDF should be used for EENS estimation are given based on the results presented in chapter 3. The main contributions and relevance of this work are also discussed.

1.5. Chapter Summary

This chapter presents an introduction to the topic, motivation and objective of this thesis. It is followed by a chapter-wise summary.

2. THEORY

EENS is calculated from a probability distribution of the error in the forecasted WEG output. Thus, in order to determine EENS, two things are required: a forecast for wind energy output, and an error distribution of the forecast. The forecast for wind energy output at time *t* is denoted by \hat{X}_t . X_t is the actual wind energy generation of the next time step at time *t* and is used to determine the accuracy of the forecast. This thesis will explore three different predictive models for forecasting WEG output as well as methods of deriving a probability distribution of the error so that EENS can be calculated.

There are two main categories of predictive models for wind power generation: physical and statistical. Physical models consider physical variables such as wind speed, temperature, atmospheric conditions, etc. Statistical models do not consider any physical variables and instead use time-series analysis of historical wind power generation data. Statistical models have the advantage of being computationally simpler as well as being easier to implement than physical models.

Two predictive models will be explored, Markov chain, and ARMA. Markov chain and ARMA model were chosen for their accuracy on shorter time horizons as well as the advantages afforded by the fact that they are purely statistical models[5][6]. The Markov chain model in particular produces a very accurate probability density function for the forecasting error which is very useful in calculating EENS[6]. These two models will be used to generate forecasts for WEG outputs on the one-hour-ahead timescale. A third model, persistence model, will also be used as a benchmark for the first two. ARMA and Markov chain models have been compared

and evaluated in the past for their forecasting ability but their respective effects on EENS have not [7].

An artificial neural network (ANN) is another statistical-only model that as become an increasingly popular method of forecasting WEG generation. ANNs are models that are so-named because they attempt to mimic the structure and functionality of animal brains. Adaptive weights are used to conceptualize the relative strengths of the connections within the network. They are trained by a training data set and used in prediction.

ANNs can be generally classified as feed-forward or feedback [8]. Feed-forward ANNs are more common in WEG forecasting and include backpropagation and radial bases function [9]. Backpropagation refers to the error of the ANN which is backpropagated through the network so that the weights can be updated in order to minimize future errors [10].

ANNs are capable of producing a point-forecast and associated probability distribution that is suitable for EENS estimation but will not be discussed in detail within this work. However, the method of estimating EENS from a forecasting model established in this work can be used with ANNs as well as other statistical models.

The next step in calculating EENS is to generate a probability distribution for these forecasts. In the case of the Markov chain model, a probability distribution will be created by the model itself for each forecast. In the case of persistence and ARMA, the probability distribution is modeled by a Gaussian or a Cauchy distribution. The scale parameters for each distribution will be determined by historical data.

There are several statistical distributions that can be used to model the error distribution of wind power generation point forecasts. As discussed previously, the forecast must be able to generate a probability distribution for a given time in order for EENS to be calculated. [11] provides a method for calculating EENS using a Weibull distribution for wind speed. Gaussian and Cauchy distributions will be utilized in this thesis and they will be fitted to WEG output generation as opposed to wind speed. For shorter time-steps, on the order of 1 hour, a Cauchy distribution will often provide a better fit than Gaussian distribution. This is a result of the excess kurtosis exhibited by the observed error distribution of wind energy forecasts. The observed error distributions have higher peaks and shorter tails than the fitted Gaussian has and are closer in appearance to Cauchy distributions. In many instances however, the central-limit theorem can be invoked to justify the use of a Gaussian distribution.

2.1. EENS Overview

The EENS of the WEG is the amount of energy that is expected to be less than the scheduled generation PG_{sched} based on the probability distribution of the forecast error. In the general case, EENS can be calculated from:

$$EENS = \int_{0}^{PG_{sched}} (PG_{sched} - PG) \cdot PDF(\overline{PG}, \beta) dPG$$
(2.3.1)

 $PDF(\overline{PG}, \beta)$ in equation (2.3.1) above differs depending on the PDF being used. The Gaussian and Cauchy distributions each have a location parameter and a scale parameter which are denoted in the general case by \overline{PG} and β , respectively. In both Gaussian and Cauchy distributions the location parameter is \overline{PG} . The scale parameter for the Gaussian distribution is σ^2 and the scale parameter for the Cauchy distribution is γ . The location parameter \overline{PG} is the point

forecast produced by the forecasting model. The scale parameters are produced by the forecasting model using the training data. These two parameters are required for EENS to be calculated. The specifics of determining the location and scale parameters and calculating EENS from it in the case of Gaussian and Cauchy distributions will be described in detail in section 2.2.3, and 2.2.4, respectively.

In the case of the Markov chain model, the model produces a discrete PDF which is immediately suitable for EENS calculation. The specifics of producing the PDF in the this case and calculating EENS from it will be described in detail in sections 2.3.3, and 2.3.4, respectively.



Figure 2.1.1: Diagram of the EENS calculator

Figure 2.1.1 shows a visual representation of the method outlined in this section. The "EENS Calculation" box represents equation 2.3.1. It can be seen from figure 2.1.1 that EENS is a function of \overline{PG} and β both of which are produced by the forecasting model.

2.2. Persistence Model (Used as a benchmark)

2.2.1. Theoretical Background

The persistence model assumes that the wind generation at the next hour is equal to the generation at the current hour. The forecasted generation at the next time step can be given by [12]:

$$\hat{X}_{t} = X_{t-1} \tag{2.2.1.1}$$

For very short time-steps (on the order of minutes) persistence provides a very accurate forecast and is in fact difficult to improve upon. For short time-steps (on the order of an hour) it still provides an adequate forecast. This is because there is high correlation between wind speeds[3], that is, wind speed does not change much from hour to hour and even less so from minute to minute.

Because persistence is very simple and easy to implement, it is often used as a benchmark to compare with other forecasting models. Other forecasting models must be able to outperform persistence to be viable.

2.2.2. Methodology

As seen in equation (2.2.1.1), the forecasted generation \hat{X}_t at time *t* is given by the actual generation of the previous time step, X_{t-1} . The probability density function (PDF) of the forecasting error gives the probability distribution of forecasted power generation \hat{X}_t at the next time step.

2.2.3. Probability Density Function

As noted previously, a probability distribution of a given point forecast's error (error PDF) is required for EENS calculation. In the case of the persistence and ARMA model, the error PDF is assumed to be either a Gaussian distribution or a Cauchy distribution.

Two parameters must be determined to construct the error PDF: a location parameter, and a scale parameter. The location parameter is the forecast at the current time step in both cases. The scale parameter is σ^2 for the Gaussian distribution and γ is the scale parameter for the Cauchy distribution. EENS is a calculated as a function of this location parameter, and scale parameter.

Gaussian: For a Gaussian distribution, the PDF is given by:

$$PDF_G(PG_t) = \frac{1}{\sqrt{2\pi\sigma^2}} \exp\left(\frac{-(PG_t - \overline{PG_t})}{2\sigma^2}\right)$$
(2.2.3.1)

 PG_t ranges from 0 to $PG_{nominal}$. $\overline{PG_t}$ is the forecasted generation of the current time step. It is the mean of the Gaussian distribution and the location parameter of the Cauchy distribution. Thus, it is given by:

$$PG_t = \hat{X}_t \tag{2.2.3.2}$$

 \hat{X}_t can be found from equation (2.2.1.1).

 σ^2 is the scale parameter of the Gaussian distribution and also the variance of the difference between the forecasted generation and the actual generation at each time step during the training data period. σ^2 is given by:

$$\sigma^2 \frac{1}{n} \sum_{t=1}^n \left(Y_t - \hat{\hat{Y}_t} \right)^2$$
(2.2.3.3)

Where *n* is the number of elements in the training data, Y_t is a time series of training data and \hat{Y}_t is a time series of the prediction of the training data.

Cauchy: In the case of a Cauchy distribution, the PDF is given by:

$$PDF_{C}(PG_{t}) = \frac{1}{\pi \gamma \left[1 + \left(\frac{PG_{t} - \overline{PG_{t}}}{\gamma}\right)^{2}\right]}$$
(2.2.3.4)

 γ is selected to be half of the interquartile range of the Gaussian distribution and is thus given by:

$$\gamma = 0.6745\sigma$$
 (2.2.3.5)

With the location parameter $\overline{PG_t}$, and the scale parameters σ^2 and γ for Gaussian and Cauchy respectively, EENS can be calculated.



Figure 2.2.3.1: Forecasting Error Probability Density Function

Figure 1 shows the actual error distribution determined from a persistence model over the training data period. A Gaussian and Cauchy distribution based on a forecast of $\overline{PG_t}$ at 100MW is overlayed on it. A bin size is chosen such that the number of bins is larger than the minimum prescribed by Scott's normal reference rule. The data comes from 3960 hours of wind generation data from the Amaranth wind farm.

2.2.4. Calculating EENS

As discussed previously, in the case of persistence and ARMA models, Gaussian and Cauchy distributions are used to fit the probability density functions of the forecast and to calculate EENS.

Gaussian: A solution for EENS calculated with a Gaussian distribution at a given PG_{sched} is derived below:

$$EENS_{G} = \frac{1}{\sqrt{2\pi\sigma^{2}}} \int_{0}^{PG_{sched}} \left(PG_{sched} - \overline{PG} \right) e^{-\frac{(PG - \overline{PG})^{2}}{2\sigma^{2}}} dPG$$

$$EENS_{G} = \frac{PG_{sched}}{\sqrt{2\pi\sigma^{2}}} \int_{0}^{PG_{sched}} e^{-\frac{(PG - \overline{PG})^{2}}{2\sigma^{2}}} dPG -$$

$$\frac{1}{\sqrt{2\pi\sigma^{2}}} \int_{0}^{PG_{sched}} PG \cdot e^{-\frac{(PG - \overline{PG})^{2}}{2\sigma^{2}}} dPG$$
(2.2.4.1)

Solving equation (2.2.4.1):

$$\frac{PG_{sched}}{2} \left[1 + erf \frac{\left(PG - \overline{PG}\right)}{2\sigma^2} \right]$$
(2.2.4.3)

Where

$$erf(x) = \frac{2}{\sqrt{\pi}} \int_0^x e^{-t} dx$$

Solving equation (2.2.4.2) with integration by parts:

let
$$a = \frac{1}{2\sigma^2}$$
, and $c = \frac{1}{\sqrt{2\pi\sigma^2}}$
 $u = ce^{-a\overline{PG^2}}e^{-aPG^2}$, $du = 2ac\overline{PG}e^{-a\overline{PG^2}}$
 $dv = xe^{-aPG^2}$, $v = -\frac{1}{2a}e^{-aPG^2}$
 $(2.2.4.2) = uv - \int v \cdot dv$
 $(2.2.4.2) = -ce^{-a\left(PG_{sched} - \overline{PG}\right)^2} - \overline{PG}\int_0^{PG_{sched}}e^{-aPG^2}e^{2a\overline{PGPG}}e^{-a\overline{PG^2}}dPG$
 $(2.2.4.2) = -ce^{-a\left(PG_{sched} - \overline{PG}\right)^2} + a\overline{PG}\left[1 + erf\left(aPG_{sched} - \overline{PG}\right)\right]$ (2.2.4.4)
Thus, EENS is given by:

$$EENS_{G} = \frac{1}{\sqrt{2\pi\sigma^{2}}} \frac{e^{-\left(PG_{sched}} - \overline{PG}\right)^{2}}{2\sigma^{2}} + \left(\frac{PG_{sched}}{2} - \frac{\overline{PG}}{2\sigma^{2}}\right)$$
$$erf\left(\frac{PG_{sched}}{2} - \overline{\overline{PG}}}{2}\sigma^{2}\right) + \frac{PG_{sched}}{2} - \frac{\overline{\overline{PG}}}{2}\sigma^{2} \qquad (2.2.4.5)$$

Here, \overline{PG} , and σ^2 are given by equations (2.2.3.2), and (2.2.3.3), respectively.

A closed-form solution does not exist for the Gaussian because of the presence of the error function in the formulation as seen in equation (2.2.1.1). However, a number of closedform approximations of the error function exist and a suitable one can be utilized. Numerical methods and look-up tables are also available.

Cauchy: A solution for EENS calculated with a Cauchy distribution at a given PGsched is derived below:

$$EENS_{C} = \int_{0}^{PG_{sched}} \left(PG_{sched} - PG\right) \frac{1}{\pi \gamma \left[1 + \frac{PG - \overline{PG}}{\gamma}\right]} dPG$$

$$EENS_{C} = \frac{PG_{sched}}{\pi \gamma} \int_{0}^{PG_{sched}} \frac{1}{1 + \frac{PG - \overline{PG}}{\gamma}} dPG - (2.2.4.6)$$

$$\frac{1}{\sqrt{2\pi\sigma^2}} \int_0^{PG_{sched}} \frac{PG}{1 + \frac{PG - \overline{PG}}{\gamma}} dPG$$
(2.2.4.7)

Solving equation (2.2.4.6):

$$(2.2.4.6) = PG_{sched}\left[\frac{1}{\pi}\tan^{-1}\left(\frac{PG-\overline{PG}}{\gamma}\right) + \frac{1}{2}\right]$$
(2.2.4.8)

Solving equation (2.2.4.7) with integration by parts:

Finding the integration constant *C*. At $PG_{sched} = 0$, EENS = 0. $0 = -\frac{\overline{PG}}{\pi} \tan^{-1} \left(-\frac{\overline{PG}}{\gamma} \right) - \ln \left| \overline{PG^2} + \gamma^2 \right| - C$ $C = -\frac{\overline{PG}}{\pi} \tan^{-1} \left(-\frac{\overline{PG}}{\gamma} \right) - \ln \left| \overline{PG^2} + \gamma^2 \right|$

Thus, EENS is given by:

$$E_{C} = \frac{PG_{sched} - \overline{PG}}{\pi} \tan^{-1} \left(PG_{sched} - \overline{PG} \right) - \frac{\gamma}{2\pi} \ln \left| \left(\frac{PG_{sched} - \overline{PG}}{\gamma} \right)^{2} \right| + \frac{PG_{sched}}{2} + \frac{\overline{PG}}{\pi} \tan^{-1} \left(\frac{-\overline{PG}}{\gamma} \right) + \ln \left| \overline{PG^{2}} \right| + \gamma^{2}$$

$$(2.2.4.10)$$

Here, \overline{PG} , is again given by equation (2.2.3.2). γ is given by equation (2.2.3.5). It should be noted that EENS is a closed-form equation when using the Cauchy distribution. Equations (2.2.4.5) and (2.2.4.10) form two of the major contributions of this work. The closed form solutions (pseudo-closed form in the case of Gaussian) for EENS provide an accurate and easily calculable estimate for EENS that did not previously exist.

2.3. Markov Chain Model

2.3.1. Theoretical Background

A Markov chain is a stochastic process with the Markov property on a finite or countable state space, that is, if the conditional probability distribution of future states depends only on the current state. Thus, future states of a Markov chain do not depend on past states.

The state variable for power generation is divided into N bins, equally spaced intervals from 0 to $PG_{nominal}$ of length $PG_{nominal}$ /N. These states are defined as [5]:

$$S = \{S_1, S_2 \dots S_N\}$$
(2.3.1.1)

Every state *Si* corresponds to an amount of power generation which is defined as:

$$S_{i} = \left(\frac{i \cdot PG_{no\min al}}{N}\right) + \frac{PG_{no\min al}}{2N}$$
(2.3.1.2)

The parameter *N* gives the size of the bins and is selected to accommodate the tradeoffs between precision and noise from sampling randomness. The $PG_{nominal}/2N$ term results from the fact that each state S_i is chosen to be the middle of the bin.

Changes from time *t* to t+1 are defined by a one-step transition probabilities matrix **P**. **P** is a symmetrical *N*x*N* matrix.



Figure 2.3.1.1: Example of a transition matrix created by a Markov chain model with N = 20

Figure 2.3.1.1 shows the highest probability clusters are centred around N = 0, and N = 20. This agrees with the assumption made previously that the WEG is most often operating at 0MW or at full power (*PG_{nominal}*). The above figure also shows that most transitions are centred around a diagonal from (0,0) to (N,N) which agrees with the assumption that WEG generation does not change very much hour to hour and the most probable transition is generally to the same state.

The estimate of the transition probabilities matrix **P** is determined based on the historical data and denoted as \hat{P} . The columns of \hat{P} correspond to the current state of the process and the rows correspond to the state at the next time step. The generic element of \hat{P} is defined as $p_{ij}(t)$ and the generic row of \hat{P} is defined as $P_i(t)$ at time *t*. Each element of the transition matrix \hat{P} corresponds to a possible state of the process. Figure 3 shows an example of a transition matrix \hat{P} with 20 states.

An estimate for $p_{ij}(t)$ is given in [5] and shown below:

$$\hat{p}_{ij} = \frac{n_{ij}(t)}{\sum_{j} n_{ij}(t)} \forall i, j, \sum_{j=1}^{N} \hat{p}_{ij}(t) = 1 \forall i$$
(2.3.1.3)

nij is the number of transitions from state S_i to state S_j observed in the training data series. Thus, P_i at time *t* can be defined as:

$$P_i(t) = \left\{ \hat{p}_{i1}(t), \, \hat{p}_{i2}(t) \dots \hat{p}_{iN}(t) \right\}$$
(2.3.1.4)



Figure 2.3.1.2: Sample two state Markov chain model

Figure 2.3.1.2 shows a simple Markov chain with two states. The numbers indicate the probability that the given state transition will occur. Note that they add up to 1 for each state. It can also be observed that a Markov chain with one state is equivalent to the persistence model as seen from equation (2.1.1.1) since every state transition is from the current state to itself.

Given that the generation at time *t* corresponds to state S_i , each element of row $P_i(t)$ of the estimated transition matrix \hat{P} gives the probability of the state of the next time step. Thus, $P_i(t)$ is a discrete probability distribution of the WEG output at the next time step. A point forecast can be obtained by using the state with the highest probability given by the previous time step. At time *t*, the largest element of $P_i(t)$ gives the most probable state at the next time step which is defined as $S_{max}(t)$.

$$S_{\max}(t) = M_{ij} \hat{P}_{ij}(t-1)$$
(2.3.1.5)

In the case where multiple states are equally likely, $S_{max}(t)$ is the average of those states. $S_{max}(t)$ corresponds to the forecasted WEG generation at time \hat{X}_t which is expressed in MW. Thus, \hat{X}_t is given by:

$$\hat{X}_{t} = N \cdot S_{\max}(t) + \frac{PG_{no\min al}}{2N}$$
 (2.3.1.6)

2.3.2. Methodology

Equation (2.3.1.3) is applied to all elements of the transition matrix \hat{P} . The result can be visualized by Figure 3. The point forecast of time *t* is given by equation (2.3.1.6).

2.3.3. Probability Density Function

As discussed previously, the Markov chain model differs from the persistence model in that the forecasted generation PG is given not as a point forecast but rather as a probability distribution. Therefore, in the case of the Markov chain model, the probability density function of the forecast does not need to be fit to a Gaussian nor a Cauchy distribution.

Given the state is S_i at time *t*-1, The vector $P_i(t)$ of the estimated transition matrix \hat{P} can immediately be used in EENS calculation. The PDF is thus given by:

$$PDF_{M}(PG_{t}) = P_{i}(t-1)$$
(2.3.3.1)

2.3.4. Calculating EENS

The probability distribution given in the Markov chain forecast is the probability density function of the forecast error used to calculate EENS. This is a discrete probability density function and at time *t* when the current generation is in state S_i , is given by $P_i(t)$. equation (2.1.1) can be reformulated as:

$$EENS_M = \sum_{k=1}^{PG_{sched}} p_{ik}(t) \cdot \left(PG_{sched} - PG\right) \cdot \frac{P_{no\min al}}{N}$$
(2.3.4.1)

2.4. ARMA Model 2.4.1. Theoretical Background

An autoregressive-moving-average (ARMA) model is a tool used for the analysis of time series composed of two polynomials and is used for modeling and predicting future values of both deterministic and stochastic processes. It is assumed that WEG generation exhibits short memory since WEG generation tends not to change very much over short time scales.

An ARMA model is composed of two parts: an auto-regressive (AR) part, and a movingaverage (MA) part. An ARMA(p,q) process is defined as an ARMA model where the AR portion has an order of p and the MA portion has an order of q. The model is characterized as such [6]:

$$\hat{X}_{t} = \sum_{j=1}^{p} a_{j} X_{t-j} + \sum_{k=0}^{q} b_{k} e_{t-k}$$
(2.4.1.1)

The first term in equation (2.4.1.1) represents the auto-regressive component and the second term represents the moving average component. It shows that \hat{X}_t is a linear combination of *p* past observations at time *t* (auto-regressive part) and a white-noise process with a mean of zero and a constant variance (moving-average part).

The simplest ARMA(p,q) process is one where *p* is 1 and *q* is 0. Similarly to the Markov chain model, this reduces to the persistence model in equation (2.2.1.1) since the model only uses the WEG generation of the previous time step.



Figure 2.4.1.1: Flowchart depicting the process of determining

 \hat{X}_{t} is an ARMA(*p*,*q*) process where p, and q are the orders of the auto-regressive part and moving average parts respectively. Two tasks remain: the first is to select the orders p, and q of the model and the second is to select the coefficients *a_j* and *b_k*. Matlab's System Identification toolbox has tools that can be used for both tasks.

2.4.2. Model Order

The Akaike information criterion (AIC) is a tool used for model selection. It evaluates statistical models used for a given data set relative to each other. It compares the trade-off between the goodness of the fit and the number of parameters used in the model. One caveat of its use however is that because it only provides a relative measure, it is unable to tell if none of the models compared are good fits. AIC is given below[13].

$$AIC = 2k - 2\ln(L) \tag{2.4.2.1}$$

Here, k is the number of parameters in the statistical model and L is the maximized value of the likelihood function of the estimated model which is assumed to be Gaussian and is given by equation (2.1.3.1). $\ln(L)$ is the log-likelihood of the likelihood function L and is given by:

$$\ln(L) = \ln\left(\frac{1}{\sqrt{2\pi\sigma_2}}\right) - \left(\frac{\overline{PG} - PG}{2\sigma_2}\right)$$
(2.4.2.2)

 \overline{PG} Is given by equation (2.2.3.2), and σ^2 is given by equation (2.2.3.3).

The preferred model is the one with the lowest AIC. The first term in equation (2.4.2.1) penalizes a model for over-fitting and the second term rewards the goodness of the fit.

AICc is a modification on AIC that corrects for finite sample sizes. It is given below[14].

$$AICc = AIC + \frac{2k(k+1)}{n-k-1}$$
(2.4.2.3)

AICc is similar to AIC but carries a greater penalty for models with extra parameters. AICc will be used as the main criterion for order selection in ARMA models.

2.4.3. Coefficient Determination

A number of methods can be used for determining the p and q coefficients of an ARMA process such as Burg and Shanks, and Yule-Walker, or least-squares estimation. Least-squares estimation is used.

2.4.4. Methodology

The first step is to determine the model order. An ARMA(p,q) process is created with the training data as the input for each p, $q = \{1, 2, ..., 10\}$. Matlab's internal least-squares estimation method is used in determining p, and q[15].Therefore, 100 ARMA(p,q) processes will be created and AICc is calculated for each of them. The one with the lowest AICc is used to determine p and q. Figure 4 below illustrates the method of model order selection.

Once the orders of the model have been selected, equation (2.4.1.1) can be used to predict each future time-step. This can be used to either model the training data or to predict future values.
2.4.5. Probability Density Function

As noted previously, a probability distribution of a given point forecast's error is required for EENS calculation.

The method of producing a probability density function for the ARMA model forecast is the same as in persistence model and is described in section 2.2.3. The one difference in the case of ARMA model is that $\overline{PG_t}$ is given by equation (2.4.1.1). σ^2 and γ are given by equations 2.2.3.3 and 2.2.3.5 for Gaussian and Cauchy distributions, respectively. With these two sets of parameters, EENS can be calculated.

2.4.6. Calculating EENS

EENS for the ARMA model is calculated in the same manner as persistence model. Using the Gaussian distribution, EENS is given by equation 2.2.4.5 and by 2.2.4.10 when using the Cauchy distribution. Again, $\overline{PG_t}$ is given by equation (2.4.1.1).

3. RESULTS AND DISCUSSION

3.1. Data

Historical hourly power generation data for every wind generator/farm in Ontario was collected from the Independent Electricity System Operator (IESO) web-site from March 3, 2013 to October 2, 2013. In the models and calculations that follow, data from the Amaranth wind farm is used. Because WEGs often operate at maximum capacity or not at all, the nominal power generation $PG_{nominal}$ is defined as the maximum generation of the WEG.

Two sets of data are used: a training data set, and validation data set. The training data is used to construct the Markov chain and ARMA models (persistence does not require training) The validation data follows the training data immediately in time and is used to verify the accuracy of each model. The training data contains 165 days of data (3960 hours) and the validation data contains 35 days (840 hours).

Data from March 3, 2013 to August 27, 2013 is used as train-ing data and data from August 28, 2013 to October 2, 2013 is used for the validation data.

3.2. Amaranth Wind Farm

3.2.1. Comparing Forecast Error

The three models are trained on the hourly training data based on 3960 hours of the Amaranth Wind Farm's wind energy output with a nominal power output, *PGnominal*, of 200MW.

Each of the three models is used to generate a one-hour-ahead forecast for the duration of the validation data (840 hours). They are plotted against the actual wind generation of the Amaranth Wind Farm during that time period.

In the Markov chain model used, N is chosen to be 200. In the ARMA model used, p and q are chosen to be 2. Plots of each predictive model between the 200th and 300th hours of the validation data are shown below.



Figure 3.2.1.1: Persistence model wind energy generation forecast compared to actual generation for Amaranth wind farm



Figure 3.2.1.2: Markov chain model wind energy generation forecast compared to actual generation for Amaranth wind farm



Figure 3.2.1.3: ARMA model wind energy generation forecast compared to actual generation for Amaranth wind farm

Figures 5 through 7 show that all three models are capable of producing an accurate forecast for the one-hour-ahead horizon. The persistence model produces a forecast that is delayed by one hour based on the actual generation. Qualitatively, they show that Markov chain and ARMA model provide a more accurate forecast of than persistence model.

The forecasts generated by each model is evaluated quantitatively by comparing their normalized root mean square error (NRMSE) which is calculated using the difference between forecasted generation and the actual generation over the duration, m, of the validation data period. It is expressed as a percentage of nominal power output of the WEG. NRMSE is defined by:

$$NRMSE = \frac{1}{PG_{no\min al}} \sqrt{\frac{1}{m} \sum_{t=1}^{m} (X_t - \hat{X}_t)^2} \times 100\%$$
(3.2.1.1)

The size of the validation period, m, is 840 elements. The results are summarized in the table below:

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Table 3.2.1.1: NRMSE	of forecast for	each predictive	model (Amaranth)
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Model	NRMSE (% of PGnominal)
Persistence	6.3302
Markov	2.6622
ARMA	5.2277



Figure 3.2.1.4: Forecast errors of all three predictive models plotted together for Amaranth wind farm

Figure 8 shows the NRMSE of each predictive model side by side during windows of 168 hours (7 days). Both Markov chain and ARMA models performed better than the persistence model. Markov chain performed significantly better than persistence and ARMA. Markov chain should be expected to work best in cases where the training data provides an accurate assessment of the wind generation of the wind farm at all times.

3.2.2. Comparing EENS

EENS was calculated using the error distributions of persistence, Markov chain, and ARMA model forecasts on the one-hour-ahead horizon. Gaussian and Cauchy distributions were used for persistence and ARMA models and their effects on EENS compared. The distribution generated by the Markov chain model's forecast was used for EENS calculation. EENS is also compared to AENS in order to evaluate the adequacy of the calculated EENS.



Figure 3.2.2.1: EENS calculated from persistence, Markov Chain, and ARMA models for Amaranth wind farm

The plot in figure 3.2.2.1 uses a forecasted generation \overline{PG} , of 100MW. It compares EENS estimations for the three models with Gaussian and Cauchy distributions used for persistence and ARMA. The scheduled generation PG_{sched} is not necessarily known at the time of the forecast. For this reason, EENS is shown here as a function of PG_{sched} . The X-axis of the plot gives the EENS for a given PG_{sched} .

In all cases at this forecasted generation, EENS is very small when the expected generation PG_{sched} is less than 80 MW. This is explained by the fact that if the forecasted generation is at 100 MW, and PG_{sched} is much less than 100 MW, there is a high probability that the expected generation will be met. Thus, EENS will be small. As PG_{sched} increases, EENS increases as well.

Figure 3.2.2.1 shows that ARMA model using Gaussian distribution gives the smallest EENS and ARMA model using Cauchy distribution gives the greatest EENS. This difference is explained by the shorter tail of the Cauchy distribution relative to the Gaussian distribution. Markov Chain model gives the most moderate EENS estimation of the five scenarios shown in Figure 3.2.2.1.



Figure 3.2.2.2: EENS plotted with AENS for persistence model with \overline{PG} at 96MW for Amaranth Island wind farm.

Figure 3.2.2.2 shows EENS plotted with actual energy not served (AENS) for persistence model using Gaussian and Cauchy distributions with \overline{PG} at 96MW. AENS is the actual energy shortfall for a given amount of *PG*_{sched}. AENS in figure 3.2.2.2 is determined as such:

- 1. Find all instances in the training data where 96MW is forecasted by the model.
- 2. Calculate the AENS for the actual generation at that time for all possible PGsched.

3. Calculate the mean of each instance.

It can be seen from the plot in figure 3.2.2.2 that the Cauchy distribution provides a better estimate of EENS than the Gaussian distribution.



Figure 3.2.2.3: EENS plotted with AENS for Markov chain model with \overline{PG} at 96MW for Amaranth wind farm.

Figure 3.2.2.3 shows EENS plotted with AENS for Markov chain model with \overline{PG}_{at} 96MW. AENS in figure 3.2.2.3 is determined in the same way as in figure 3.2.2.2. The plot in figure 3.2.2.3 shows that Markov chain model provides a better estimate of EENS than the persistence model.



Figure 3.2.2.4: EENS plotted with AENS for ARMA model with \overline{PG}_{at} 96MW for Amaranth wind farm.

Figure 3.2.2.4 shows EENS plotted with AENS for ARMA model with \overline{PG} at 96MW. AENS in figure 3.2.2.4 is determined in the same way as in figure 3.2.2.2. The plot in figure 3.2.2.4 shows that ARMA model provides a better estimate of EENS than the persistence model however it is difficult to determine qualitatively if it provides a better estimate than the Markov chain model.

Model	NRMSE (% of PGnominal)
Persistence (Gaussian)	9.91
Persistence (Cauchy)	12.48
Markov Chain	5.23
ARMA (Gaussian)	12.41
ARMA (Cauchy)	10.70

Table 3.2.2.1: NRMSE of EENS vs. AENS for each predictive model and distribution (Amaranth)

Table 3.2.2.1 gives the NRMSE (as defined in section 3.2.1) between EENS and AENS for each model and distribution with PGsched. It can be seen that the Markov chain model provides the best estimate of the five scenarios but ARMA model using the Cauchy distribution also outperforms persistence model. In both persistence and ARMA models, Cauchy outperforms Gaussian.

3.3. Wolfe Island Wind Farm

3.3.1. Comparing Forecast Error

The three models are trained on the hourly training data based on 4800 hours of the Wolfe Island Wind Farm's wind energy output with a nominal power output, *PG_{nominal}*, of 197 MW.

Each of the three models is used to generate a one-hour-ahead forecast for the duration of the validation data (840 hours). They are plotted against the actual wind generation of the Wolfe Island Wind Farm during that time period.

In the Markov chain model used, N is chosen to be 200. In the ARMA model used, p and q are chosen to be 2. Plots of each predictive model between the 200th and 300th hours of the validation data are shown below.



Figure 3.3.1.1: Persistence model wind energy generation forecast compared to actual generation for Wolfe Island wind farm



Figure 3.3.1.2: Persistence model wind energy generation forecast compared to actual generation for Wolfe Island wind farm



Figure 3.3.1.3: Persistence model wind energy generation forecast compared to actual generation for Wolfe Island wind farm

Figures 10 through 12 show qualitatively that the three models provide good estimates of WEG generation for the Wolfe Island wind farm.

As in table 3.2.1.1, table 3.3.1.1 shows the NRMSE of each model and its predictive accuracy using the data from the Wolfe Island wind farm. The sample size, m, is 840. The results are similar to the results from the Amaranth wind farm. The accuracy of each model is slightly worse in the case of Wolfe Island.

Table 3.3.1.1: NRMSE of forecast for each predictive model (Wolfe Island)

Model	NRMSE (% of <i>PGnominal</i>)
Persistence	6.4271
Markov	2.8568
ARMA	6.2634





As in figure 3.2.1.4, figure 3.3.1.4 shows the NRMSE of each predictive model side by side during windows of 168 hours (7 days). Again, both Markov chain and ARMA models performed better than the persistence model and Markov chain performed the best of the three.

Forecasting Errors (Wolfe Island)

3.3.2. Comparing EENS



Figure 3.3.2.1: EENS calculated from persistence, Markov Chain, and ARMA models for Wolfe Island wind farm

The plot in figure 14 use a forecasted generation, \overline{PG} , of 100 MW. It compares EENS estimations for the three models with Gaussian and Cauchy distributions used for persistence and ARMA. The results are similar to those in figure 9. For Wolfe Island, the ARMA and persistence EENS is much closer than that of Amaranth. The Markov chain EENS is vertically shifted upward compared to the Amaranth case because a \overline{PG} of 93 MW is used for Markov chain as a

result of the discrete nature of the Markov chain model. In all cases, the EENS is slightly higher than the Amaranth case because of the accuracy of each forecast in the Wolfe Island case is slightly worse.



Figure 3.3.2.2: EENS plotted with AENS for persistence model with \overline{PG} at 90MW for Wolfe Island wind farm.

Figure 3.3.2.2 shows EENS plotted with AENS for persistence model for \overline{PG} at 90MW. AENS is determined in the same way as in figure 3.2.2.2



Figure 3.3.2.3: EENS plotted with AENS for Markov chain model with \overline{PG} at 90MW for Wolfe Island wind farm

Figure 3.3.2.3 shows EENS plotted with AENS for persistence model for \overline{PG} at 90MW. AENS is determined in the same way as in figure 3.2.2.2. A comparison between figure 3.3.2.2 and 3.3.2.3 shows qualitatively that Markov chain model again provides a more accurate EENS estimate than persistence model.



Figure 3.3.2.4: EENS plotted with AENS for ARMA model with \overline{PG} at 90MW for Wolfe Island wind farm.

Figure 3.3.2.4 shows EENS plotted with AENS for ARMA model with \overline{PG} at 90MW. AENS in figure 3.3.2.4 is determined in the same way as in figure 3.2.2.2. The plot in figure 3.3.2.4 shows that Cauchy distribution provides a better EENS estimate than Gaussian distribution for ARMA model.

Model	NRMSE (% of <i>PGnominal</i>)
Persistence (Gaussian)	6.15
Persistence (Cauchy)	9.98
Markov Chain	1.34
ARMA (Gaussian)	4.58
ARMA (Cauchy)	4.46

Table 3.3.2.1: NRMSE of EENS vs. AENS for each predictive model and distribution (Amaranth)

Table 3.3.2.1 gives the NRMSE (as defined in section 3.2.1) between EENS and AENS for each model and distribution with PG_{sched} ranging between 60MW and 140MW. It can be seen that the Markov chain model again provides the best estimate of the five scenarios and ARMA also provides a more accurate estimate than persistence model. As with Amaranth wind farm, Cauchy distribution outperforms Gaussian for both persistence and ARMA models.

3.4. ERCOT System-wide

3.4.1.Comparing Forecast Error

The three models are trained on the hourly training data based on 240 hours of ERCOT's (Electric Reliability Council of Texas) system-wide wind energy output with a nominal power output, *PG_{nominal}*, of 12212 MW.

Each of the three models is used to generate a one-hour-ahead forecast for the duration of the validation data (48 hours). They are plotted against the actual wind generation of the Wolfe Island Wind Farm during that time period.

In the Markov chain model used, N is chosen to be 100. In the ARMA model used, p and q are chosen to be 2, and 1 respectively. Plots of each predictive model using the validation data are shown below.



Figure 3.4.1.1: Persistence model wind energy generation forecast compared to actual generation for ERCOT system-wide



Figure 3.4.1.2: Markov chain model wind energy generation forecast compared to actual generation for ERCOT system-wide



Figure 3.4.1.3: ARMA model wind energy generation forecast compared to actual generation for ERCOT system-wide

As in table 3.2.1.1, table 3.4.1.1 shows the NRMSE of each model and its predictive accuracy using the data from ERCOT system-wide. The sample size, m, is 48.

Model	NRMSE
Persistence	5.0167
Markov	3.961
ARMA	3.7641

Table 3.4.1.1: NRMSE of forecast for each predictive model



Figure 3.4.1.4: Forecast errors of all three predictive models plotted together for ERCOT system-wide

As in figure 3.2.1.4, figure 3.4.1.4 shows the NRMSE of each predictive model side by side during windows of 6 hours. Unlike figure 3.2.1.4, and figure 3.3.1.4 however, it is not immediately clear which model performs best. Table 3.4.1.1 shows numerically however that Markov chain and ARMA outperform persistence and ARMA performs best overall.

3.4.2. Comparing EENS



Figure 3.4.2.1: EENS calculated from persistence, Markov Chain, and ARMA models for ERCOT system-wide

The plot in figure 14 use a forecasted generation, \overline{PG} , of 6000 MW. It compares EENS estimations for the three models with Gaussian and Cauchy distributions used for persistence and ARMA. In this scenario, The persistence and ARMA models using Gaussian distributions have lower EENS estimates than with Cauchy distributions for smaller values of *PG*. The Gaussian

distribution exhibits greater slope in the linear portion starting around 6500 MW and the intersection point is near 7600 MW. The Markov chain model exhibits smaller EENS estimates compared to the other two models for values of PG smaller than 6700 MW, and higher EENS estimates for higher values of PG. It should be noted that the Markov chain plot exhibits a staircase pattern because the number of bins, N, is small relative to the nominal output power.

No comparisons between AENS and EENS are generated for the ERCOT system-wide case study because the training data is not sufficiently large for accurate results and conclusions to be drawn from it.

3.4.3. Comparison with Previous Work

The previously referenced paper [11] studied the use of ARMA models on Texas' ERCOT wind energy generators. In that paper, accuracy of the model was defined as "the number of forecasts made by the model that carry an error less than a preset value, expressed as a percentage of the total number of forecasts made. For example, if 100 hour-ahead forecasts are made with the number of counts of the error less than 25% being equal to 90; the accuracy of the forecast is said to 90% in the 25% error limit. [11]" This definition was used for persistence, Markov chain, and ARMA models to evaluate their performance relative to the results shown in [11].

January	April	July	October				
83.888	82.491	73.032	82.253				

Table 3.4.3.1: Accuracy with 25% error limit for one hour ahead forecast in [11].

Table 3.4.3.2: Accuracy with 25% error limit for one hour ahead forecast in for persistence, Markov chain, and ARMA models.

Model	Accuracy
Persistence	99.792
Markov chain	95.833
ARMA	99.792

The results in table 3.4.3.1 and table 3.4.3.2 show that the three models examined here provided good estimates of WEG generation for the ERCOT system. There are however, a few caveats about the results shown in table 3.4.3.2. The size of the training data and the validation data used is significantly smaller than was used in [11]. Also, the data used for table 3.4.3.1 is from 2006 while the data used for table 3.4.3.2 is from 2014. The ERCOT grid has changed significantly since then and the total WEG capacity has increased since then.

4. CONCLUSIONS

The ability to accurately forecast wind energy generator power generation as well as the expected energy not served of a wind energy generator is very important in quantifying the risks associated with wind energy. Expected energy not served calculation requires an error distribution for the forecasted wind energy generator power generation. To this end, various predictive models can be used to produce this error distribution. Although much work has been done on evaluating and comparing predictive models for wind energy generator power forecasting, their effects on expected energy not served has been thus far unexplored.

In this thesis, Markov chain model, and ARMA models are used to produce a point forecast for the one-hour-ahead horizon as well as an error distribution that could be used for expected energy not served calculation considering a wind farm data from Ontario, Canada. These two models were compared to persistence model which was used to establish a benchmark.

Of the two predictive models examined, Markov chain model provided the better forecast, defined here as least normalized root-mean-square error. Both Markov chain and ARMA models outperformed persistence model and produce an accurate forecast. As evidenced by tables 3.2.2.1, and 3.3.2.1, Markov chain also provides the best estimation of expected energy not served as compared to actual energy not served, again as defined as least normalized root-mean-square error. Again, Markov chain and ARMA models both outperform persistence model. Markov chain model in particular gives a very accurate error distribution which is useful in producing accurate expected energy not served calculations.

Two other case studies were examined. The first involved data from Ontario's Wolfe Island wind farm. The results from that were similar to those of the Amaranth wind farm though slightly less accurate. As a result, the estimated expected energy not served skewed higher. The second involved data from Texas' ERCOT system. These results were also compared to the results from [11] which used older data from the ERCOT system. In most cases, Markov chain model is recommended in order to produce the best expected energy not served estimate based on the case studies examined. It should be noted however, that the most suitable model can differ depending on the specific application or location. This thesis provides a methodology by which the best model for estimating expected energy not served can be determined for any given situation or models.

A closed-form solution was found for expected energy not served when using a Cauchy distribution. A solution for expected energy not served was also found when using a Gaussian distribution. It is not fully closed-form because of the presence of the error function within the solution but look-up tables can be used for efficient calculation. Both solutions aid in reducing the computational complexity of calculating expected energy not served which is important in solving for OPF.

5. APPENDIX

5.1. Simulation Data

5.1.1. Amaranth Wind Farm Raw Data

5.1.1.1. Training Data

The data below is the hourly training data from Amaranth wind farm used to create the Markov chain and ARMA models. It is

used to generate the plots and tables section 3.2.

	Hour																						
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24
16	23	12	10	8	8	9	12	12	8	6	1	0	0	2	4	13	10	5	2	11	30	33	61
67	41	40	30	22	28	27	24	7	17	33	17	4	1	1	0	0	2	2	3	9	4	5	19
34	54	78	118	124	135	155	155	165	169	175	181	183	182	181	182	182	179	181	168	146	128	93	79
64	75	116	111	91	61	59	80	119	108	117	125	133	107	95	115	104	114	117	129	155	158	144	132
131	130	120	111	116	123	109	119	128	135	145	131	106	115	115	122	104	85	74	64	58	82	83	83
75	72	83	78	68	70	69	82	82	79	74	50	58	56	40	58	72	100	97	71	83	51	36	32
40	50	56	59	72	77	66	57	85	124	118	116	119	125	133	132	136	131	114	74	76	92	79	90
56	40	36	19	12	21	22	20	36	47	63	52	50	62	82	95	92	61	31	29	33	25	27	21
19	14	13	8	1	8	26	19	1	2	3	9	12	16	21	33	37	31	23	25	24	40	57	77
73	84	72	80	94	110	87	73	87	74	71	89	135	128	111	79	42	27	17	21	24	17	17	18
30	37	39	45	39	37	37	35	43	38	33	38	38	29	35	62	68	63	58	47	47	38	32	26
33	49	53	56	46	38	33	31	25	15	26	63	110	117	98	80	67	48	34	28	32	29	32	21
12	6	4	4	7	8	10	13	9	6	8	8	7	2	10	21	27	35	27	23	21	16	14	17
22	28	47	49	54	50	45	22	17	20	20	22	17	14	15	11	9	7	9	10	23	16	20	24
18	20	31	23	19	15	11	15	5	0	1	3	10	17	22	36	35	31	36	63	71	94	101	87
85	92	104	96	91	81	82	93	89	75	82	51	74	101	94	89	69	48	46	52	59	69	62	72
72	100	121	146	164	144	170	169	183	182	180	182	182	182	175	144	124	146	113	105	99	119	123	120
124	101	54	54	50	38	46	33	34	47	53	97	139	163	176	177	176	156	124	90	85	113	108	95
90	71	54	65	84	46	24	24	48	121	121	98	108	138	150	153	150	141	81	56	33	49	67	69
62	63	127	131	133	104	146	160	155	139	144	135	114	112	126	123	121	119	99	69	67	68	78	35
120 114 67 128 168 171 143 136 138 46 116 97 101 145 157 150 153 143 162 152 146 108 113 100 146 36 106 143 127 86 104 103 111 119 145 141 130 117 81 109 135 161 162 161 161 160 169 170 169 167 134 109 111 122 118 17 20 33 147 135 160 166 158 140 135 137 181 166 121 156 171 176 182 180 182 175 180 167 120 126 124 117 138 84 134 182 184 184 184 180 167 177 184 182 183 184 184 175 175 175 174 174 162 142 117 125 142 155 156 162 163 162 164 164 159 135 131 116 82 101 115 107 82 104 130 124 109 113 99 122 113 100 96 110 123 101 86 114 115 97 108 126 122 114 119 126 103 111 143 105 56 127 156 180 179 113 104 126 57 109 146 153 153 143 133 86 139 167 152 125 92 124 125 120 114 121 118 90 107 112

63 105 151 105 54 67 100 157 170 153 162 140 114 118 129 164 167 177 179 181 183 180 174 178 178 180 181 181 181 177 166 173 166 143 85 126 128 118 137 149 150 150 155 135 97 109 104 105 107 103 148 155 155 123 114 134 169 181 181 182 183 186 177 161 131 79 115 122 126 117 109 48 117 69 137 129 74 102 125 141 135 151 147 138 128 111 111 136 93 106 116 131 133 117 136 129 103 106 90 104 81 100 103 105 95 108 149 160 111 64 114 124 156 153 112 79 106 130 150 151 138 98 108 109 108 113 130 130 122 104 78 113 135 146 155 150 157 146 120 104 117 124 111 74 109 139 107

58	58	59	45	35	43	35	37	16	17	13	19	23	22	36	34	25	15	14	11	12	9	19	33
38	36	28	15	17	10	6	3	3	6	15	17	9	10	11	30	39	49	45	9	1	3	13	22
48	55	42	57	60	59	45	43	37	28	57	65	47	44	67	78	70	68	57	46	60	59	30	38
29	29	16	11	17	15	17	6	8	24	22	28	17	23	17	15	10	7	4	6	6	16	14	14
8	22	17	18	23	20	16	27	35	39	37	29	34	29	22	16	25	40	41	29	41	71	84	72
45	36	34	34	27	14	6	0	2	4	8	8	5	3	1	0	0	2	5	16	9	2	1	3
8	23	20	43	33	38	27	7	5	4	4	1	1	1	2	1	1	1	1	1	2	2	1	2
13	38	32	17	11	9	9	2	3	6	6	9	16	18	22	26	24	22	38	46	54	50	45	43
68	93	96	99	116	107	90	84	105	75	58	43	49	43	39	29	23	13	9	2	4	8	5	8
3	9	8	9	14	26	21	4	6	16	40	53	69	72	89	98	112	82	48	31	29	50	64	77
75	64	69	77	84	56	63	46	48	57	88	101	100	94	85	72	70	56	36	35	31	44	49	67
64	46	40	30	32	9	21	32	28	47	85	81	40	58	63	49	18	25	18	19	23	14	17	28
48	46	37	30	21	19	15	10	7	13	11	17	19	17	13	12	6	3	0	0	0	1	1	1
1	2	2	3	5	7	10	5	4	3	2	3	3	1	1	3	5	10	8	3	2	2	4	5
19	2	4	14	7	7	3	1	1	1	1	4	11	21	8	8	11	15	12	9	4	1	1	1
1	1	1	2	2	2	2	3	11	6	2	8	12	41	59	31	41	40	26	20	15	21	14	5
20	44	19	25	34	28	38	46	34	16	9	2	3	5	9	13	22	22	26	24	45	67	86	96
79	66	79	76	77	67	63	60	71	70	79	66	57	68	69	66	66	63	45	48	30	35	50	56
71	60	81	56	20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	3	5	21	24	22
16	14	9	14	19	18	22	23	11	6	10	19	27	44	38	30	19	17	11	20	29	16	31	27
28	24	10	7	2	2	1	1	1	1	1	1	2	2	1	0	0	0	2	3	10	12	32	40
46	45	47	47	42	48	28	8	6	6	3	4	11	1/	1/	16	26	21	22	8	5	2	2	4
13	9	3	10	3	3	1	1	1	1	3	3	1	1	2	12	1	2	4	9	5	4	13	17
18	14	11	10	70	18	3	3	3	/ 2	12	19	30	10	17	47	18	21	2 2	0	2 15	9 20	8 22	9 45
35	50	53	63	83	73	85	111	ے 138	- 130	100	101	9	107	20	105	0	102	102	9 70	13	20 65	06 06	40
56	31	24	20	10	28	23	16	130	139	21	24	99 22	22	20	105	90 21	28	31	10	43	20	90 11	90 58
53	٦٦ ٨٩	24 11	20 /1	19	20	16	8	3	1	2 I 1	2 4 1	22	1	20	13	21	20	21	7	۱ <i>۲</i>	23	10	11
33 8	43 1	++ 2	-+ 1	40	0	3	6	1/	7	2	1	1	1	1	1	2 1	- -	1	11	9 21	24	20	10
3	4	2	1	0	0	0	0	0	0	2	0	0	0	0	0	0	1	1	0	21	24	20	0
0	1	2	י ז	8	8	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1	1	<u>د</u> 1	1	0	1	0	0	0	0	0	0	0	1	0	0	2		5	1	0	0	0	2
7	39	51	61	52	32	9	2	3	13	21	29	42	74	107	109	82	50	36	18	29	35	28	26
26	36	28	25	31	27	12	2	6	8	6	23 7	16	1	27	108	84	28	26	38	50	74	82	84
20	00	20	20	01	~ '	14	4	0	0	5	'	.0		~ (100	01	20	20	00	00		02	01

93 106 109 114 115 101 90 111 141 160 166 170 174 174 143 59 134 66 107 110 65 119 69 107 55 105 121 130 138 116 107 114 110 118 97 100 82 121 109 125 79 114 104 98 125 135 141 120 104 110 76 105 123 114 111 110

10	15	34	33	36	34	38	19	18	12	8	1	2	2	3	2	3	2	4	7	10	18	26	25
15	10	9	5	2	1	0	0	0	0	1	1	1	2	1	1	1	2	3	6	7	17	31	47
42	31	31	33	37	46	40	27	17	29	40	53	51	45	13	11	14	61	118	130	91	69	115	145
149	139	135	144	163	172	167	167	167	167	167	167	167	50	44	76	61	32	17	20	22	45	32	33
7	2	2	2	5	2	0	0	0	0	0	2	2	0	2	11	4	1	1	5	1	0	0	2

5.1.1.2. Validation Data

The data below is the hourly validation data from Amaranth wind farm used to verify the accuracy of the three models. It is used to generate the plots and tables in section 3.2

											I	Hour											
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24
4	6	3	6	12	22	14	9	11	10	19	21	20	19	23	13	14	15	17	23	39	50	38	27
14	6	4	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	5	6	0	0
2	2	13	43	50	53	54	44	29	36	56	70	107	94	94	94	94	94	31	33	38	38	38	38
38	38	38	38	38	38	38	38	4	1	0	0	0	0	0	0	0	9	10	11	11	10	12	18
8	5	5	2	1	5	10	15	26	17	21	26	24	20	30	16	11	10	5	2	9	9	2	8
6	5	2	2	2	5	6	12	29	50	67	55	62	91	96	113	97	81	74	83	70	103	99	66
54	50	50	50	44	46	44	36	54	44	49	68	84	134	126	106	103	98	53	61	84	63	36	31
48	60	71	49	59	83	88	85	80	86	85	78	81	65	57	34	19	34	25	30	37	33	37	47
33	35	30	37	27	48	42	29	32	27	37	43	43	45	39	31	28	22	19	22	15	12	6	3
1	0	0	0	1	2	8	19	16	11	10	8	12	14	17	24	24	37	40	38	51	80	101	98
116	135	108	89	89	88	56	103	72	65	59	49	45	34	49	52	41	39	31	18	17	14	10	11
22	19	87	108	105	63	45	21	46	46	43	22	11	12	9	2	2	5	7	1	3	6	9	11
16	22	19	22	36	37	54	38	32	28	10	8	9	6	4	14	16	19	33	69	91	83	54	44
66	113	136	129	57	35	71	88	89	80	103	105	97	101	111	100	94	99	112	123	131	132	142	99
102	112	109	92	79	50	30	20	27	70	102	56	62	87	81	61	35	23	20	23	7	6	31	15
18	38	31	35	28	27	18	23	40	45	95	89	101	115	103	128	136	95	74	61	51	37	43	68
62	64	61	53	55	57	45	45	45	45	45	45	45	59	72	64	53	40	27	21	24	13	3	3
5	5	5	10	17	16	11	8	4	13	14	9	8	6	12	19	24	28	29	34	34	39	66	111
97	47	73	73	71	71	71	57	35	51	35	56	69	57	33	37	34	39	48	53	35	26	31	23
15	9	12	48	49	55	33	28	44	46	38	28	24	31	29	21	28	25	16	12	10	16	19	16
18	25	40	39	33	38	27	30	13	10	6	8	6	3	3	6	6	10	21	26	25	25	27	32
38	47	47	48	56	57	56	41	13	9	11	6	10	11	16	17	19	15	18	37	57	53	50	60
68	58	74	53	46	40	37	13	12	20	25	27	18	15	13	24	24	21	25	32	37	32	43	56
53	39	39	49	52	52	59	80	90	94	89	128	112	111	95	111	95	69	47	73	69	48	35	20
10	22	6	8	25	33	32	16	16	14	26	26	35	46	98	134	137	128	109	102	95	115	102	65

40	25	23	32	34	22	31	39	61	57	57	58	48	43	41	38	39	25	11	9	9	8	9	8
2	0	0	0	0	0	0	1	6	14	9	6	4	4	4	2	1	3	11	11	20	21	18	14
13	3	0	2	3	3	0	0	0	0	0	0	0	0	0	0	1	2	6	8	4	2	3	12
10	16	7	9	15	10	9	5	0	0	0	1	2	2	0	0	2	4	5	10	12	9	15	21
28	25	18	11	6	3	4	1	0	1	2	2	1	1	0	0	0	3	4	4	1	0	2	14
17	15	13	8	5	7	13	8	1	0	0	0	1	1	0	0	2	3	16	17	18	37	25	26
34	45	55	53	53	51	37	18	11	11	10	10	12	15	17	27	36	32	54	62	61	71	66	86
119	106	99	89	84	84	87	65	39	36	27	23	33	39	30	24	23	12	10	10	21	27	25	35
27	18	15	9	7	7	8	9	8	7	7	1	5	14	33	35	23	18	19	2	0	0	0	3
6	22	35	46	48	47	36	24	13	9	19	39	56	73	105	116	113	100	105	156	156	160	165	159

5.1.2. Wolfe Island Wind Farm Raw Data

5.1.2.1. Training Data

The data below is the hourly training data from Wolfe Island wind farm used to create the Markov chain and ARMA models. It

is used to generate the plots and tables section 3.3.

											Но	ur											
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24
16	23	12	10	8	8	9	12	12	8	6	1	0	0	2	4	13	10	5	2	11	30	33	61
67	41	40	30	22	28	27	24	7	17	33	17	4	1	1	0	0	2	2	3	9	4	5	19
34	54	78	118	124	135	155	155	165	169	175	181	183	182	181	182	182	179	181	168	146	128	93	79
64	75	116	111	91	61	59	80	119	108	117	125	133	107	95	115	104	114	117	129	155	158	144	132
131	130	120	111	116	123	109	119	128	135	145	131	106	115	115	122	104	85	74	64	58	82	83	83
75	72	83	78	68	70	69	82	82	79	74	50	58	56	40	58	72	100	97	71	83	51	36	32
40	50	56	59	72	77	66	57	85	124	118	116	119	125	133	132	136	131	114	74	76	92	79	90
56	40	36	19	12	21	22	20	36	47	63	52	50	62	82	95	92	61	31	29	33	25	27	21
19	14	13	8	1	8	26	19	1	2	3	9	12	16	21	33	37	31	23	25	24	40	57	77
73	84	72	80	94	110	87	73	87	74	71	89	135	128	111	79	42	27	17	21	24	17	17	18
30	37	39	45	39	37	37	35	43	38	33	38	38	29	35	62	68	63	58	47	47	38	32	26
33	49	53	56	46	38	33	31	25	15	26	63	110	117	98	80	67	48	34	28	32	29	32	21
12	6	4	4	7	8	10	13	9	6	8	8	7	2	10	21	27	35	27	23	21	16	14	17
22	28	47	49	54	50	45	22	17	20	20	22	17	14	15	11	9	7	9	10	23	16	20	24
18	20	31	23	19	15	11	15	5	0	1	3	10	17	22	36	35	31	36	63	71	94	101	87
85	92	104	96	91	81	82	93	89	75	82	51	74	101	94	89	69	48	46	52	59	69	62	72
72	100	121	146	164	144	170	169	183	182	180	182	182	182	175	144	124	146	113	105	99	119	123	120
124	101	54	54	50	38	46	33	34	47	53	97	139	163	176	177	176	156	124	90	85	113	108	95
90	71	54	65	84	46	24	24	48	121	121	98	108	138	150	153	150	141	81	56	33	49	67	69
62	63	127	131	133	104	146	160	155	139	144	135	114	112	126	123	121	119	99	69	67	68	78	35
44	47	48	56	59	48	46	67	46	96	79	79	120	114	96	89	84	76	67	56	40	24	18	13

67

13 11 16 13 3 0 1 2 10 23 34 45 50 63 68 73 61 80 75 67 128 168 171 143 94 90 91 90 89 87 91 92 91 89 87 80 86 112 77 34 21 19 8 136 138 142 164 156 4 14 25 29 37 52 79 103 55 46 116 148 113 41 54 43 64 102 1 0 97 101 86 54 54 0 0 1 2 4 2 3 28 32 39 17 38 29 24 29 37 27 55 22 83 70 50 33 35 51 88 15 16 23 34 26 83 93 73 17 36 43 54 88 112 96 129 98 110 108 113 89 98 100 146 145 157 150 153 143 162 152 146 97 38 54 51 29 36 106 143 127 87 79 104 95 91 79 86 104 103 111 97 89 57 57 55 40 27 39 56 52 26 18 28 17 15 4 15 42 52 60 68 76 96 119 145 141 130 117 92 62 45 31 43 38 56 86 82 31 38 50 81 109 135 161 162 161 161 160 169 170 169 167 134 80 45 55 51 59 109 111 122 118 98 60 34 31 44 37 22 37 31 20 17 20 16 19 16 32 29 12 5 5 9 14 28 53 44 49 38 47 33 147 135 152 160 166 158 140 135 137 181 166 121 156 171 176 182 180 182 175 180 167 120 126 124 117 138 118 87 74 63 84 134 182 184 184 184 180 167 177 184 182 183 184 184 175 175 175 174 174 162 146 138 126 142 117 125 142 155 156 162 163 162 164 164 159 135 131 116 93 84 55 25 18 20 1 0 1 1 20 16 1 6 41 69 62 59 62 76 68 67 74 88 86 78 50 35 19 13 20 34 43 41 47 51 72 66 59 59 82 101 115 107 82 104 129 130 124 109 113 78 62 65 99 122 113 100 96 110 123 101 89 81 86 114 115 68 86 93 60 95 103 111 80 23 10 11 18 19 23 51 97 108 126 122 122 114 119 126 143 105 51 47 52 38 20 14 19 22 26 30 56 127 156 180 179 113 51 63 32 38 56 45 26 35 62 71 84 67 45 32 25 7 3 11 14 24 30 38 39 40 54 56 47 50 63 86 61 61 69 44 21 35 53 40 28 20 21 31 29 28 35 34 35 26 17 20 31 35 57 104 126 121 109 68 51 58 35 31 34 31 57 109 146 153 153 143 133 126 108 103 104 88 75 64 50 46 53 52 48 42 43 38 40 32 26 23 19 21 21 21 18 14 17 20 31 24 28 20 15 15 22 33 26 21 22 20 28 43 66 72 86 139 167 152 125 80 57 72 70 92 124 125 120 114 121 118 101 68 74 60 36 31 35 35 25 21 18 17 17 19 34 47 65 71 90 71 46 29 20 50 64 54 37 40 16 14 24 58 77 68 60 47 36 33 47 58 90 107 112 90 72 71 57 54 43 56 51 52 62 57 64 63 75 82 87 89 52 36 48 80 89 85 65 71 70 71 53 39 24 7 19 52 78 87 73 59 44 30 19 12 18 32 52 59 56 53 43 28 32 42 39 16 10 10 8 10 10 6 24 28 17 38 32 24 27 34 25 17 24 22 2 2 4 12 7 11 12 29 12 16 14 9

21 26 33 34 23 24 20 9 1 2 5 11 12 9 14 16 22 15 9 4 3 1 1 1 0 0 9 10 22 8 11 37 22 16 15 15 26 32 45 58 69 66 50 31 43 63 105 151 105 54 28 11 37 49 5 14 22 26 22 38 55 59 56 64 71 47 36 32 23 10 3 22 34 48 81 73 67 100 157 170 153 162 140 114 118 129 164 167 177 179 181 183 180 174 178 178 180 181 181 181 177 166 173 166 143 101 80 70 76 93 90 72 68 85 126 128 118 137 149 150 150 155 135 102 59 37 29 23 10 2 3 15 31 36 34 38 35 56 47 58 71 72 76 64 53 53 51 59 65 72 82 97 109 104 105 107 103 148 155 155 123 114 134 169 181 181 182 183 186 177 161 131 86 75 45 38 47 58 49 72 79 61 38 28 16 32 79 115 122 126 117 109 81 40 33 30 20 21 37 25 17 31 40 33 17 11 14 11 4 10 14 22 46 52 37 29 21 11 16 32 46 40 35 33 22 20 20 17 18 20 30 35 26 25 28 21 21 21 22 33 34 46 50 44 40 34 34 37 21 22 18 55 61 65 63 54 35 7 18 32 48 62 82 83 51 48 117 72 55 34 33 33 42 67 62 46 25 35 65 95 46 4 52 68 23 22 19 13 13 26 25 15 19 25 23 19 13 6 17 26 44 51 62 69 137 129 85 43 54 35 23 45 42 31 26 37 54 43 55 65 101 81 33 58 74 102 125 141 135 143 145 151 147 138 128 111 111 136 108 95 121 93 106 116 131 133 117 97 96 89 87 83 79 75 63 48 35 44 49 42 32 32 42 38 23 25 62 62 71 69 77 79 67 60 70 72 66 45 44 41 40 42 53 53 41 42 50 35 17 19 57 60 59 61 72 75 72 63 49 31 19 14 19 41 41 43 26 17 13 10 50 56 52 50 45 55 44 31 43 57 46 39 39 32 24 12 8 51 16 27 19 40 34 21 64 94 75 67 67 79 89 136 129 103 106 82 65 84 119 109 74 61 44 32 51 63 64 30 27 38 28 27 38 46 56 63 64 81 100 100 68 39 60 80 90 104 54 40 50 46 96 95 103 105 78 58 40 29 27 44 90 98 95 108 149 160 111 75 80 93 59 65 82 40 64 114 75 36 33 31 56 57 35 39 62 96 91 64 49 63 78 46 26 34 25 27 36 32 33 42 43 44 45 46 65 124 156 153 112 82 79 79 106 130 150 151 138 141 144 121 84 67 61 45 36 35 42 62 57 53 58 95 98 108 109 108 113 130 130 122 104 81 43 34 49 63 52 34 34 26 20 11 15 28 30 26 22 23 19 21 17 14 19 15 12 -5 18 24 37 43 37 34 21 12 7 10 18 18 13 17 19 20 20 32 49 62 62 64 72 55 65 67 73 80 94 77 78 113 135 146 155 150 157 146 120 104 117 124 111 68 49 71 30 30 11 13 13 12 8 11 10 15 10 10 11 11 15 20 9 12 13 9 6 10 6 4 6 7 11 4 10

8 12 16 14 16 12 3 3 4 2 0 0 0 0 1 2 4 22 38 30 30 35 42 48 48 73 88 83 101 96 56 34 16 32 23 40 36 30 33 43 59 80 60 71 49 35 19 11 14 17 14 20 24 17 24 45 60 54 52 48 45 45 38 27 20 9 11 4 13 20 19 29 36 18 46 36 51 80 63 46 55 55 67 37 38 41 42 28 14 3 11 37 43 86 76 56 92 74 41 31 47 58 56 34 29 24 24 24 27 35 27 44 49 52 95 138 154 157 158 160 158 159 160 160 159 158 157 157 160 159 151 95 112 160 160 159 158 143 139 159 160 156 158 159 159 159 159 159 160 160 158 159 160 160 156 145 149 155 155 149 116 89 63 40 40 31 18 29 19 33 55 55 38 32 14 36 40 75 97 105 94 100 93 94 63 45 40 36 40 49 54 66 65 63 61 56 65 79 103 117 87 79 104 112 104 93 96 107 111 91 74 93 86 63 56 30 17 21 37 43 29 23 10 82 84 88 96 9 11 1 11 22 24 33 31 11 14 14 10 16 17 82 67 113 128 100 104 130 122 133 95 73 126 138 135 128 139 138 145 154 134 114 103 99 107 127 135 123 118 116 114 121 130 136 133 101 87 75 71 89 84 83 95 96 82 67 69 74 78 71 65 52 44 33 33 21 5 16 55 39 23 34 55 61 61 66 86 96 82 75 65 77 65 55 64 69 65 72 91 64 43 43 70 68 58 44 33 39 52 53 48 37 31 30 23 20 24 30 20 44 41 34 33 36 32 18 16 15 12 7 12 16 38 4 7 18 36 54 46 54 37 22 29 54 77 81 74 85 115 129 124 132 122 80 60 42 42 47 75 102 107 106 92 60 47 64 130 53 54 86 121 149 147 134 123 126 125 133 117 119 116 108 108 111 115 110 126 131 124 126 133 108 77 70 57 52 49 65 70 72 66 49 43 44 78 84 96 97 88 85 90 75 78 84 96 114 134 116 65 42 23 44 28 63 98 105 109 117 85 61 42 35 24 36 38 26 30 61 74 65 34 23 15 12 22 36 29 37 57 61 48 34 36 57 69 64 59 49 38 46 52 50 68 92 59 56 66 88 93 85 80 95 109 83 64 61 46 28 21 9 19 24 30 41 58 59 77 72 67 35 52 72 104 112 126 126 99 154 158 160 52 83 90 121 130 118 81 96 109 123 98 62 60 107 157 160 148 158 154 134 72 13 17 30 82 80 8 11 10 23 12 10 11 9 11 6 21 5 12 16 41 28 28 6 14 55 43 30 27 80 53 52 55 80 139 107 55 53 29 13 14 35 27 17 17 55 69 94 79 108 105 146 149 146 125 156 160 159 158 158 158 158 157 158 155 154 151 151 158 160 134 119 73 16 26 26 11 5 27 76 124 156 159 152 157 148 126 106 107 109 132 131 147

148 125 142 141 126 82 70 69 100 140 154 125 143 124 138 148 141 125 94 69 48 35 55 33 20 28 25 22 16 18 16 6 1 0 4 2 0 1 5 13 35 43 52 70 90 135 156 158 159 155 153 147 127 78 67 49 36 30 37 54 64 75 71 119 131 102 71 79 76 97 138 154 158 159 156 137 85 63 52 18 26 9 3 3 3 3 3 3 6 4 1 1 11 50 43 42 45 72 89 95 99 85 64 49 56 55 37 26 38 34 76 73 96 121 155 156 133 87 37 38 111 155 155 146 149 151 159 161 158 156 159 159 159 158 156 136 83 38 56 118 128 99 23 4 68 136 115 151 156 155 156 158 153 154 158 158 159 159 159 159 158 158 159 158 156 156 156 156 155 156 149 101 119 125 116 108 151 150 132 116 87 66 69 87 79 67 59 41 26 30 36 29 23 6 7 9 8 11 13 16 18 16 29 43 52 33 38 59 43 40 56 70 97 12 9 12 11 100 82 58 56 52 52 52 26 17 9 78 9 14 19 17 16 37 78 117 107 113 122 112 140 152 154 150 150 149 141 114 111 69 67 50 52 52 50 44 54 66 78 77 33 12 8 25 124 154 154 154 115 140 135 135 127 118 61 100 108 114 95 100 124 99 54 54 50 96 113 114 89 88 76 88 92 74 74 51 98 150 156 155 118 100 145 85 75 36 70 68 38 36 43 40 32 31 30 17 7 0 0 0 0 4 11 13 13 25 34 24 22 11 9 45 47 70 76 67 9 17 42 73 92 107 121 66 41 22 17 11 6 17 23 11 5 5 9 11 12 8 6 6 115 63 50 25 20 55 74 82 95 112 98 107 96 94 86 66 48 36 33 55 56 52 67 15 85 64 33 15 7 1 3 5 2 1 6 5 0 3 7 3 16 12 14 29 38 70 68 50 49 54 45 51 36 47 52 29 27 24 23 11 6 89 101 76 52 42 32 36 37 49 56 82 112 142 130 98 92 91 67 46 41 34 25 14 10 14 16 13 22 13 25 54 63 102 102 104 86 90 103 99 93 97 92 52 54 50 34 25 28 19 25 32 47 58 65 86 124 141 114 83 122 137 127 122 118 85 52 46 46 53 64 83 106 112 105 100 93 77 80 97 108 148 156 153 146 145 134 117 113 111 116 108 110 77 68 85 76 75 65 53 60 52 49 69 111 144 135 115 110 76 82 90 81 87 86 61 41 37 46 64 76 77 76 59 55 43 33 36 58 57 42 35 54 57 54 63 57 56 52 20 25 18 11 15 23 29 26 33 38 28 20 18 34 45 69 88 78 36 30 37 20 15 15 9 23 27 28 51 60 67 66 43 29 10 7 3 7 3 1 4 2 10 17 8 2 0 0 1 0 0 2 2 5 86 9 2 13 13 8 18 6 9 11 28 0 29 22 18 10 0 0 0 0 0 0 0 1 2 11 22 10 11 16 32 52 64 73 68 62 37 2 4 16 36 102 122 129 97 111 134 136 115 110 73 87 79 100 106 114 104 106 76 50 35 25 21 19 17 12 11 5 3 3 5 7 23 73 88 88 108 136 153 160 148 102 53 55 83 82 115 117 109 115 145 155 155 148 145 146 147 151 158 159 159 156 140 147 116 65 40 55 74 87 79 75 50 43 69 36 25 38 18 14 10 5 1 1 1 3 11 28 52 55 58 70 74 70 52 42 35 41 70 82 66 84 107 114 135 134 94 81 78 98 110 120 130 100 69

56 28 64 81 147 152 159 157 135 147 139 133 146 145 123 97 72 40 27 21 36 29 60 79 84 32 19 12 8 20 12 9 23 37 38 28 6 15 10 19 43 64 57 38 32 17 15 26 26 17 22 35 45 34 30 40 39 61 52 32 30 56 46 47 43 24 27 22 59 105 90 55 26 12 23 18 25 27 23 31 35 41 50 52 63 62 59 62 76 103 103 93 40 62 49 30 26 15 9 22 27 16 12 19 42 37 58 72 103 77 83 77 51 36 63 54 45 42 41 31 27 16 17 20 28 27 64 92 118 145 151 140 76 67 71 82 96 95 89 82 82 59 67 61 55 57 96 149 119 103 111 86 106 135 142 112 34 9 24 65 11 14 56 65 62 88 92 52 81 95 103 79 118 127 121 106 151 158 156 152 89 89 50 44 39 58 73 66 42 42 39 26 21 25 27 18 25 144 150 157 159 160 161 161 160 160 160 160 160 158 153 151 145 142 145 143 133 144 139 127 123 116 121 104 103 98 100 84 34 11 17 15 10 9 14 28 32 34 45 43 34 65 65 44 52 36 26 20 15 11 13 23 28 17 15 10 6 14 24 25 16 9 19 24 43 47 27 21 10 19 31 62 82 96 134 137 101 71 58 1 22 10 8 31 57 39 23 72 51 83 76 88 102 144 158 159 158 158 138 77 43 84 113 112 112 94 132 151 139 87 70 61 43 16 0 10 21 28 43 53 69 80 73 59 49 43 47 49 53 66 64 72 80 61 64 42 20 74 15 40 64 118 127 108 103 120 87 69 79 94 109 118 125 139 139 137 116 130 53 43 82 102 57 54 108 159 160 154 102 69 49 35 77 116 128 121 133 141 114 129 122 106 56 36 11 13 8 29 33 23 87 117 108 122 142 154 151 145 140 139 136 124 93 90 71 73 95 100 70 76 71 30 30 48 41 27 14 10 7 13 15 31 26 19 11 40 54 34 8 13 22 32 41 36 24 23 24 17 12 20 43 48 48 9 11 45 51 47 46 31 44 47 42 42 49 59 37 15 17 13 2 10 14 20 21 19 15 12 15 12 14 15 22 20 18 14 13 12 10 12 4 12 12 17 27 22 59 92 88 88 76 14 21 92 112 116 118 116 135 135 139 125 117 61 57 49 33 34 47 48 41 36 26 15 9 12 14 34 41 64 33 29 45 45 45 29 10 48 35 42 45 53 48 34 22 18 12 13 14 30 30 20 51 24 18 25 21 11 6 19 24 19 11 16 27 33 55 71 74 75 76 76 76 76 76 76 77 77 77 76 74 76 76 75 70 55 72 74 76 75 75 64 68 77 77 75 76 77 77 77 77 76 77 77 76 77 76 76 75 75 75 76 77 77 77 76 60 49 43 47 59 63 61 50 47 49 34 29 23 18 13 16 15 5 33 39 50 51 40 30 39 50 42 43 56 64 70 76 59 35 21 17 11 76 77 77 77 75 71 72 69 4 28 60 52 36 27 28 34 42 35 40 40 42 37 33 33 37 36 44 49 39 21 11 29 10 2 13 17 23 31 36 40 52 50 47 41 45 50 52 44 46 54 50 42 19 19 22 27 23 11 4 26 41 39 28 19 16 11 11 3 0 11 10 13 20 18 16 12 13 8 12 16 19 14 7 10 6 13 16 20 31 22 18 13 14 19 34 42 49 47 46 51 64 66 71 73 65 45 24 20 21 28 38 53 63 57 43 50 44 50 32 19 49 22 55 71 60 58 63 65 57 73 72 70 65 64 67 64 61 61 68 66 51 55 52 44 46 39 33 26 29 37 23 18 23 34 32 43 57 59 61 59 55 47 46 31 39 28 40 47 53 23 16 13 28 34 20 18 24 43 59 65 65 52 42 29 15 1 12 20 14 23 28 22 20 37 49 46 25 14 11 8 20 23 15 19 24 17 13 9 23 32 37 33 33 35 27 27 25 32 33 36 35 36 50 45 37 38 27 15 11 28 29 4 0 1 0 0 2 7 10 15 16 29 26 31 22 13 12 18 24 40 63 68 70 62 71 76 77

5.1.2.2. Validation Data

The data below is the hourly validation data from Wolfe Island wind farm used to verify the accuracy of the three models. It is

used to generate the plots and tables in section 3.3

												Hour											
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24
4	6	3	6	12	22	14	9	11	10	19	21	20	19	23	13	14	15	17	23	39	50	38	27
14	6	4	6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	5	6	0	0
2	2	13	43	50	53	54	44	29	36	56	70	107	94	94	94	94	94	31	33	38	38	38	38
38	38	38	38	38	38	38	38	4	1	0	0	0	0	0	0	0	9	10	11	11	10	12	18
8	5	5	2	1	5	10	15	26	17	21	26	24	20	30	16	11	10	5	2	9	9	2	8
6	5	2	2	2	5	6	12	29	50	67	55	62	91	96	113	97	81	74	83	70	103	99	66
54	50	50	50	44	46	44	36	54	44	49	68	84	134	126	106	103	98	53	61	84	63	36	31
48	60	71	49	59	83	88	85	80	86	85	78	81	65	57	34	19	34	25	30	37	33	37	47
33	35	30	37	27	48	42	29	32	27	37	43	43	45	39	31	28	22	19	22	15	12	6	3
1	0	0	0	1	2	8	19	16	11	10	8	12	14	17	24	24	37	40	38	51	80	101	98
116	135	108	89	89	88	56	103	72	65	59	49	45	34	49	52	41	39	31	18	17	14	10	11
22	19	87	108	105	63	45	21	46	46	43	22	11	12	9	2	2	5	7	1	3	6	9	11
16	22	19	22	36	37	54	38	32	28	10	8	9	6	4	14	16	19	33	69	91	83	54	44
400	113	136	129	57	35	71	88	89	80	103	105	97	101	111	100	94 25	99	112	123	131	132	142	99
102	20	109	92	79	5U 27	30	20	27	10	102	00	101	8/ 115	102	100	35	23	20	23	[[]	0 27	31	15
10	30 64	31 61	30 52	20 55	21 57	10	23 45	40	40	95	09 45	101	50	103	120	52	95 40	74 27	21	24	31 12	43	00
02 5	04 5	5	10	17	57 16	40	40	40 1	40	40	40	40 0	59	12	10	24	40 20	21	21	24	20	5 66	ۍ 111
07	17	73	73	71	71	71	57	4 35	51	35	9 56	60	57	33	37	24	20	29 18	53	35	28	31	23
15	4/ Q	12	/8	/ I /Q	55	23	28	ΔΔ ΔΔ	46	38	28	24	31	20	21	28	25	16	12	10	20 16	10	23 16
18	25	12	-0 -20	33	38	27	20	13	10	6	20	6	3	20	6	20	10	21	26	25	25	27	32
38	20 47	40	48	56	57	56	41	13	9	11	6	10	11	16	17	19	15	18	37	57	53	50	60
68	58	74	53	46	40	37	13	12	20	25	27	18	15	13	24	24	21	25	32	37	32	43	56
53	39	39	49	52	52	59	80	90	_0 94	89	128	112	111	95	111	95	69	47	73	69	48	35	20
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10	22	6	8	25	33	32	16	16	14	26	26	35	46	98	134	137	128	109	102	95	115	102	65
40	25	23	32	34	22	31	39	61	57	57	58	48	43	41	38	39	25	11	9	9	8	9	8
2	0	0	0	0	0	0	1	6	14	9	6	4	4	4	2	1	3	11	11	20	21	18	14
13	3	0	2	3	3	0	0	0	0	0	0	0	0	0	0	1	2	6	8	4	2	3	12
10	16	7	9	15	10	9	5	0	0	0	1	2	2	0	0	2	4	5	10	12	9	15	21
28	25	18	11	6	3	4	1	0	1	2	2	1	1	0	0	0	3	4	4	1	0	2	14
17	15	13	8	5	7	13	8	1	0	0	0	1	1	0	0	2	3	16	17	18	37	25	26
34	45	55	53	53	51	37	18	11	11	10	10	12	15	17	27	36	32	54	62	61	71	66	86
119	106	99	89	84	84	87	65	39	36	27	23	33	39	30	24	23	12	10	10	21	27	25	35
27	18	15	9	7	7	8	9	8	7	7	1	5	14	33	35	23	18	19	2	0	0	0	3
6	22	35	46	48	47	36	24	13	9	19	39	56	73	105	116	113	100	105	156	156	160	165	159

5.1.3. ERCOT System-wide Raw Data

5.1.3.1. Training Data

The data below is the hourly training data from the ERCOT system-wide used to create the Markov chain and ARMA models.

It is used to generate the plots and tables section 3.4.

					Ho	our					
1	2	3	4	5	6	7	8	9	10	11	12
9554.8	9362.31	8327	7099.26	6338.87	6003.01	5602.71	5447.11	6474.38	6166.71	5731.21	5305.24
8727.32	8613.33	8397.51	8040.86	7461.66	7040.15	6351.71	6588.31	7970.88	8545.73	8566.86	8166.12
1820.8	1976.87	2128.83	2752.86	3436.34	3979.16	4114.92	3830.86	2558.99	2248.96	3501.81	4220.43
679.34	781.32	1027.15	1550.42	2030	2155.8	2110.45	1974.87	1342.18	1181.71	1778.51	1932.04
6629.28	6385.92	5860.43	5103.72	4372.51	3969.99	3975.78	3674.02	2983.4	3418.6	4185.37	4046
9288.2	9275.83	9089.71	8604.97	8054.47	6099.93	4061.01	3097.43	2555.08	2484.02	2177.27	2169.81
4829.18	4937.51	4716.93	3969.75	4111.1	4153.23	4254.91	4455.27	4650.85	5703.12	6271.63	6016.5
9119.13	9064.24	8994.01	8980.39	8968.66	8772.8	8607.35	8645.82	8745.09	8958.45	8812.39	8507.42

9244.11	9105.43	8956.52	8498.43	8306.01	8207.26	8030.05	7624.55	7392.86	7213.8	6502.64	6386.37
9002.65	8776.63	8679.92	8421.33	7844.11	7095.24	6296.18	6318.25	7571.28	8112.22	7463.71	6459.29

					Ho	our					
13	14	15	16	17	18	19	20	21	22	23	24
5037.53	4873.38	5139.43	4736.39	4476.55	5263.51	5873.18	6341.34	6914.51	7340.4	7754.27	8311.37
7359.39	6355.34	5695.04	5884.06	6697.3	7183.5	7627.75	6149.3	3612.71	2223.3	1813.93	1684.56
3808.84	3424.41	3466.09	3681.33	3829.01	3566.18	3162.03	2165.47	1083.86	741.22	723.69	769.66
1879.01	1470.85	1467.26	1587.05	1790.54	2076.53	2250.42	2405.44	2586.07	4060.31	5656.85	6599.23
4338.01	4510.5	4517.47	4556.46	4588.09	4671.75	5224.44	5398.41	6219.67	7551	8480.46	9150.56
2008.73	2025.26	2011.15	2091.31	2225.86	2442.32	2710.15	3194.65	3733.71	4949.77	5551.06	5382.94
5767.31	6053.74	6593.25	7380.02	8147.7	8783.21	9183.78	9226	8984.95	9024.83	9147.5	9181.73
8132.72	7728.79	7452.51	7230.17	7112.94	7392.17	7561.07	7749.76	8018.77	8645.5	9171.22	9284.34
6008.76	5452.68	5084.97	5448.39	6110.5	6842.59	7765.66	8351.67	8443.56	8532.28	8794.49	9017.56
5632.05	5289.15	5560.6	6210.07	6630.9	7332.79	7696.59	7458.72	6256.91	5999.42	6387.87	6865.02

5.1.3.2. Validation Data

The data below is the hourly validation data from ERCOT system-wide used to verify the accuracy of the three models. It is used to generate the plots and tables in section 3.4

					Ho	our					
1	2	3	4	5	6	7	8	9	10	11	12
6953.88	6964.82	7560.1	7505.61	6859.51	6468.97	5894.84	5142.95	5158.75	5382.66	4778.69	4119.7
4629.46	4816.23	5215.44	5214.61	4434.27	3892.21	3425.81	2940.78	3084.9	3718.1	4074.4	4180.54
					Ho	our					
13	14	15	16	17	18	19	20	21	22	23	24
3718.63	3719.3	3374.31	3338.69	3664.04	4704.71	5844.89	5544.6	3903.39	3566.71	4104.15	4187.59
4038.94	3762.79	3454.73	3840.56	4904.17	5146.76	5249.03	5245.77	5607.97	5158.31	5275.15	4921.21

52	Forecasted	l Data		4	6	4.83	6.69
J.Z.	I UIECASIEU	Dala		6	4	4.50	5.94
521	Amaranth W	ind Far	m	0	6	0.00	8.55
J.Z.T.	Forecasted [niu i an Data		0	0	0.00	0.57
	I UIECASIEU L	Jala		0	0	0.00	2.85
			1	0	0	0.00	2.17
	The data below	w gives	the forecasts	0	0	0.00	2.35
1				0	0	0.00	2.28
produc	ed by each mod	del over	the period of	0	0	0.00	2.29
.1 1	. 1		1 117 1 1	0	0	0.00	2.27
the val	idation data for	Amaran	th Wind Farm.	0	0	0.00	2.20
T .	1	.1 1 .	1 / 1 1 .	0	0	0.00	2.24
It is us	sed to generate 1	the plots	and tables in	0	0	0.00	2.23
	2.2			0	0	0.00	2.22
section	1 3.2.			0	0	0.00	2.20
				0	0	0.00	2.19
A (1		<u>ر</u> 1		0	0	0.00	2.18
Actual	Persistence N	Aarkov A	AKMA	2	0	0.00	2.17
4		4.83	3.80	5	25	/.00	4.30
6	b 4	4.50	/.04	0	5	4.30	7.40
3		4.50	8.49	0	0	0.00	/.81
10	3	4.50	4.45	0	0	0.00	0.48
12		10.00	9.20	2	0	0.00	2.38
22	2 12	27.30	15.03	12	2	0.00	4.50
14	$\frac{1}{14}$	20.50	25.36	13	12	20.50	5.85 17.20
11		0.1/	12.75	43	13	39.30 46.50	17.20
11	9	/.50	10.30	53	43	40.30	49.40
10) 10	10.00	13.44	54	53	54.50 44.50	40.33
15		20.90	11.34	54 44	54	44.50	52.40
21	$1 \qquad 19$	22.50	22.75	20	J4 14	40.50	<i>J</i> 2.30
20	21	21.30	21.60	29	20	36.50	25.90
12	$\frac{20}{2}$ 10	20.90	20.90	56	36	41 50	38 51
23 12	1	20.50	19.97	50 70	56	68 73	58.97
1.	1 13	20.50	23.04	107	50 70	99.83	69.88
15	+ 15 5 1/	20.50	16.63	94	107	87.94	111 22
15	7 15	21.00	16.35	94	94	87.94	83 70
23	13 R 17	20.50	18.82	94	94	87.94	91.67
2-	$\frac{17}{2}$	20.50	25.32	94	94	87.94	89.40
50	23	46 50	42.52 42.67	94 94	94	87 94	90.08
25	, 59 2 50	47 50	±2.07 50.89	31	94	25 50	89 91
27	,	-7.50 22.50	34 10	33	31	36 17	14 25
ے ۔ 1 /	1 30 1 77	20.50	25 72	38	33	47 50	38 47
14	τ <u>2</u> / δ 1/	20.50 4 50	12 50	38	38	47 50	37 50
C	, 14	4.30	12.30	50	50	т	57.50

38	38	47.50	37.78	5	10	7.00	11.05
38	38	47.50	37.70	2	5	0.00	5.37
38	38	47.50	37.72	9	2	6.17	3.39
38	38	47.50	37.72	9	9	6.17	12.37
38	38	47.50	37.72	2	9	0.00	9.77
38	38	47.50	37.72	8	2	8.50	2.09
38	38	47.50	37.72	6	8	4.50	11.50
38	38	47.50	37.72	5	6	7.00	6.38
38	38	47.50	37.73	2	5	0.00	6.64
38	38	47.50	37.73	2	2	0.00	2.95
4	38	4.83	37.73	2	2	0.00	4.00
1	Z	0.00	3.14	5	2	7.00	3.68
0	1	0.00	5.02	6	5	4.50	7.37
0	(0.00	1.45	12	6	10.00	7.49
0	(0.00	2.46	29	12	38.50	14.66
0	(0.00	2.15	50	29	46.50	33.02
0	(0.00	2.22	67	50	64.50	52.97
0	(0.00	2.19	55	67	66.50	67.67
0	(0.00	2.18	62	55	63.50	49.02
9	() 6.17	2.17	91	62	78.28	62.83
10	9	9 10.00	12.97	96	91	87.83	93.72
11	10) 7.50	11.05	113	96	94.50	90.85
11	11	7.50	12.79	97	113	96.40	112.15
10	11	10.00	12.28	81	97	49.50	86.81
12	10) 10.00	11.21	74	81	81.37	74.92
18	12	2 21.50	13.91	83	74	52.50	69.96
8	18	8 8.50	20.34	70	83	68.73	82.23
5	8	3 7.00	6.46	103	70	112.50	63.09
5	4	5 7.00	6.84	99	103	104.00	108.30
2	4	5 0.00	6.72	66	99	58.50	90.48
1	2	2 0.00	3.13	54	66	44.50	55.98
5	1	7.00	2.95	50	54	46.50	51.52
10	4	5 10.00	7.80	50	50	46.50	48.01
15	1() 15.50	12.40	50	50	46.50	49.03
26	15	5 26.30	17.07	44	50	46.50	48.74
17	26	5 21.00	28.94	46	44	41.00	41.62
21	17	22.50	14.69	44	46	46.50	46.08
26	21	26.30	23.60	36	44	36.50	42.40
24	26	5 23.50	27.04	54	36	44.50	33.85
20	24	4 21.50	23.64	44	54	46.50	57.95
30	20) 34.83	19.81	49	44	68.50	38.99
16	30) 15.50	32.93	68	49	67.00	50.47
11	16	5 7.50	12.32	84	68	71.00	70.01
10	11	10.00	12.24	134	84	131.00	83.63

126	134	126.83	139.83	37	27	30.50	25.96
106	126	117.33	114.06	43	37	39.50	40.27
103	106	112.50	97.49	43	43	39.50	43.36
98	103	109.50	98.70	45	43	37.50	42.47
53	98	54.50	92.37	39	45	38.50	45.13
61	53	53.50	40.13	31	39	25.50	37.15
84	61	71.00	64.82	28	31	30.00	29.84
63	84	54.75	85.36	22	28	27.30	28.33
36	63	36.50	54.21	19	22	20.90	21.55
31	36	25.50	30.75	22	19	27.30	19.89
48	31	47.50	31.50	15	22	15.50	23.97
60	48	60.50	51.72	12	15	10.00	14.37
71	60	67.50	60.32	6	12	4.50	13.52
49	71	68.50	71.07	3	6	4.50	6.54
59	49	81.50	41.54	1	3	0.00	4.93
83	59	52.50	62.08	0	1	0.00	2.97
88	83	78.36	85.02	0	0	0.00	2.31
85	88	112.50	84.44	0	0	0.00	2.48
80	85	95.50	81.03	1	0	0.00	2.42
86	80	93.14	76.02	2	1	0.00	3.62
85	86	112.50	84.70	8	2	8.50	4.46
78	85	73.50	81.02	19	8	20.90	11.41
81	78	49.50	73.69	16	19	15.50	22.62
65	81	67.50	79.42	11	16	7.50	15.77
57	65	60.00	58.55	10	11	10.00	11.72
34	57	36.50	54.97	8	10	8.50	11.67
19	34	20.90	28.36	12	8	10.00	9.27
34	19	36.50	18.00	14	12	20.50	14.76
25	34	22.50	39.01	17	14	21.00	15.57
30	25	34.83	22.13	24	17	23.50	18.93
37	30	30.50	33.00	24	24	23.50	26.37
33	37	36.17	38.27	37	24	30.50	24.22
37	33	30.50	31.94	40	37	33.50	40.46
47	37	51.50	38.57	38	40	47.50	39.38
33	47	36.17	48.68	51	38	62.50	37.29
35	33	39.83	28.94	80	51	95.50	53.52
30	35	34.83	37.03	101	80	89.12	83.71
37	30	30.50	28.69	98	101	109.50	100.28
27	37	22.50	39.50	116	98	117.28	91.92
48	27	47.50	24.36	135	116	137.64	116.00
42	48	52.00	53.97	108	135	105.50	131.94
29	42	38.50	38.22	89	108	88.50	94.93
32	29	20.50	27.13	89	89	88.50	82.79
27	32	22.50	33.93	88	89	78.36	86.32

56	88	41.50	84.12	19	22	20.90	24.22
103	56	112.50	46.31	22	19	27.30	18.99
72	103	74.25	113.72	36	22	36.50	24.09
65	72	67.50	57.05	37	36	30.50	39.44
59	65	81.50	64.99	54	37	44.50	36.22
49	59	68.50	55.50	38	54	47.50	57.59
45	49	37.50	46.23	32	38	20.50	32.20
34	45	36.50	44.10	28	32	30.00	32.31
49	34	68.50	31.49	10	28	10.00	27.46
52	49	55.75	53.15	8	10	8.50	7.22
41	52	41.50	50.52	9	8	6.17	10.64
39	41	38.50	38.06	6	9	4.50	10.84
31	39	25.50	39.25	4	6	4.83	7.16
18	31	21.50	29.29	14	4	20.50	5.80
17	18	21.00	16.53	16	14	15.50	18.20
14	17	20.50	18.99	19	16	20.90	17.02
10	14	10.00	14.66	33	19	36.17	20.95
11	10	7.50	11.09	69	33	63.50	36.64
22	11	27.30	13.31	91	69	78.28	75.39
19	22	20.90	25.88	83	91	52.50	90.68
87	19	75.00	18.64	54	83	44.50	76.68
108	87	105.50	102.46	44	54	46.50	45.88
105	108	94.41	103.56	66	44	58.50	42.75
63	105	54.75	99.67	113	66	94.50	70.10
45	63	37.50	50.33	136	113	128.00	118.73
21	45	22.50	42.93	129	136	124.00	132.39
46	21	41.00	16.22	57	129	60.00	120.09
46	46	41.00	53.97	35	57	39.83	37.12
43	46	39.50	43.08	71	35	67.50	34.61
22	43	27.30	42.62	88	71	78.36	78.61
11	22	7.50	17.51	89	88	88.50	86.37
12	11	10.00	11.52	80	89	95.50	85.36
9	12	6.17	14.43	103	80	112.50	74.86
2	9	0.00	9.97	105	103	94.41	105.55
2	2	0.00	2.83	97	105	96.40	99.14
5	2	7.00	4.87	101	97	89.12	91.40
7	5	7.00	7.87	111	101	106.42	98.47
1	7	0.00	9.39	100	111	110.72	108.48
3	1	4.50	1.72	94	100	87.94	92.40
6	3	4.50	6.32	99	94	104.00	89.85
9	6	6.17	8.58	112	99	83.50	96.63
11	9	7.50	11.52	123	112	115.50	110.33
16	11	15.50	13.06	131	123	134.50	119.63
22	16	27.30	18.62	132	131	135.00	126.61

142	132	146.83	125.84	74	95	81.37	80.75
99	142	104.00	138.13	61	74	53.50	69.69
102	99	92.10	82.94	51	61	62.50	57.27
112	102	83.50	102.48	37	51	30.50	48.83
109	112	107.68	108.90	43	37	39.50	34.44
92	109	84.50	103.47	68	43	67.00	45.79
79	92	74.00	84.63	62	68	63.50	72.57
50	79	46.50	74.46	64	62	55.50	57.65
30	50	34.83	42.54	61	64	53.50	64.36
20	30	21.50	27.70	53	61	54.50	58.82
27	20	22.50	19.95	55	53	66.50	50.81
70	27	68.73	30.59	57	55	60.00	55.53
102	70	92.10	79.21	45	57	37.50	56.57
56	102	41.50	103.67	45	45	37.50	41.85
62	56	63.50	41.34	45	45	37.50	46.09
87	62	75.00	66.53	45	45	37.50	44.87
81	87	49.50	89.33	45	45	37.50	45.22
61	81	53.50	75.56	45	45	37.50	45.12
35	61	39.83	55.50	45	45	37.50	45.14
23	35	20.50	30.04	59	45	81.50	45.13
20	23	21.50	22.95	72	59	74.25	61.96
23	20	20.50	21.37	64	72	55.50	72.74
7	23	7.00	25.42	53	64	54.50	60.03
6	7	4.50	5.01	40	53	33.50	50.48
31	6	25.50	9.67	27	40	22.50	37.61
15	31	15.50	38.36	21	27	22.50	25.69
18	15	21.50	10.85	24	21	23.50	21.90
38	18	47.50	22.37	13	24	11.50	26.58
31	38	25.50	43.08	3	13	4.50	12.00
35	31	39.83	28.69	3	3	4.50	4.17
28	35	30.00	37.64	5	3	7.00	6.40
27	28	22.50	26.64	5	5	7.00	8.14
18	27	21.50	28.60	5	5	7.00	7.62
23	18	20.50	17.20	10	5	10.00	7.75
40	23	33.50	26.49	17	10	21.00	13.70
45	40	37.50	44.23	16	17	15.50	20.38
95	45	98.00	45.12	11	16	7.50	17.24
89	95	88.50	104.98	8	11	8.50	12.12
101	89	89.12	80.53	4	8	4.83	9.97
115	101	123.50	102.02	13	4	11.50	5.76
103	115	112.50	112.68	14	13	20.50	17.78
128	103	112.50	95.22	9	14	6.17	15.50
136	128	128.00	130.33	8	9	8.50	10.13
95	136	98.00	129.86	6	8	4.50	10.46

12	• • • • •					
14	20.90	15.86	28	38	30.00	36.37
19	23.50	21.97	24	28	23.50	26.88
24	30.00	26.21	31	24	25.50	24.80
28	38.50	29.79	29	31	38.50	33.80
29	36.50	29.95	21	29	22.50	28.79
34	36.50	35.91	28	21	30.00	20.61
34	38.50	34.18	25	28	22.50	31.38
39	58.50	40.69	16	25	15.50	24.66
66	106.42	71.27	12	16	10.00	15.77
111	96.40	116.56	10	12	10.00	13.51
97	51.50	86.70	16	10	15.50	11.74
47	66.50	35.23	19	16	20.90	19.45
73	66.50	81.33	16	19	15.50	20.82
73	67.50	68.05	18	16	21.50	16.80
71	67.50	69.48	25	18	22.50	20.35
71	67.50	69.08	40	25	33.50	27.73
71	60.00	69.21	39	40	38.50	43.63
57	39.83	52.36	33	39	36.17	37.84
35	62.50	30.77	38	33	47.50	32.30
51	39.83	56.23	27	38	22.50	39.90
35	41.50	29.65	30	27	34.83	24.48
56	63.50	62.56	13	30	11.50	32.53
69	60.00	68.70	10	13	10.00	9.76
57	36.17	52.52	6	10	4.50	12.71
33	30.50	28.34	8	6	8.50	7.03
37	36.50	40.11	6	8	4.50	11.06
34	38.50	33.10	3	6	4.50	7.48
39	47.50	41.13	3	3	4.50	4.88
48	54.50	49.63	6	3	4.50	5.61
53	39.83	53.19	6	6	4.50	8.99
35	26.30	30.53	10	6	10.00	8.00
26	25.50	26.24	21	10	22.50	13.08
31	20.50	33.48	26	21	26.30	24.82
23	15.50	21.77	25	26	22.50	27.44
15	6.17	15.52	25	25	22.50	25.47
9	10.00	10.09	27	25	22.50	26.03
12	47.50	15.24	32	27	20.50	28.27
48	68.50	57.02	38	32	47.50	33.63
49	66.50	46.18	47	38	51.50	39.29
55	36.17	56.52	47	47	51.50	48.48
33	30.00	27.09	48	47	47.50	45.83
28	46.50	29.56	56	48	41.50	47.80
44	41.00	48.08	57	56	60.00	56.85
	$ \begin{array}{r} 19\\ 24\\ 28\\ 29\\ 34\\ 34\\ 39\\ 66\\ 111\\ 97\\ 47\\ 73\\ 73\\ 73\\ 71\\ 71\\ 71\\ 71\\ 71\\ 71\\ 73\\ 74\\ 73\\ 75\\ 75\\ 73\\ $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	19 23.50 21.97 24 30.00 26.21 28 38.50 29.79 29 36.50 29.95 34 36.50 35.91 34 38.50 34.18 39 58.50 40.69 66 106.42 71.27 111 96.40 116.56 97 51.50 86.70 47 66.50 35.23 73 66.50 81.33 73 67.50 68.05 71 67.50 69.48 71 67.50 69.48 71 67.50 69.08 71 60.00 69.21 57 39.83 52.36 35 62.50 30.77 51 39.83 56.23 35 41.50 29.65 56 63.50 62.56 69 60.00 68.70 57 36.17 52.52 33 30.50 28.34 37 36.50 40.11 34 38.50 33.10 39 47.50 41.13 48 54.50 49.63 53 39.83 53.19 35 26.30 30.53 26 25.50 26.24 31 20.50 33.48 23 15.50 21.77 15 6.17 15.24 48 68.50 57.02 49 66.50 46.18 55 36.17 56.52 33 30.00 27.09 <td< td=""><td>19$23.50$$21.97$$24$$24$$30.00$$26.21$$31$$28$$38.50$$29.79$$29$$29$$36.50$$29.95$$21$$34$$36.50$$35.91$$28$$34$$38.50$$34.18$$25$$39$$58.50$$40.69$$16$$66$$106.42$$71.27$$12$$111$$96.40$$116.56$$10$$97$$51.50$$86.70$$16$$47$$66.50$$35.23$$19$$73$$66.50$$81.33$$16$$73$$67.50$$68.05$$18$$71$$67.50$$69.08$$40$$71$$60.00$$69.21$$39$$57$$39.83$$52.36$$33$$35$$62.50$$30.77$$38$$51$$39.83$$56.23$$27$$35$$41.50$$29.65$$30$$56$$63.50$$62.56$$13$$69$$60.00$$68.70$$10$$57$$36.17$$52.52$$6$$33$$30.50$$28.34$$8$$37$$36.50$$40.11$$6$$34$$38.50$$33.10$$3$$39$$47.50$$49.63$$6$$53$$39.83$$53.19$$6$$53$$39.83$$53.19$$6$$52$$6.30$$30.53$$10$$26$$25.50$$26.24$$21$$31$$20.50$</td></td<> <td>1921.5021.97242824$30.00$$26.21$$31$$24$28$38.50$$29.79$$29$$31$29$36.50$$25.979$$29$$31$29$36.50$$25.979$$29$$31$34$36.50$$35.91$$28$$21$34$38.50$$40.69$$16$$25$$66$$106.42$$71.27$$12$$16$$111$$96.40$$116.56$$10$$12$$97$$51.50$$86.70$$16$$10$$47$$66.50$$35.23$$19$$16$$73$$67.50$$68.05$$18$$16$$71$$67.50$$69.08$$40$$25$$71$$60.00$$69.21$$39$$40$$57$$39.83$$52.36$$33$$39$$35$$62.50$$30.77$$38$$33$$51$$39.83$$56.23$$27$$38$$35$$41.50$$29.65$$30$$27$$56$$63.50$$62.56$$13$$30$$69$$60.00$$68.70$$10$$13$$37$$36.50$$40.11$$6$$8$$34$$38.50$$33.10$$3$$6$$33$$30.50$$28.34$$8$$6$$37$$36.50$$40.11$$6$$8$$34$$38.50$$33.10$$3$$6$$33$$30.50$$21.77$$25$<t< td=""><td>1923.50$21.97$2428$23.50$24$30.00$$26.21$$31$$24$$25.50$28$38.50$$29.79$$29$$31$$38.50$29$36.50$$29.95$$21$$29$$22.50$34$36.50$$35.91$$28$$21$$30.00$34$38.50$$41.18$$25$$28$$22.50$39$58.50$$40.69$$16$$25$$15.50$66$106.42$$71.27$$12$$16$$10.00$111$96.40$$116.56$$10$$12$$10.00$97$51.50$$86.70$$16$$10$$15.50$47$66.50$$35.23$$19$$16$$20.90$73$67.50$$69.48$$25$$18$$12.50$71$67.50$$69.48$$25$$18$$22.50$71$67.50$$69.08$$40$$25$$33.50$71$60.00$$69.21$$39$$40$$38.50$57$39.83$$52.236$$33$$39$$36.17$35$62.50$$30.77$$38$$33$$47.50$51$39.83$$56.23$$27$$38$$22.50$$35$$41.50$$29.65$$30$$27$$34.83$$56$$63.50$$6.33$$11.50$$6$$4.50$$33$$30.50$$28.34$$8$$6$$8.50$$37$$36.50$$41.13$$3$<</td></t<></td>	19 23.50 21.97 24 24 30.00 26.21 31 28 38.50 29.79 29 29 36.50 29.95 21 34 36.50 35.91 28 34 38.50 34.18 25 39 58.50 40.69 16 66 106.42 71.27 12 111 96.40 116.56 10 97 51.50 86.70 16 47 66.50 35.23 19 73 66.50 81.33 16 73 67.50 68.05 18 71 67.50 69.08 40 71 60.00 69.21 39 57 39.83 52.36 33 35 62.50 30.77 38 51 39.83 56.23 27 35 41.50 29.65 30 56 63.50 62.56 13 69 60.00 68.70 10 57 36.17 52.52 6 33 30.50 28.34 8 37 36.50 40.11 6 34 38.50 33.10 3 39 47.50 49.63 6 53 39.83 53.19 6 53 39.83 53.19 6 52 6.30 30.53 10 26 25.50 26.24 21 31 20.50	1921.5021.97242824 30.00 26.21 31 24 28 38.50 29.79 29 31 29 36.50 25.979 29 31 29 36.50 25.979 29 31 34 36.50 35.91 28 21 34 38.50 40.69 16 25 66 106.42 71.27 12 16 111 96.40 116.56 10 12 97 51.50 86.70 16 10 47 66.50 35.23 19 16 73 67.50 68.05 18 16 71 67.50 69.08 40 25 71 60.00 69.21 39 40 57 39.83 52.36 33 39 35 62.50 30.77 38 33 51 39.83 56.23 27 38 35 41.50 29.65 30 27 56 63.50 62.56 13 30 69 60.00 68.70 10 13 37 36.50 40.11 6 8 34 38.50 33.10 3 6 33 30.50 28.34 8 6 37 36.50 40.11 6 8 34 38.50 33.10 3 6 33 30.50 21.77 25 <t< td=""><td>1923.50$21.97$2428$23.50$24$30.00$$26.21$$31$$24$$25.50$28$38.50$$29.79$$29$$31$$38.50$29$36.50$$29.95$$21$$29$$22.50$34$36.50$$35.91$$28$$21$$30.00$34$38.50$$41.18$$25$$28$$22.50$39$58.50$$40.69$$16$$25$$15.50$66$106.42$$71.27$$12$$16$$10.00$111$96.40$$116.56$$10$$12$$10.00$97$51.50$$86.70$$16$$10$$15.50$47$66.50$$35.23$$19$$16$$20.90$73$67.50$$69.48$$25$$18$$12.50$71$67.50$$69.48$$25$$18$$22.50$71$67.50$$69.08$$40$$25$$33.50$71$60.00$$69.21$$39$$40$$38.50$57$39.83$$52.236$$33$$39$$36.17$35$62.50$$30.77$$38$$33$$47.50$51$39.83$$56.23$$27$$38$$22.50$$35$$41.50$$29.65$$30$$27$$34.83$$56$$63.50$$6.33$$11.50$$6$$4.50$$33$$30.50$$28.34$$8$$6$$8.50$$37$$36.50$$41.13$$3$<</td></t<>	1923.50 21.97 2428 23.50 24 30.00 26.21 31 24 25.50 28 38.50 29.79 29 31 38.50 29 36.50 29.95 21 29 22.50 34 36.50 35.91 28 21 30.00 34 38.50 41.18 25 28 22.50 39 58.50 40.69 16 25 15.50 66 106.42 71.27 12 16 10.00 111 96.40 116.56 10 12 10.00 97 51.50 86.70 16 10 15.50 47 66.50 35.23 19 16 20.90 73 67.50 69.48 25 18 12.50 71 67.50 69.48 25 18 22.50 71 67.50 69.08 40 25 33.50 71 60.00 69.21 39 40 38.50 57 39.83 52.236 33 39 36.17 35 62.50 30.77 38 33 47.50 51 39.83 56.23 27 38 22.50 35 41.50 29.65 30 27 34.83 56 63.50 6.33 11.50 6 4.50 33 30.50 28.34 8 6 8.50 37 36.50 41.13 3 <

57	41.50	55.45	39	39	38.50	35.53
56	41.50	54.66	49	39	68.50	39.82
41	11.50	36.87	52	49	55.75	50.60
13	6.17	8.34	52	52	55.75	51.11
9	7.50	11.74	59	52	81.50	50.97
11	4.50	13.15	80	59	95.50	59.43
6	10.00	6.72	90	80	67.83	82.24
10	7.50	13.37	94	90	87.94	87.71
11	15.50	12.64	89	94	88.50	90.96
16	21.00	18.84	128	89	112.50	84.04
17	20.90	18.25	112	128	83.50	132.95
19	15.50	20.81	111	112	106.42	99.65
15	21.50	15.25	95	111	98.00	108.08
18	30.50	20.45	111	95	106.42	86.45
37	60.00	41.78	95	111	98.00	111.95
57	54.50	59.67	69	95	63.50	85.40
53	46.50	49.72	47	69	51.50	61.82
50	60.50	48.99	73	47	66.50	42.19
60	67.00	61.22	69	73	63.50	79.11
68	71.50	67.32	48	69	47.50	63.67
58	81.37	53.56	35	48	39.83	42.89
74	54.50	76.77	20	35	21.50	33.25
53	41.00	44.85	10	20	10.00	17.99
46	33.50	45.64	22	10	27.30	10.36
40	30.50	38.20	6	22	4.50	26.97
37	11.50	36.74	8	6	8.50	2.94
13	10.00	8.31	25	8	22.50	12.26
12	21.50	15.30	33	25	36.17	29.99
20	22.50	22.89	32	33	20.50	34.48
25	22.50	26.70	16	32	15.50	31.98
27	21.50	28.00	16	16	15.50	13.46
18	15.50	16.80	14	16	20.50	18.79
15	11.50	16.41	26	14	26.30	14.84
13	23.50	14.11	26	26	26.30	30.39
24	23.50	27.98	35	26	39.83	25.90
24	22.50	23.97	46	35	41.00	38.01
21	22.50	21.52	98	46	109.50	47.74
25	20.50	27.02	134	98	131.00	107.45
32	30.50	33.84	137	134	154.50	133.53
37	20.50	37.89	128	137	112.50	129.66
32	39.50	30.71	109	128	107.68	120.00
43	41.50	46.00	102	109	92.10	99.99
56	54.50	57.22	95	102	98.00	97.38
53	38.50	50.39	115	95	123.50	89.74
	$\begin{array}{c} 57\\ 56\\ 41\\ 13\\ 9\\ 11\\ 6\\ 10\\ 11\\ 16\\ 17\\ 19\\ 15\\ 18\\ 37\\ 57\\ 53\\ 50\\ 60\\ 68\\ 58\\ 74\\ 53\\ 50\\ 60\\ 68\\ 58\\ 74\\ 53\\ 46\\ 40\\ 37\\ 13\\ 12\\ 20\\ 25\\ 27\\ 18\\ 15\\ 13\\ 24\\ 24\\ 21\\ 25\\ 32\\ 37\\ 32\\ 43\\ 56\\ 53\end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	57 41.50 55.45 56 41.50 54.66 41 11.50 36.87 13 6.17 8.34 9 7.50 11.74 11 4.50 13.15 6 10.00 6.72 10 7.50 13.37 11 15.50 12.64 16 21.00 18.84 17 20.90 18.25 19 15.50 20.81 15 21.50 15.25 18 30.50 20.45 37 60.00 41.78 57 54.50 59.67 53 46.50 49.72 50 60.50 48.99 60 67.00 61.22 68 71.50 67.32 58 81.37 53.56 74 54.50 76.77 53 41.00 44.85 46 33.50 45.64 40 30.50 38.20 37 11.50 36.74 13 10.00 8.31 12 21.50 15.30 20 22.50 22.89 25 22.50 26.70 27 21.50 21.52 25 20.50 27.98 24 22.50 23.97 21 22.50 27.92 32 39.50 30.71 43 41.50 46.00 56 54.50 57.22 53 38.50 50.39 <td>57$41.50$$55.45$$39$$56$$41.50$$54.66$$49$$41$$11.50$$36.87$$52$$13$$6.17$$8.34$$52$$9$$7.50$$11.74$$59$$11$$4.50$$13.15$$80$$6$$10.00$$6.72$$90$$10$$7.50$$13.37$$94$$11$$15.50$$12.64$$89$$16$$21.00$$18.84$$128$$17$$20.90$$18.25$$112$$19$$15.50$$20.81$$111$$15$$21.50$$15.25$$95$$18$$30.50$$20.45$$111$$37$$60.00$$41.78$$95$$57$$54.50$$59.67$$69$$53$$46.50$$49.72$$47$$50$$60.50$$48.99$$73$$60$$67.00$$61.22$$69$$68$$71.50$$67.32$$48$$58$$81.37$$53.56$$35$$74$$54.50$$76.77$$20$$53$$41.00$$44.85$$10$$46$$33.50$$45.64$$22$$40$$30.50$$38.20$$6$$37$$11.50$$36.74$$8$$13$$10.00$$8.31$$25$$12$$21.50$$22.89$$32$$25$$22.50$$26.70$$16$$27$$21.50$$23.97$$46$$21$$22.50$<</td> <td>57$41.50$$55.45$$39$$39$$56$$41.50$$54.66$$49$$39$$41$$11.50$$36.87$$52$$49$$13$$6.17$$8.34$$52$$52$$9$$7.50$$11.74$$59$$52$$9$$7.50$$13.15$$80$$59$$6$$10.00$$6.72$$90$$80$$10$$7.50$$13.37$$94$$90$$11$$15.50$$12.64$$89$$94$$16$$21.00$$18.84$$128$$89$$17$$20.90$$18.25$$112$$128$$19$$15.50$$20.81$$111$$112$$15$$21.50$$15.25$$95$$111$$18$$30.50$$20.45$$111$$95$$37$$60.00$$41.78$$95$$111$$57$$54.50$$59.67$$69$$95$$53$$46.50$$49.72$$47$$69$$50$$60.50$$48.99$$73$$47$$60$$67.00$$61.22$$69$$73$$68$$71.50$$67.77$$20$$35$$53$$41.00$$44.85$$10$$20$$46$$33.50$$45.64$$22$$10$$40$$30.50$$38.20$$6$$22$$37$$11.50$$36.74$$8$$6$$13$$10.00$$8.31$$25$$8$$12$$21.50$$28.00$</td> <td>57$41.50$$55.45$$39$$39$$38.50$$56$$41.50$$54.66$$49$$39$$68.50$$41$$11.50$$36.87$$52$$49$$55.75$$13$$6.17$$8.34$$52$$52$$55.75$$9$$7.50$$11.74$$59$$52$$81.50$$11$$4.50$$13.15$$80$$59$$95.50$$6$$10.00$$6.72$$90$$80$$67.83$$10$$7.50$$13.37$$94$$90$$87.94$$11$$15.50$$12.64$$89$$94$$88.50$$16$$21.00$$18.84$$128$$89$$112.50$$17$$20.90$$18.25$$112$$128$$83.50$$19$$15.50$$20.81$$111$$112$$106.42$$37$$60.00$$41.78$$95$$111$$98.00$$18$$30.50$$20.45$$111$$95$$164.2$$37$$60.00$$41.78$$95$$111$$98.00$$53$$46.50$$49.72$$47$$69$$51.50$$50$$60.50$$48.99$$73$$47$$66.50$$53$$46.50$$48.99$$73$$47$$66.50$$53$$41.00$$44.85$$10$$20$$10.00$$46$$33.50$$45.64$$22$$10$$27.30$$45$$50$$76.77$$20$$35$$28$$22.50$</td>	57 41.50 55.45 39 56 41.50 54.66 49 41 11.50 36.87 52 13 6.17 8.34 52 9 7.50 11.74 59 11 4.50 13.15 80 6 10.00 6.72 90 10 7.50 13.37 94 11 15.50 12.64 89 16 21.00 18.84 128 17 20.90 18.25 112 19 15.50 20.81 111 15 21.50 15.25 95 18 30.50 20.45 111 37 60.00 41.78 95 57 54.50 59.67 69 53 46.50 49.72 47 50 60.50 48.99 73 60 67.00 61.22 69 68 71.50 67.32 48 58 81.37 53.56 35 74 54.50 76.77 20 53 41.00 44.85 10 46 33.50 45.64 22 40 30.50 38.20 6 37 11.50 36.74 8 13 10.00 8.31 25 12 21.50 22.89 32 25 22.50 26.70 16 27 21.50 23.97 46 21 22.50 <	57 41.50 55.45 39 39 56 41.50 54.66 49 39 41 11.50 36.87 52 49 13 6.17 8.34 52 52 9 7.50 11.74 59 52 9 7.50 13.15 80 59 6 10.00 6.72 90 80 10 7.50 13.37 94 90 11 15.50 12.64 89 94 16 21.00 18.84 128 89 17 20.90 18.25 112 128 19 15.50 20.81 111 112 15 21.50 15.25 95 111 18 30.50 20.45 111 95 37 60.00 41.78 95 111 57 54.50 59.67 69 95 53 46.50 49.72 47 69 50 60.50 48.99 73 47 60 67.00 61.22 69 73 68 71.50 67.77 20 35 53 41.00 44.85 10 20 46 33.50 45.64 22 10 40 30.50 38.20 6 22 37 11.50 36.74 8 6 13 10.00 8.31 25 8 12 21.50 28.00	57 41.50 55.45 39 39 38.50 56 41.50 54.66 49 39 68.50 41 11.50 36.87 52 49 55.75 13 6.17 8.34 52 52 55.75 9 7.50 11.74 59 52 81.50 11 4.50 13.15 80 59 95.50 6 10.00 6.72 90 80 67.83 10 7.50 13.37 94 90 87.94 11 15.50 12.64 89 94 88.50 16 21.00 18.84 128 89 112.50 17 20.90 18.25 112 128 83.50 19 15.50 20.81 111 112 106.42 37 60.00 41.78 95 111 98.00 18 30.50 20.45 111 95 164.2 37 60.00 41.78 95 111 98.00 53 46.50 49.72 47 69 51.50 50 60.50 48.99 73 47 66.50 53 46.50 48.99 73 47 66.50 53 41.00 44.85 10 20 10.00 46 33.50 45.64 22 10 27.30 45 50 76.77 20 35 28 22.50

102	115	92.10	116.01	11	3	7.50	5.90
65	102	67.50	92.84	11	11	7.50	14.76
40	65	33.50	55.07	20	11	21.50	12.19
25	40	22.50	35.92	21	20	22.50	23.74
23	25	20.50	23.41	18	21	21.50	21.60
32	23	20.50	24.60	14	18	20.50	18.60
34	32	36.50	35.07	13	14	11.50	14.65
22	34	27.30	34.45	3	13	4.50	14.58
31	22	25.50	20.20	0	3	0.00	2.56
39	31	38.50	35.11	2	0	0.00	2.40
61	39	53.50	40.42	3	2	4.50	4.84
57	61	60.00	65.34	3	3	4.50	5.32
57	57	60.00	53.35	0	3	0.00	5.16
58	57	71.50	56.81	0	0	0.00	1.59
48	58	47.50	57.02	0	0	0.00	2.60
43	48	39.50	44.95	0	0	0.00	2.29
41	43	41.50	42.42	0	0	0.00	2.36
38	41	47.50	40.74	0	0	0.00	2.32
39	38	38.50	37.62	0	0	0.00	2.32
25	39	22.50	39.72	0	0	0.00	2.30
11	25	7.50	22.28	0	0	0.00	2.29
9	11	6.17	10.47	0	0	0.00	2.27
9	9	6.17	11.46	1	0	0.00	2.26
8	9	8.50	11.15	2	1	0.00	3.45
9	8	6.17	10.02	6	2	4.50	4.29
8	9	8.50	11.53	8	6	8.50	8.84
2	8	0.00	9.88	4	8	4.83	9.92
0	2	0.00	3.13	2	4	0.00	4.79
0	0	0.00	2.65	3	2	4.50	3.85
0	0	0.00	2.77	12	3	10.00	5.31
0	0	0.00	2.71	10	12	10.00	15.69
0	0	0.00	2.71	16	10	15.50	10.28
0	0	0.00	2.69	7	16	7.00	19.04
1	0	0.00	2.67	9	7	6.17	5.69
6	1	4.50	3.86	15	9	15.50	11.93
14	6	20.50	9.51	10	15	10.00	17.33
9	14	6.17	17.48	9	10	6.17	9.76
6	9	4.50	9.16	5	9	7.00	10.73
4	6	4.83	7.94	0	5	0.00	5.63
4	4	4.83	5.87	0	0	0.00	1.07
4	4	4.83	6.45	0	0	0.00	2.37
2	4	0.00	6.26	1	0	0.00	1.98
1	2	0.00	3.89	2	1	0.00	3.28
3	1	4.50	3.36	2	2	0.00	4.09

0	2	0.00	3.84	0	0	0.00	1.80
0	0	0.00	1.50	0	0	0.00	1.62
2	0	0.00	2.16	1	0	0.00	1.66
4	2	4.83	4.36	1	1	0.00	2.84
5	4	7.00	6.11	0	1	0.00	2.49
10	5	10.00	6.80	0	0	0.00	1.37
12	10	10.00	12.60	2	0	0.00	1.68
9	12	6.17	13.32	3	2	4.50	3.99
15	9	15.50	9.50	16	3	15.50	4.51
21	15	22.50	17.80	17	16	21.00	19.98
28	21	30.00	22.61	18	17	21.50	16.72
25	28	22.50	29.63	37	18	30.50	18.86
18	25	21.50	24.00	25	37	22.50	41.08
11	18	7.50	17.21	26	25	26.30	20.25
6	11	4.50	10.75	34	26	36.50	27.46
3	6	4.50	6.59	45	34	37.50	35.00
4	3	4.83	4.17	55	45	66.50	46.05
1	4	0.00	6.06	53	55	54.50	54.89
0	1	0.00	1.89	53	53	54.50	49.95
1	0	0.00	1.88	51	53	62.50	51.39
2	1	0.00	3.07	37	51	30.50	48.59
2	2	0.00	3.92	18	37	21.50	32.58
1	2	0.00	3.66	11	18	7.50	14.36
1	1	0.00	2.52	11	11	7.50	11.19
0	1	0.00	2.83	10	11	10.00	12.10
0	0	0.00	1.53	10	10	10.00	10.63
0	0	0.00	1.89	12	10	10.00	11.05
3	0	4.50	1.77	15	12	15.50	13.32
4	3	4.83	5.40	17	15	21.00	16.27
4	4	4.83	5.54	27	17	22.50	17.82
1	4	0.00	5.49	36	27	36.50	29.39
0	1	0.00	1.89	32	36	20.50	36.87
2	0	0.00	1.71	54	32	44.50	29.91
14	2	20.50	4.15	62	54	63.50	58.37
17	14	21.00	17.86	61	62	53.50	59.79
15	17	15.50	17.51	71	61	67.50	58.20
13	15	11.50	15.20	66	71	58.50	70.70
8	13	8.50	13.46	86	66	93.14	61.10
5	8	7.00	7.94	119	86	118.83	87.93
7	5	7.00	5.92	106	119	117.33	119.90
13	7	11.50	8.90	99	106	104.00	95.10
8	13	8.50	15.24	89	99	88.50	93.87
1	8	0.00	7.39	84	89	71.00	82.24
0	1	0.00	1.23	84	84	71.00	79.61

87	84	75.00	80.39	35
65	87	67.50	83.80	46
39	65	38.50	56.40	48
36	39	36.50	33.06	47
27	36	22.50	36.19	36
23	27	20.50	24.47	24
33	23	36.17	23.04	13
39	33	38.50	35.47	9
30	39	34.83	39.10	19
24	30	23.50	27.24	39
23	24	20.50	23.45	56
12	23	10.00	23.34	73
10	12	10.00	10.14	105
10	10	10.00	11.53	116
21	10	22.50	11.12	113
27	21	22.50	24.46	100
25	27	22.50	27.82	105
35	25	39.83	24.44	156
27	35	22.50	37.44	156
18	27	21.50	24.08	160
15	18	15.50	17.11	165
9	15	6.17	15.51	159
7	9	7.00	8.75	
7	7	7.00	8.28	
8	7	8.50	8.41	
9	8	6.17	9.56	
8	9	8.50	10.42	
7	8	7.00	8.96	
7	7	7.00	8.17	
1	7	0.00	8.39	
5	1	7.00	1.10	
14	5	20.50	8.00	
33	14	36.17	16.82	
35	33	39.83	37.11	
23	35	20.50	33.67	
18	23	21.50	20.24	
19	18	20.90	18.10	
2	19	0.00	19.91	
0	2	0.00	1.05	
0	0	0.00	2.57	
0	0	0.00	1.52	
3	0	4.50	1.81	
6	3	4.50	5.32	
22	6	27.30	7.90	

5	22	39.83	26.38
5	35	41.00	36.68
3	46	47.50	46.94
7	48	51.50	46.39
5	47	36.50	45.36
4	36	23.50	32.44
3	24	11.50	21.74
9	13	6.17	11.60
9	9	20.90	9.71
9	19	38.50	22.27
5	39	41.50	42.69
3	56	66.50	57.24
5	73	94.41	73.50
5	105	117.28	107.30
3	116	94.50	110.81
)	113	110.72	106.24
5	100	94.41	91.97
5	105	148.83	102.13
5	156	148.83	160.55
)	156	167.50	143.76
5	160	170.50	153.47
)	165	136.50	156.75

				0	0	0.00	2.24
				0	0	0.00	2.45
5.2.2.	Wolfe Island	d Wind Fa	arm	0	0	0.00	2.38
	Forecasted	Data		0	0	0.00	2.38
			1	0	0	0.00	2.37
	The data belo	ow gives i	ine forecasts	0	0	0.00	2.36
				0	0	0.00	2.35
produce	ed by each mo	odel over t	he period of	0	0	0.00	2.33
				0	0	0.00	2.32
the val	idation data f	for Wolfe	Island wind	0	0	0.00	2.31
				0	0	0.00	2.30
farm. I	t is used to	generate th	ne plots and	0	0	0.00	2.29
				2	0	5.50	2.28
tables in	n section 3.3.			5	2	10.50	4.69
				6	5	5.50	7.59
				0	6	0.00	7.92
Actual	Persistence	Markov	ARMA	0	0	0.00	0.54
4	0	6 50	3 79	2	0	5.50	2.74
6	4	5 50	7 13	2	2	5.50	4.49
3	6	4.50	8.54	13	2	12.50	3.95
6	3	5.50	4.46	43	13	44.00	17.44
12	6	9.50	9.31	50	43	45.50	49.75
22	12	21.50	15.11	53	50	50.50	48.52
14	22	20.50	25.48	54	53	51.50	52.54
9	14	9.50	12.66	44	54	50.50	52.55
11	9	7.50	10.44	29	44	38.50	40.43
10	11	12.50	13.52	36	29	34.83	25.89
19	10	25.50	11.37	56	36	53.50	38.75
21	19	21.50	22.92	70	56	//.50	59.13
20	21	22.50	21.86	107	70	107.77	69.99
19	20	25.50	20.96	94	107	91.57	111.60
23	19	22.50	20.01	94	94	91.57	83.35
13	23	12.50	25.14	94	94	91.57	91.87
14	13	20.50	11.47	94	94	91.57	89.33
15	14	13.50	16.78	94	94	91.57	90.12
17	15	21.50	16.38	31	94	30.50	42.91
23	17	22.50	18.92	33	<u></u> ১।	32.50	13.01
39	23	37.10	25.42	30 20	20	21.50	20.90
50	39	45.50	42.86	30	30 20	21.50	27 00
38	50	31.50	50.96	30	30 20	21.50	37.00
27	38	29.50	33.98	30	30 20	21.50	27 70
14	27	20.50	25.75	30	30 20	21.50	27.79
6	14	5.50	12.45	30 20	20	21.50	27.70
4	6	6.50	6.74	30 20	30 20	31.50	31.10 27 70
6	4	5.50	6.02	30 20	30 20	31.50	31.10 27 70
0	6	0.00	8.65	30 20	30 20	31.50	31.10 07 70
0	0	0.00	0.57	30 20	00 20	31.50	31.10 27 70
0	0	0.00	2.99	30	38	31.50	31.18

38	38	31.50	37.78	12	6	9.50	7.62
4	38	6.50	37.78	29	12	38.50	14.86
1	4	0.00	-3.44	50	29	45.50	33.29
0	1	0.00	5.30	67	50	62.50	53.21
0	0	0.00	1.45	55	67	72.50	67.84
0	0	0.00	2.59	62	55	78.00	48.90
0	0	0.00	2.23	91	62	65.50	63.09
0	0	0.00	2.33	96	91	92.50	94.00
0	0	0.00	2.28	113	96	103.21	90.79
0	0	0.00	2.28	97	113	109.50	112.40
9	0	9.50	2.27	81	97	83.03	86.53
10	9	12.50	13.17	74	81	77.50	74.94
11	10	7.50	11.10	83	74	52.50	69.96
11	11	7.50	12.92	70	83	77.50	82.39
10	11	12.50	12.36	103	70	112.50	62.91
12	10	9.50	11.31	99	103	93.28	108.79
18	12	15.83	14.04	66	99	79.50	90.17
8	18	9.50	20.49	54	66	51.50	55.79
5	8	10.50	6.42	50	54	45.50	51.59
5	5	10.50	7.00	50	50	45.50	48.01
2	5	5.50	6.81	50	50	45.50	49.09
1	2	0.00	3.22	44	50	50.50	48.77
5	1	10.50	3.08	46	44	47.00	41.60
10	5	12.50	7.96	44	46	50.50	46.19
15	10	13.50	12.54	36	44	34.83	42.39
26	15	18.50	17.21	54	36	51.50	33.84
17	26	21.50	29.14	44	54	50.50	58.23
21	17	21.50	14.64	49	44	50.00	38.78
26	21	18.50	23.84	68	49	79.00	50.70
24	26	25.50	27.13	84	68	83.00	70.16
20	24	22.50	23.72	134	84	123.08	83.72
30	20	31.50	19.89	126	134	123.15	140.28
16	30	20.83	33.16	106	126	111.42	113.61
11	16	7.50	12.19	103	106	112.50	97.42
10	11	12.50	12.43	98	103	107.50	98.68
5	10	10.50	11.14	53	98	50.50	92.27
2	5	5.50	5.45	61	53	62.50	39.66
9	2	9.50	3.51	84	61	83.00	65.19
9	9	9.50	12.57	63	84	53.50	85.41
2	9	5.50	9.84	36	63	34.83	53.88
8	2	9.50	2.17	31	36	36.50	30.64
6	8	5.50	11.74	48	31	42.50	31.57
5	6	10.50	6.42	60	48	51.00	51.90
2	5	5.50	6.80	71	60	73.25	60.34
2	2	5.50	3.04	49	71	50.00	71.14
2	2	5.50	4.16	59	49	62.00	41.23
5	2	10.50	3.81	83	59	52.50	62.36
6	5	5.50	7.54	88	83	86.83	85.11

85	88	70.50	84.35	19	8	25.50	11.53
80	85	67.83	80.96	16	19	20.83	22.74
86	80	62.50	75.94	11	16	7.50	15.73
85	86	70.50	84.74	10	11	12.50	11.77
78	85	85.50	80.90	8	10	9.50	11.73
81	78	83.03	73.59	12	8	9.50	9.31
65	81	66.67	79.44	14	12	20.50	14.88
57	65	54.50	58.30	17	14	21.50	15.62
34	57	26.50	54.97	24	17	25.50	19.02
19	34	25.50	28.09	24	24	25.50	26.48
34	19	26.50	17.98	37	24	39.50	24.23
25	34	28.50	39.20	40	37	37.50	40.66
30	25	31.50	21.91	38	40	31.50	39.36
37	30	39.50	33.16	51	38	37.50	37.33
33	37	32.50	38.26	80	51	67.83	53.70
37	33	39.50	31.88	101	80	88.50	83.95
47	37	59.50	38.64	98	101	107.50	100.33
33	47	32.50	48.73	116	98	109.50	91.79
35	33	36.00	28.73	135	116	133.00	116.21
30	35	31.50	37.17	108	135	105.17	131.94
37	30	39.50	28.56	89	108	88.50	94.51
27	37	29.50	39.63	89	89	88.50	82.76
48	27	42.50	24.18	88	89	86.83	86.31
42	48	41.50	54.28	56	88	53.50	84.05
29	42	38.50	37.96	103	56	112.50	45.95
32	29	35.30	27.11	72	103	67.50	114.40
27	32	29.50	34.00	65	72	66.67	56.26
37	27	39.50	25.87	59	65	62.00	65.27
43	37	44.00	40.43	49	59	50.00	55.30
43	43	44.00	43.33	45	49	45.83	46.18
45	43	45.83	42.46	34	45	26.50	44.07
39	45	37.10	45.15	49	34	50.00	31.37
31	39	36.50	37.07	52	49	51.50	53.38
28	31	33.50	29.80	41	52	38.10	50.40
22	28	21.50	28.34	39	41	37.10	37.96
19	22	25.50	21.50	31	39	36.50	39.28
22	19	21.50	19.91	18	31	15.83	29.18
15	22	13.50	24.02	17	18	21.50	16.45
12	15	9.50	14.29	14	17	20.50	19.06
6	12	5.50	13.57	10	14	12.50	14.63
3	6	4.50	6.50	11	10	7.50	11.10
1	3	0.00	4.97	22	11	21.50	13.36
0	1	0.00	2.99	19	22	25.50	26.01
0	0	0.00	2.36	87	19	80.50	18.56
0	0	0.00	2.54	108	87	105.17	103.24
1	0	0.00	2.47	105	108	99.59	103.26
2	1	5.50	3.69	63	105	53.50	99.64
8	2	9.50	4.52	45	63	45.83	49.83

21	45	21.50	43.00	88	71	86.83	78.94
46	21	47.00	15.96	89	88	88.50	86.30
46	46	47.00	54.39	80	89	67.83	85.32
43	46	44.00	42.84	103	80	112.50	74.72
22	43	21.50	42.68	105	103	99.59	105.81
11	22	7.50	17.26	97	105	109.50	98.91
12	11	9.50	11.56	101	97	88.50	91.32
9	12	9.50	14.48	111	101	117.50	98.47
2	9	5.50	9.95	100	111	94.50	108.47
2	2	5.50	2.81	94	100	91.57	92.16
5	2	10.50	4.94	99	94	93.28	89.81
7	5	10.50	7.92	112	99	127.50	96.60
1	7	0.00	9.44	123	112	113.50	110.34
3	1	4.50	1.70	131	123	134.50	119.58
6	3	5.50	6.43	132	131	132.50	126.53
9	6	9.50	8.63	142	132	141.25	125.69
11	9	7.50	11.60	99	142	93.28	138.11
16	11	20.83	13.12	102	99	94.00	82.28
22	16	21.50	18.71	112	102	127.50	102.72
19	22	25.50	24.29	109	112	110.69	108.72
22	19	21.50	18.97	92	109	73.83	103.31
36	22	34.83	24.20	79	92	68.50	84.35
37	36	39.50	39.60	50	79	45.50	74.31
54	37	51.50	36.18	30	50	31.50	42.18
38	54	31.50	57.82	20	30	22.50	27.60
32	38	35.30	31.92	27	20	29.50	19.85
28	32	33.50	32.43	70	27	77.50	30.66
10	28	12.50	27.43	102	70	94.00	79.54
8	10	9.50	7.10	56	102	53.50	103.65
9	8	9.50	10.78	62	56	78.00	40.65
6	9	5.50	10.87	87	62	80.50	66.87
4	6	6.50	7.20	81	87	83.03	89.30
14	4	20.50	5.86	61	81	62.50	75.30
16	14	20.83	18.38	35	61	36.00	55.28
19	16	25.50	17.03	23	35	22.50	29.78
33	19	32.50	21.06	20	23	22.50	22.89
69	33	63.50	36.82	23	20	22.50	21.32
91	69	65.50	75.73	7	23	10.50	25.42
83	91	52.50	90.71	6	7	5.50	4.77
54	83	51.50	76.53	31	6	36.50	9.75
44	54	50.50	45.65	15	31	13.50	38.55
66	44	79.50	42.82	18	15	15.83	10.49
113	66	103.21	70.35	38	18	31.50	22.55
136	113	116.50	119.07	31	38	36.50	43.16
129	136	121.28	132.34	35	31	36.00	28.47
57	129	54.50	119.90	28	35	33.50	37.73
35	57	36.00	36.38	27	28	29.50	26.46
71	35	73.25	34.83	18	27	15.83	28.63

23	18	22.50	17.06	8	11	9.50	12.09
40	23	37.50	26.59	4	8	6.50	9.97
45	40	45.83	44.33	13	4	12.50	5.74
95	45	104.50	45.05	14	13	20.50	17.91
89	95	88.50	105.46	9	14	9.50	15.45
101	89	88.50	80.04	8	9	9.50	10.11
115	101	111.50	102.25	6	8	5.50	10.49
103	115	112.50	112.57	12	6	9.50	7.94
128	103	112.50	94.94	19	12	25.50	15.96
136	128	116.50	130.58	24	19	25.50	22.02
95	136	104.50	129.60	28	24	33.50	26.25
74	95	77.50	80.22	29	28	38.50	29.82
61	74	62.50	69.62	34	29	26.50	29.96
51	61	37.50	57.06	34	34	26.50	35.97
37	51	39.50	48.72	39	34	37.10	34.16
43	37	44.00	34.25	66	39	79.50	40.76
68	43	79.00	45.87	111	66	117.50	71.51
62	68	78.00	72.69	97	111	109.50	116.84
64	62	62.21	57.36	47	97	59.50	86.26
61	64	62.50	64.40	73	47	79.50	34.85
53	61	50.50	58.65	73	73	79.50	81.84
55	53	72.50	50.69	71	73	73.25	67.72
57	55	54.50	55.51	71	71	73.25	69.55
45	57	45.83	56.49	71	71	73.25	69.01
45	45	45.83	41.65	57	71	54.50	69.18
45	45	45.83	46.11	35	57	36.00	52.17
45	45	45.83	44.77	51	35	37.50	30.62
45	45	45.83	45.17	35	51	36.00	56.49
45	45	45.83	45.05	56	35	53.50	29.31
45	45	45.83	45.08	69	56	63.50	62.94
59	45	62.00	45.07	57	69	54.50	68.60
72	59	67.50	62.05	33	57	32.50	52.36
64	72	62.21	72.71	37	33	39.50	28.15
53	64	50.50	59.81	34	37	26.50	40.27
40	53	37.50	50.36	39	34	37.10	32.99
27	40	29.50	37.44	48	39	42.50	41.23
21	27	21.50	25.56	53	48	50.50	49.66
24	21	25.50	21.85	35	53	36.00	53.19
13	24	12.50	26.60	26	35	18.50	30.31
3	13	4.50	11.82	31	26	36.50	26.28
3	3	4.50	4.13	23	31	22.50	33.54
5	3	10.50	6.42	15	23	13.50	21.65
5	5	10.50	8.14	9	15	9.50	15.52
5	5	10.50	7.61	12	9	9.50	10.08
10	5	12.50	7.75	48	12	42.50	15.34
17	10	21.50	13.75	49	48	50.00	57.39
16	17	20.83	20.42	55	49	72.50	45.96
11	16	7.50	17.19	33	55	32.50	56.67

28	33	33.50	26.78	41	56	38.10	54.71
44	28	50.50	29.70	13	41	12.50	36.75
46	44	47.00	48.22	9	13	9.50	8.20
38	46	31.50	45.07	11	9	7.50	11.93
28	38	33.50	36.32	6	11	5.50	13.22
24	28	25.50	26.83	10	6	12.50	6.76
31	24	36.50	24.82	11	10	7.50	13.53
29	31	38.50	33.90	16	11	20.83	12.70
21	29	21.50	28.74	17	16	21.50	19.00
28	21	33.50	20.59	19	17	25.50	18.31
25	28	28.50	31.52	15	19	13.50	20.93
16	25	20.83	24.59	18	15	15.83	15.28
12	16	9.50	15.75	37	18	39.50	20.61
10	12	12.50	13.55	57	37	54.50	42.04
16	10	20.83	11.77	53	57	50.50	59.84
19	16	25.50	19.57	50	53	45.50	49.64
16	19	20.83	20.85	60	50	51.00	49.08
18	16	15.83	16.82	68	60	79.00	61.38
25	18	28.50	20.45	58	68	57.50	67.39
40	25	37 50	27.83	74	58	77 50	53 47
39	40	37 10	43 79	53	74	50 50	77.06
33	39	32 50	37 78	46	53	47.00	44 52
38	33	31.50	32 31	40	46	37 50	45.82
27	38	29 50	40.01	37	40	39.50	38.16
30	27	31 50	24 36	13	37	12 50	36.82
13	30	12 50	24.00	10	13	9.50	8 12
10	13	12.50	9 57	20	10	22 50	15 53
6	10	5 50	12.88	20	20	28.50	22.00
8	6	9.50	7.02	25	20	20.50	26.80
6	8	5.50	11 10	18	23	15.83	20.00
3	6	4 50	7.50	15	18	13.00	16 78
3	3	4.50	1.00	13	10	12.50	16.70
5	3	4.50	4.90 5.70	13	13	25 50	14 17
6	5	5.50	0.10	24	13	25.50	29.20
10	6	12.50	9.10	24	24	20.00	20.20
10	10	12.00	0.00	21	24	21.00	23.90
21	10	21.00	13.Z1 24.00	20	21	20.00	21.00
20	21	10.00	24.99	3Z 27	20	35.30	27.10
20	20	20.00	27.30	37 22	32	39.50	33.97 27.00
20	20	20.50	20.00	3Z	37	35.30	37.90
27	25	29.50	20.11	43	32	44.00	30.71
32	27	35.30	28.30	56	43	53.50	46.23
38	32	31.50	33.74	53	56	50.50	57.33
47	38	59.50	39.39	39	53	37.10	50.36
4/	47	59.50	48.60	39	39	37.10	35.49
48	47	42.50	45.84	49	39	50.00	39.96
56	48	53.50	47.88	52	49	51.50	50.74
57	56	54.50	56.97	52	52	51.50	51.14
56	57	53.50	55.46	59	52	62.00	51.03

80	59	67.83	59.55	39	31	37.10	35.31
90	80	72.50	82.46	61	39	62.50	40.43
94	90	91.57	87.71	57	61	54.50	65.56
89	94	88.50	91.00	57	57	54.50	53.16
128	89	112.50	83.97	58	57	57.50	56.89
112	128	127.50	133.39	48	58	42.50	56.99
111	112	117.50	99.17	43	48	44.00	44.84
95	111	104.50	108.28	41	43	38.10	42.43
111	95	117.50	86.17	38	41	31.50	40.73
95	111	104.50	112.24	39	38	37.10	37.61
69	95	63.50	85.03	25	39	28.50	39.76
47	69	59.50	61.71	11	25	7.50	22.13
73	47	79.50	42.06	9	11	9.50	10.45
69	73	63.50	79.49	9	9	9.50	11.52
48	69	42.50	63.40	8	9	9.50	11.19
35	48	36.00	42.79	9	8	9.50	10.06
20	35	22.50	33.22	8	9	9.50	11.60
10	20	12.50	17.91	2	8	5.50	9.91
22	10	21.50	10.38	0	2	0.00	3.13
6	22	5.50	27.18	0	0	0.00	2.73
8	6	9.50	2.72	0	0	0.00	2.83
25	8	28.50	12.49	0	0	0.00	2.78
33	25	32.50	30.15	0	0	0.00	2.78
32	33	35.30	34.53	0	0	0.00	2.76
16	32	20.83	32.00	1	0	0.00	2.75
16	16	20.83	13.35	6	1	5.50	3.95
14	16	20.50	18.95	14	6	20.50	9.63
26	14	18.50	14.83	9	14	9.50	17.61
26	26	18.50	30.61	6	9	5.50	9.14
35	26	36.00	25.86	4	6	6 50	8.04
46	35	47.00	38 19	4	4	6 50	5.93
98	46	107 50	47 82	4	4	6 50	6.55
134	98	123.08	107.97	2	4	5.50	6.35
137	134	128.36	133.56	- 1	2	0.00	3.97
128	137	112.50	129.54	3	- 1	4.50	3.45
109	128	110.69	119.87	11	3	7.50	6.02
102	109	94.00	99.78	11	11	7.50	14.93
95	102	104 50	97.36	20	11	22 50	12 24
115	95	111 50	89.63	21	20	21 50	23.95
102	115	94.00	116.22	18	21	15.83	21.63
65	102	66 67	92 49	14	18	20.50	18 68
40	65	37 50	54 79	13	14	12 50	14 71
25	40	28.50	35.82	3	13	4 50	14 68
23	25	22.50	23.34	0	.0	0.00	2.56
32	23	35.30	24 66	2	0	5 50	2 55
34	.32	26.50	35 17	- 3	2	4 50	4.96
22	34	21.50	34 43	3	- 3	4 50	5 43
31	22	36.50	20.10	0	3	0.00	5.28
• •		20.00		•	5	0.00	5.25

0	0	0.00	1.67	1	4	0.00	6.25
0	0	0.00	2.74	0	1	0.00	2.03
0	0	0.00	2.41	1	0	0.00	2.07
0	0	0.00	2.49	2	1	5.50	3.26
0	0	0.00	2.45	2	2	5.50	4.10
0	0	0.00	2.45	1	2	0.00	3.84
0	0	0.00	2.43	1	1	0.00	2.69
0	0	0.00	2.42	0	1	0.00	3.02
0	0	0.00	2.41	0	0	0.00	1.70
1	0	0.00	2.40	0	0	0.00	2.09
2	1	5.50	3.60	3	0	4.50	1.96
6	2	5.50	4.44	4	3	6.50	5.62
8	6	9.50	9.02	4	4	6.50	5.72
4	8	6.50	10.06	1	4	0.00	5.68
2	4	5.50	4.88	0	1	0.00	2.04
3	2	4.50	4.00	2	0	5.50	1.91
12	3	9.50	5.46	14	2	20.50	4.37
10	12	12.50	15.92	17	14	21.50	18.17
16	10	20.83	10.34	15	17	13.50	17.65
7	16	10.50	19.29	13	15	12.50	15.37
9	7	9.50	5.68	8	13	9.50	13.63
15	9	13.50	12.18	5	8	10.50	8.08
10	15	12.50	17.49	7	5	10.50	6.10
9	10	9.50	9.82	13	7	12.50	9.11
5	9	10.50	10.91	8	13	9.50	15.48
0	5	0.00	5.72	1	8	0.00	7.49
0	0	0.00	1.21	0	1	0.00	1.40
0	0	0.00	2.55	0	0	0.00	2.01
1	0	0.00	2.13	0	0	0.00	1.81
2	1	5.50	3.46	1	0	0.00	1.86
2	2	5.50	4.26	1	1	0.00	3.05
0	2	0.00	4.00	0	1	0.00	2.68
0	0	0.00	1.64	0	0	0.00	1.57
2	0	5.50	2.34	2	0	5.50	1.89
4	2	6.50	4.54	3	2	4.50	4.21
5	4	10.50	6.29	16	3	20.83	4.71
10	5	12.50	6.97	17	16	21.50	20.31
12	10	9.50	12.81	18	17	15.83	16.83
9	12	9.50	13.47	37	18	39.50	19.08
15	9	13.50	9.63	25	37	28.50	41.44
21	15	21.50	18.05	26	25	18.50	20.17
28	21	33.50	22.78	34	26	26.50	27.78
25	28	28.50	29.84	45	34	45.83	35.19
18	25	15.83	24.08	55	45	72.50	46.30
11	18	7.50	17.32	53	55	50.50	55.09
6	11	5.50	10.86	53	53	50.50	50.04
3	6	4.50	6.74	51	53	37.50	51.57
4	3	6.50	4.33	37	51	39.50	48.69
18	37	15.83	32.59	9	8	9.50	9.70
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11	18	7.50	14.40	8	9	9.50	10.55
11	11	7.50	11.38	7	8	10.50	9.07
10	11	12.50	12.28	7	7	10.50	8.30
10	10	12.50	10.79	1	7	0.00	8.52
12	10	9.50	11.23	5	1	10.50	1.17
15	12	13.50	13.52	14	5	20.50	8.22
17	15	21.50	16.46	33	14	32.50	17.00
27	17	29.50	17.99	35	33	36.00	37.39
36	27	34.83	29.65	23	35	22.50	33.68
32	36	35.30	37.06	18	23	15.83	20.25
54	32	51.50	29.99	19	18	25.50	18.23
62	54	78.00	58.79	2	19	5.50	20.04
61	62	62.50	59.84	0	2	0.00	-1.12
71	61	73.25	58.33	0	0	0.00	2.81
66	71	79.50	70.92	0	0	0.00	1.62
86	66	62.50	61.09	3	0	4.50	1.96
119	86	126.50	88.31	6	3	5.50	5.48
106	119	111.42	120.16	22	6	21.50	8.05
99	106	93.28	94.86	35	22	36.00	26.67
89	99	88.50	94.01	46	35	47.00	36.83
84	89	83.00	82.17	48	46	42.50	47.12
84	84	83.00	79.69	47	48	59.50	46.46
87	84	80.50	80.46	36	47	34.83	45.45
65	87	66.67	83.89	24	36	25.50	32.42
39	65	37.10	56.20	13	24	12.50	21.79
36	39	34.83	33.02	9	13	9.50	11.65
27	36	29.50	36.36	19	9	25.50	9.84
23	27	22.50	24.44	39	19	37.10	22.50
33	23	32.50	23.17	56	39	53.50	42.94
39	33	37.10	35.68	73	56	79.50	57.41
30	39	31.50	39.19	105	73	99.59	73.69
24	30	25.50	27.23	116	105	109.50	107.61
23	24	22.50	23.55	113	116	103.21	110.78
12	23	9.50	23.44	100	113	94.50	106.22
10	12	12.50	10.13	105	100	99.59	91.86
10	10	12.50	11.70	156	105	158.00	102.27
21	10	21.50	11.22	156	156	158.00	161.01
27	21	29.50	24.70	160	156	161.50	143.40
25	27	28.50	27.91	165	160	170.50	153.60
35	25	36.00	24.52	159	165	160.50	156.64
27	35	29.50	37.66				
18	27	15.83	24.01				
15	18	13.50	17.20				
9	15	9.50	15.61				
7	9	10.50	8.81				
7	7	10.50	8.42				
8	7	9.50	8.53				

5.2.3.	ERCOT System-wide			
	Forecasted Data			

The data below gives the forecasts produced by each model over the period of the validation data for ERCOT system-wide. It is used to generate the plots and tables in section 3.4.

Actual	Persistence	Markov	ARMA
6953.88	6865.02	7693.56	6953.90
6964.82	6953.88	6533.42	6630.00
7560.1	6964.82	7458.04	7086.10
7505.61	7560.1	7458.04	7977.70
6859.51	7505.61	7693.56	7155.30
6468.97	6859.51	5800.70	6383.00
5894.84	6468.97	6594.48	6303.70
5142.95	5894.84	5190.10	5393.50
5158.75	5142.95	5190.10	4666.60
5382.66	5158.75	6289.18	5385.00
4778.69	5382.66	5190.10	5416.90
4119.7	4778.69	4359.68	4151.00
3718.63	4119.7	4050.31	3808.80
3719.3	3718.63	4050.31	3479.10
3374.31	3719.3	4335.26	3815.60
3338.69	3374.31	4335.26	2967.70
3664.04	3338.69	4050.31	3496.10
4704.71	3664.04	4945.86	3846.90
5844.89	4704.71	5678.58	5531.30
5544.6	5844.89	5556.46	6401.60
3903.39	5544.6	3317.59	4907.50
3566.71	3903.39	2808.76	2683.10
4104.15	3566.71	4359.68	3885.80
4187.59	4104.15	4274.20	4392.40
4629.46	4187.59	4762.68	4068.20
4816.23	4629.46	5190.10	5063.20
5215.44	4816.23	5190.10	4707.80
5214.61	5215.44	5190.10	5597.90
4434.27	5214.61	4884.80	4955.40
3892.21	4434.27	3317.59	3805.80
3425.81	3892.21	3968.90	3693.10
2940.78	3425.81	3480.42	3067.00
3084.9	2940.78	2442.40	2656.40
3718.1	3084.9	4050.31	3345.60
4074.4	3718.1	4359.68	4131.30

4180.54	4074.4	4274.20	4142.40
4038.94	4180.54	4359.68	4202.80
3762.79	4038.94	4050.31	3856.40
3454.73	3762.79	3968.90	3569.20
3840.56	3454.73	3317.59	3240.30
4904.17	3840.56	5251.16	4281.40
5146.76	4904.17	5190.10	5609.30
5249.03	5146.76	5190.10	4938.90
5245.77	5249.03	5190.10	5408.40
5607.97	5245.77	5556.46	5105.90
5158.31	5607.97	5190.10	5969.30
5275.15	5158.31	5637.87	4492.30
4921.21	5275.15	5251.16	5698.30

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